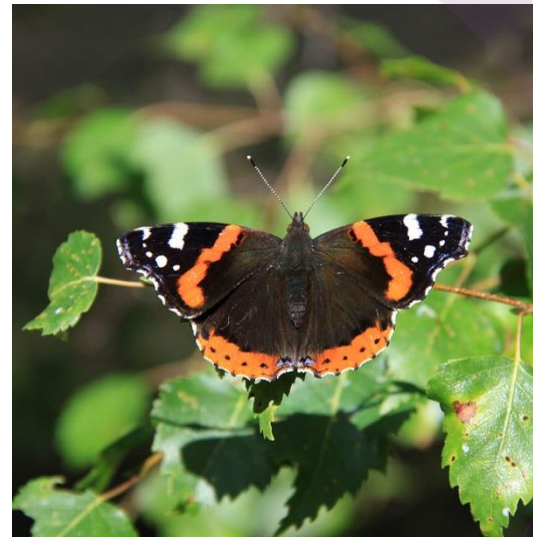


Mid Sussex District Council

Air quality modelling to inform the Site Allocations Development Plan Document

Ashdown Forest – Sites DPD Scenario Results

Air Quality Assessment




Report for

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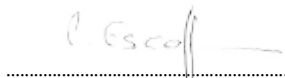
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Document revisions

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| 1 | Draft Report | 31/1/2020 |
| 2 | Final Report | 27/02/2020 |
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Executive summary

Purpose of this report

Mid Sussex District Council (MSDC) has produced a Site Allocations Development Plan Document to identify where new housing and employment uses will be delivered. As part of the plan-making process, a Habitats Regulations Assessment is being undertaken to determine the potential significant impacts to sensitive species and habitats within Ashdown Forest. This report has been prepared as part of the wider Habitats Regulations Assessment and addresses potential air quality impacts.

The ADMS-Roads dispersion model has been used to model the dispersion of pollutants from traffic emissions at ecological receptors by defining a series of perpendicular transects up to 200 m from the roadside throughout Ashdown Forest. Concentrations of NO_x and NH₃ were predicted without and with traffic flows associated with MSDC site allocations, including consideration of in-combination traffic flows from adjoining local authorities' development plans. The current version of traffic data is referred to as the Sites DPD Scenario, which will be used to inform the next stage of the Site Allocations Development Plan Document.

A conservative approach has been adopted throughout, including the assumption that background concentrations will not improve in future years, as well as the use of the strictest appropriate critical loads and levels.

The main findings of the assessment are shown in Table i.

Table i Summary of results

| Pollutant | Assessment criteria | Background* | Results summary |
|-----------------------------------|-----------------------|--|--|
| Annual mean NO_x | 30 µgm ⁻³ | 10.04 µgm ⁻³ to 11.36 µgm ⁻³ | Predicted annual mean concentrations of NO _x exceed the critical level up to 10 m from the roadside, but reduce to less than 30 µgm ⁻³ beyond this. |
| Daily mean NO_x | 200 µgm ⁻³ | 20.08 µgm ⁻³ to 22.73 µgm ⁻³ | No exceedance across any modelled transects. |
| NH₃ | 1 µgm ⁻³ | 0.76 µgm ⁻³ | There are no exceedances of the critical level greater than 25 m from the roadside at any modelled transects. |
| Nitrogen deposition | 10 kgN/ha/yr | 14.2 kgN/ha/yr | Minimum critical load is exceeded across Ashdown Forest due to high background nitrogen deposition rates. The increase in nitrogen deposition as a result of MSDC site allocations are not greater than 1 % of critical load at modelled transects. |
| Acid deposition | 0.499 keq N/ha/yr | 1.01 keq N/ha/yr | Minimum critical load is exceeded across Ashdown Forest due to high background acid deposition rates. The increase in acid deposition as a result of MSDC site allocations are not greater than 1 % of critical load function at modelled transects. |

Note: * Background concentrations of NO_x vary dependent on transect location, so a range is provided in Table i.

The assessment concluded that the relevant air quality criteria are being breached as a result of road traffic associated with the MSDC site allocations and therefore assessment by a qualified ecologist is required to determine the potential for this representing a significant risk to sensitive species at Ashdown Forest.

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1. Introduction

Wood Environment and Infrastructure Solutions Ltd. ('Wood') has undertaken an air quality assessment on behalf of Mid Sussex District Council (MSDC) to inform the preparation of the MSDC Site Allocations Development Plan Document (DPD). This report will be used to inform a Habitats Regulations Assessment (HRA) undertaken by Footprint Ecology to determine the potential risk to species and habitats at designated protected wildlife sites.

Site allocations for the MSDC Site Allocations DPD have been agreed at 876 dwellings per annum (dpa) up to 2023/ 2024, and 1090 dpa to 2031 thereafter subject to further Habitats Regulations Assessment work.

Transport modelling was carried out for nine different site allocation scenarios in total, including both housing and employment potential allocations. However, as a result of the Transport Assessment and other evidence, only Scenarios 4, 7 and 8 were brought forward as potential site allocation options to be considered in terms of impact to air quality at Ashdown Forest. These three scenarios represented the most realistic and deliverable mix of potential site allocations to be considered further in the site selection process. All other scenarios were developed for internal use to test the transport model and were not taken forward. The Scenarios previously modelled for air quality are as follows:

- Scenario 4 comprised 32 housing sites, plus a large site at Haywards Heath Golf Course (33 sites in total)¹.
- Scenario 7 comprised 26 housing constant sites, plus a large site at Haywards Heath Golf Course (27 sites in total)².
- Scenario 8 comprised 26 housing constant sites, plus four sites at Folders Lane, Burgess Hill (30 sites in total)².

More detailed information on the MSDC site allocation scenarios modelled are provided in the Transport Assessment³. Scenarios 7 and 8 relate to the refined options developed by MSDC as informed by a comprehensive site selection process and considered factors relating to sustainability, transport, air quality and Habitats Regulations Assessment. These scenarios were taken forward to the Regulation 18 consultation that was undertaken in autumn 2019.

Since the Regulation 18 consultation, a more refined Sites DPD Scenario has been developed and traffic data provided by Transport Consultants, Systra, and the site allocations and mitigation associated with this scenario has been considered in terms of the impact to air quality at Ashdown Forest Special Area of Conservation (SAC), Special Protection Area (SPA) and Site of Special Scientific Interest (SSSI). Additionally, consideration has been made of the potential in-combination impact of the MSDC local plan and other local plans for neighbouring councils.

The Sites DPD Scenario comprised 22 housing sites, all of which are included in Scenario 8; some of the site yields have been adjusted following further evidence testing.

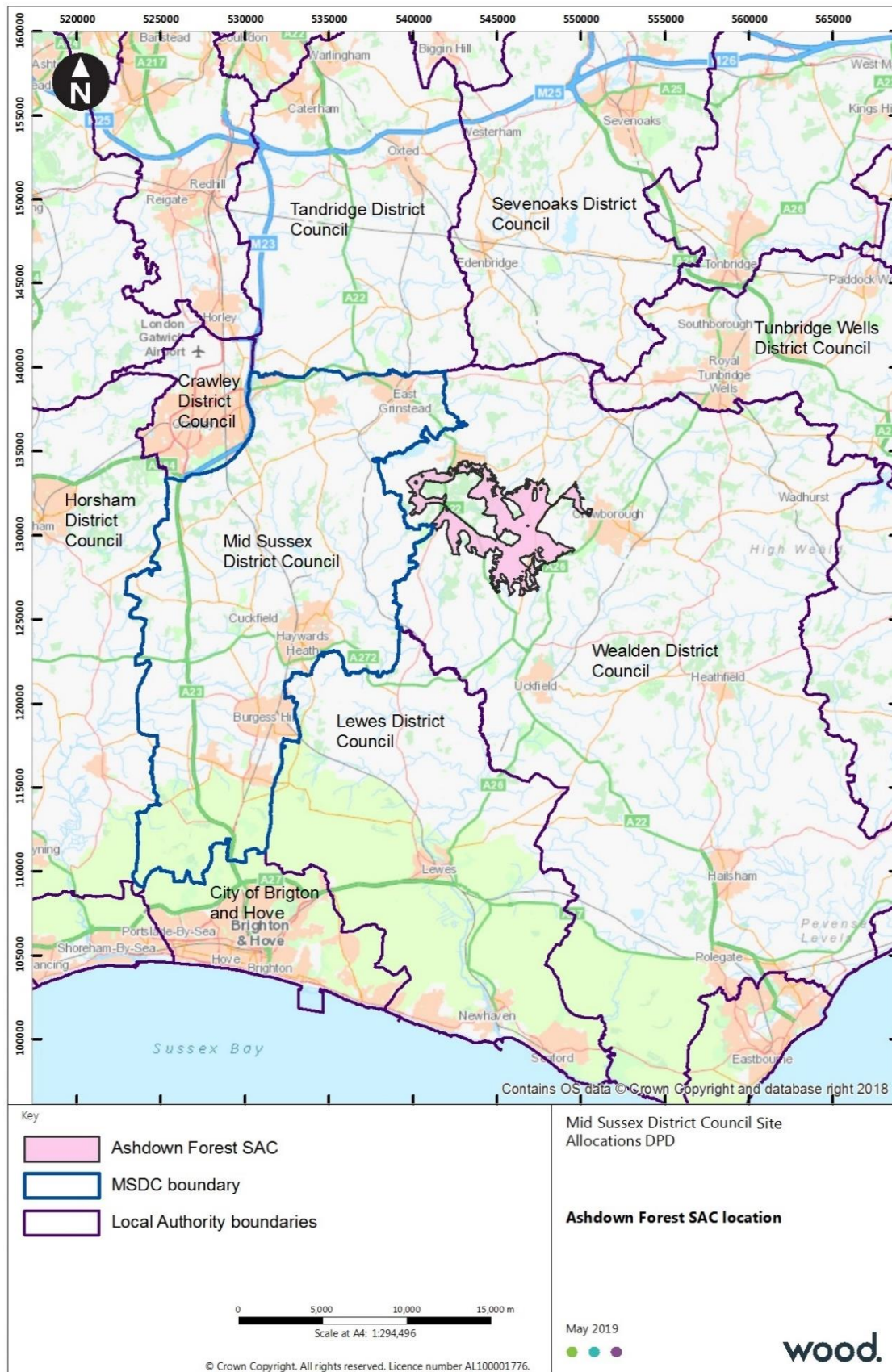
Figure 1.1 shows the location of Ashdown Forest in relation to the MSDC boundary and the surrounding local authorities.

¹ Wood (2019) Air quality modelling to inform Mid Sussex District Council Site Allocations Development Plan Document – Scenario 4 Results.

² Wood (2019) Air quality modelling to inform Mid Sussex District Council Site Allocations Development Plan Document – Scenario 7 & 8 Results.

³ Systra (2019) Mid Sussex Transport Study.

Figure 1.1 Ashdown Forest location



2. Relevant legislation, policies and guidance

2.1 Legislation and policy

National Planning Policy Framework

The National Planning Policy Framework (NPPF)⁴ outlines the Government's planning policies for England and how these should be applied when developing a locally prepared plan for housing. It is determined that planning policies should:

"sustain compliance with and contribute towards EU limits values or national objectives for pollutants..."

Paragraph 177 relates to the impact of development on sensitive ecological sites and states:

"The presumption in favour of sustainable development does not apply where the plan or project is likely to have significant effect on a habitats site (either alone or in combination with other plans or projects), unless an appropriate assessment has concluded that the plan or project will not adversely affect the integrity of the habitats site."

Conservation of Habitats and Species Regulations

The Conservation of Species and Habitats Regulations⁵ came into force in November 2017, consolidating the Conservation of Habitats and Species Regulations 2010 with subsequent amendments. The Regulations provide the designation for European sites and place responsibility on the UK government to ensure conservation of such sites. The Regulations require appropriate assessment of potentially damaging operations, which includes residential development, to show that there will be no adverse effect on the integrity of the site before planning consent will be granted.

Air Quality Standards, Objectives and Critical Loads

The concept of critical levels and critical loads were introduced by the United Nations Economic Commission for Europe Convention on Long-range Transboundary Air Pollution (CLRTAP). Critical levels relate to pollutant concentrations above which direct adverse effects on receptors may occur, whereas critical loads relate to potential effects of deposition.

The legislative framework for air quality consists of legally enforceable EU Limit Values that are transposed into UK legislation as Air Quality Standards (AQs) that must be at least as challenging as the EU Limit Values set by the European directive on air quality (2008/50/EC). These are concentrations recorded over a given time period, which are considered to be acceptable in terms of what is scientifically known about the effects of each pollutant on health and on the environment. Action in the UK is then driven by the UK's Air Quality Strategy⁶ that sets out how UK Government will comply with UK Air Quality Standards with the support of action by local authorities and the devolved administrations to meet Air Quality Objectives (AQOs).

AQOs relating to concentrations of oxides of nitrogen (NO_x), above which there is an increased risk of damage to ecological receptors, which can include growth effects, physiological effects and biochemical effects, would be considered to assess impacts upon the Ashdown Forest SAC.

⁴ Department for Communities and Local Government (2019) National Planning Policy Framework

⁵ Conservation of Species and Habitats Regulations (2017) Available from:
<https://www.legislation.gov.uk/uksi/2017/1012/part/1/made?view=plain>

⁶ Defra in partnership with the Scottish Executive, Welsh Assembly Government and Department of the Environment Northern Ireland (2007) The Air Quality Strategy for England, Scotland, Wales and Northern Ireland.

It should be noted that critical loads are not statutory standards which are to be achieved but are an indicator of when harmful effects can occur for different habitat types.

Critical levels and critical loads used in this assessment are discussed in more detail in Section 4.1.

2.2 Guidance

Environment Agency Guidance

The Environment Agency's Horizontal Guidance Note H1⁷ provides methods for quantifying the environmental impacts of emissions to all media. It should be noted that this methodology was withdrawn in February 2016 however is still widely used alongside other resources. The H1 Assessment Guidance was replaced by the Environment Agency's Air Emission Risk Assessment for your Environmental Permit⁸, which contains long and short-term Environmental Assessment Levels (EALs) and Environmental Quality Standards (EQS) for releases to air derived from a number of published UK and international sources. These EALs and EQS will be used as "standards" for the evaluation of the pollutants considered in this study.

Design Manual for Roads and Bridges (DMRB)

The DMRB guidance⁹ states that internationally designated biodiversity sites (SPAs, SACs and Ramsar sites) and SSSIs within 200 m of an affected route or corridor, where there is expected to be an increase > 1,000 annual average daily traffic movements (AADT), need to be considered within an assessment. Beyond 200 m from the roadside, atmospheric concentrations are likely to be at background concentrations due to sufficient dispersion of traffic emissions.

Wealden District Council High Court Judgement¹⁰

This case concerned the importance of taking into consideration the in-combination and cumulative effect of proposed developments when assessing the air quality impacts on ecologically sensitive areas, specifically European designated sites. Prior to the high court judgement, the DMRB threshold of an increase in road traffic flow of more than 1,000 AADT was used to scope out air quality assessments. This case concerned the cumulative impact of Local Plans produced by multiple councils impacting Ashdown Forest SAC. The Joint Core Strategy (JCS) prepared by Lewes District Council and South Downs National Park Authority, scoped out an air quality assessment as the AADT increase for the JCS was below 1,000. However, the Judge determined that, whilst the DMRB threshold was relevant to determine potential air quality impacts, the land allocations included in the JCS would impact the Ashdown Forest SAC and, when considered in combination with the increased traffic associated with allocations in the Wealden District Council (WDC) Core Strategy, the threshold would be breached.

This case set a precedent whereby the cumulative impact of proposed developments should be assessed when there is the possibility of affecting ecologically sensitive sites. This has been demonstrated through subsequent court cases whereby planning permission has not been granted or allowed by appeal. Consequently, in March 2017, a judge quashed Policies SP1 and SP2 in the JCS due to the potential for increased nitrogen deposition adversely impacting Ashdown Forest SAC. This reduced the number of proposed residences in the JCS by 1,177 homes¹¹.

⁷ Environment Agency (2011) Horizontal Guidance Note H1.

⁸ <https://www.gov.uk/guidance/air-emissions-risk-assessment-for-your-environmental-permit>

⁹ Highways England (2007) Design Manual for Roads and Bridges (Volume 11, Section 3).

¹⁰ The Planning Inspectorate (2015) Appeal decision

¹¹ <http://www.bailii.org/ew/cases/EWHC/Admin/2017/351.html>

As a consequence of this decision, it is important that local authorities thoroughly consider the cumulative effects upon air quality of traffic associated with multiple developments. This is an on-going situation and currently there are no guidelines as to the spatial extent of an air quality assessment as part of an HRA.

Wealden District Council Local Plan Examination

The Inspector's response to the submission of the WDC Local Plan was published on 20th December 2019 recommending the withdrawal of the WDC Local Plan. In relation to HRA, the letter reiterates the importance of engagement with neighbouring authorities and Natural England throughout the process. In terms of the air quality assessment evidence base for the HRA, the Inspector deemed the methodology inappropriate as the projected baseline scenario assumed no improvement in vehicle emissions (either through improvements in technology or increased numbers of electric vehicles) from the present day, which is considered to be unreasonable and lacking in scientific credibility. Reference was made to the requirement to consider advice provided in the Institute of Air Quality Management (IAQM) non-statutory guidance¹⁴ released in June 2019.

Institute of Air Quality Management (IAQM) position statement

IAQM published a statement¹² in 2016 about the use of the 1% criterion¹³ in Habitats Regulations Assessments to determine in which circumstances air quality impacts are too small and have insignificant effects on the integrity of a designated site. Above the 1% criterion should be an indication that there may be potential for a significant effect, but this will require evaluation by a qualified ecologist and is dependent on the circumstances of the habitat. Critical levels and critical loads used in this assessment can be seen in Table 4.1.

A guide to the assessment of air quality impacts on designated nature conservation sites

IAQM released a guidance document¹⁴ in June 2019 with the aim of providing some clarity on carrying out air quality assessments on impacts to designated sites. This guidance discusses the policy and legal background underpinning the proposed methodology, including the impact of the Wealden Judgement. It outlines the way in which air quality consultants and ecologists should work together, highlighting the responsibilities of each when carrying out Habitats Regulations Assessments.

Whilst the new IAQM guidance is acknowledged as best practice, methodology for this air quality assessment was agreed prior to the release of the IAQM guidance. The original approach to this assessment is broadly consistent with IAQM guidance and has been reconfirmed with Natural England. It is acknowledged that the way in which assessment of in-combination impacts is carried out has been clarified by the release of the IAQM guidance, therefore this methodology has been included in Appendix F. This includes consideration of the difference between the future 'no-growth' scenario and the 'Do-Something' scenario taking account of additional traffic flows associated with MSDC local plan and surrounding local authorities' plans and projects.

¹² IAQM (2016) Use of Criterion for the Determination of an Insignificant Effect of Air Quality Impacts on Sensitive Habitats, January 2016.

¹³ Environment Agency (2011) H1 Annex F – Air emissions.

¹⁴ IAQM (2019) A guide to the assessment of air quality impacts on designated nature conservation sites.

3. Scope of the assessment

3.1 Sensitive species in Ashdown Forest

Ashdown Forest has been given the European designation of an SPA and SAC, as well as the UK designation of SSSI. Ashdown Forest is adjacent to Mid Sussex District, located between East Grinstead and Crowborough, so is likely to be impacted by emissions from vehicles travelling to or from Mid Sussex District. Habitats and species of interest at Ashdown Forest include¹⁵:

- Northern Atlantic Wet Heaths and *Erica Tetralix* (Cross-leaved heath);
- European dry heaths;
- *Triturus cristatus* (Great Crested Newt);
- *Caprimulgus europaeus* (European nightjar) (due to impact to breeding habitat); and
- *Sylvia undata* (Dartford warbler) (due to impact to breeding habitat).

Modelled transects

The focus of this air quality assessment is the potential impact of road traffic emissions on the Ashdown Forest SAC. As guidance states that ecological receptors may be affected by traffic emissions up to a distance of 200 m from the road, a series of perpendicular transects have been used to model concentrations across this area. Transect locations were selected through consultation with Footprint Ecology, who used a habitat map (Figure 3.1) to create the map included in Figure 3.2 categorising road segments by the area of Annex I habitats, defined by the Habitats Directive as habitats of European interest¹⁶. Any roads with Annex I area of greater than 100 m² per 1 m of road were selected for a transect. This approach was discussed and agreed with Natural England. Additionally, advice from Natural England to Footprint Ecology stated that the main roads of concern were the A22 and A26. Receptor points were included at 0 m, 2 m, 5 m, 10 m, 25 m, 50 m, 100 m, 150 m and 200 m from the roadside. Transect points were modelled to the SAC boundary only, which in some cases did not extend to 200 m from the roadside, for example Transect T2 where the SAC boundary is 180 m from the roadside. Transect points were modelled at ground level.

3.2 In-combination assessment

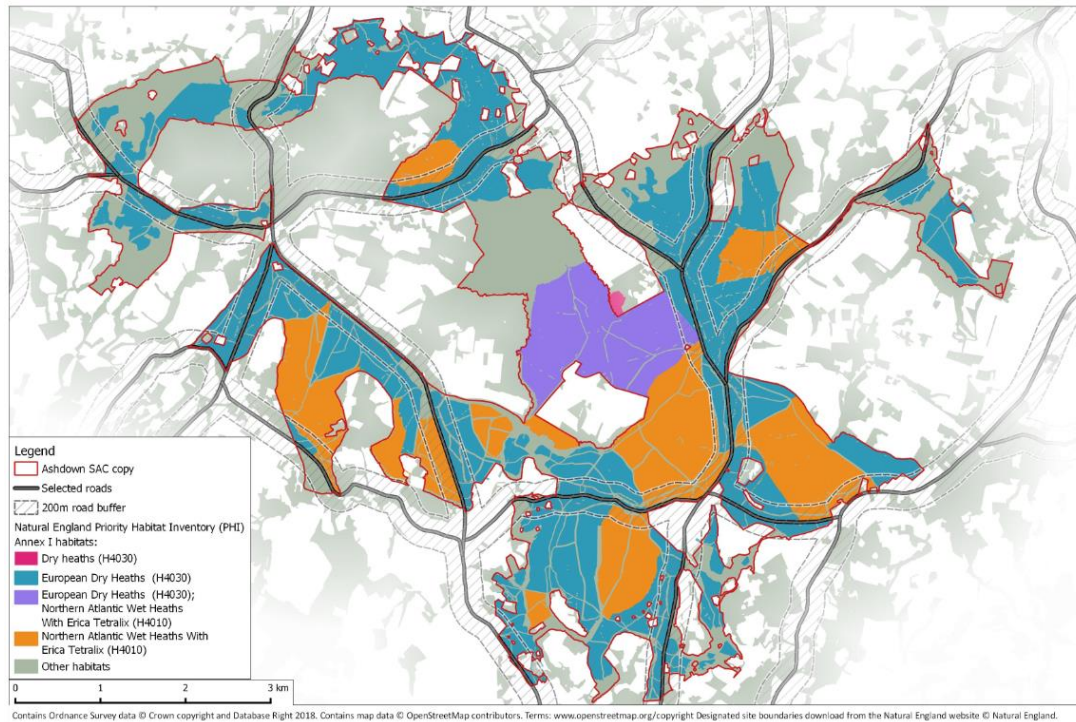
In line with the outcome of the Wealden Judgement, the in-combination impact to air quality at Ashdown Forest has been considered. Traffic data provided by Systra and used in this assessment include flows from adjoining councils' development policies.

The IAQM guidance acknowledges that in order to consider the in-combination impact of a specific project or plan alongside other local authority projects in terms of nitrogen and acid deposition, assumptions must be made as it is unlikely that traffic data for a future 'no growth' scenario will be provided. In this instance, IAQM suggest using baseline traffic flows with future emission factors (referred to as Scenario A in this assessment) in order to calculate the in-combination process contribution (PC). The in-combination assessment of nitrogen and acid deposition can be seen in Appendix F.

Transect locations are shown on Figure 3.3, and additional details of modelled transect points are provided in Appendix B.

¹⁵ <http://www.apis.ac.uk/>

¹⁶ European Commission DG Environment (2013) Interpretation Manual of European Union Habitats.

Figure 3.1 Habitats map for Ashdown Forest¹⁷Figure 3.2 Roads with the greatest area of Annex 1 species within 200 m¹⁸

Map 6: Road segments categorised by the area of Annex I (m2) per m of road.

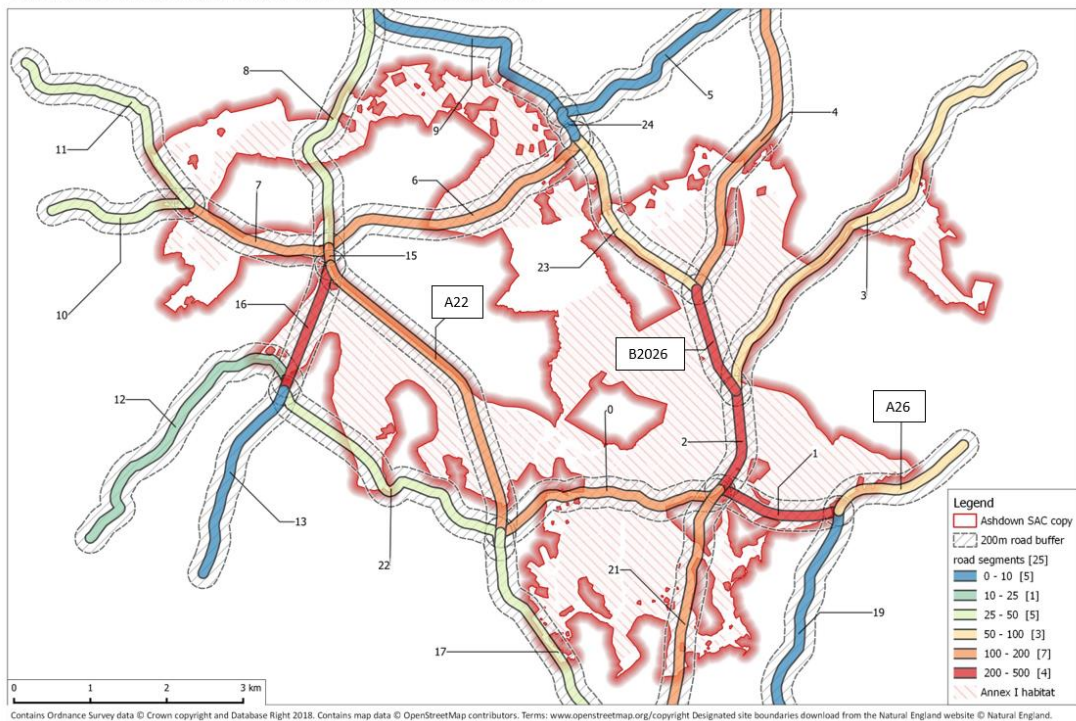
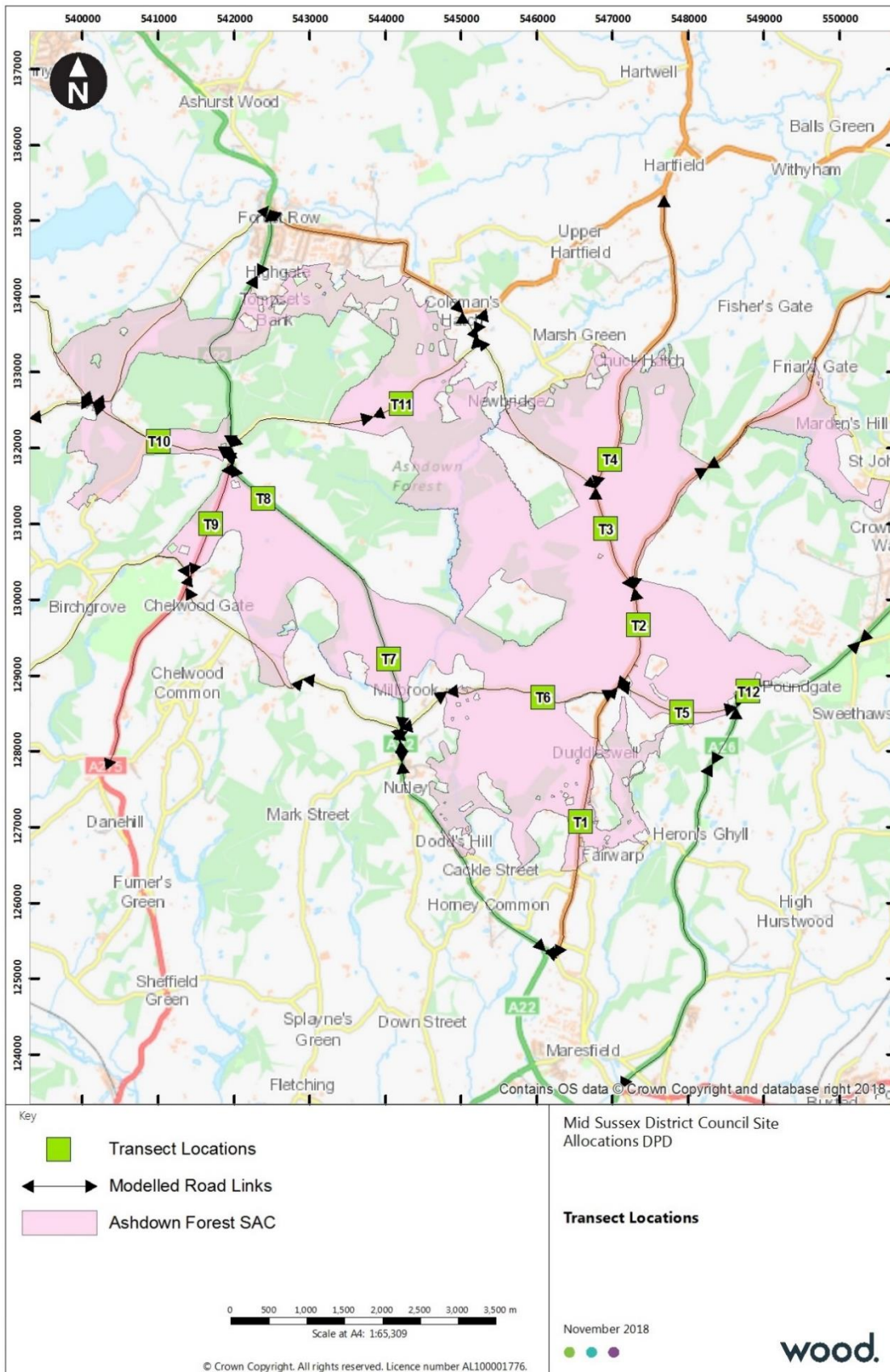
¹⁷ Footprint Ecology (2019) Habitats map for Ashdown Forest.¹⁸ Footprint Ecology (2018) Roads with the greatest area of Annex 1 species within 200 m

Figure 3.3 Transect locations



4. Assessment methodology

4.1 Assessment criteria

Table 4.1 shows the air quality standards, objectives, environmental assessment levels, targets, critical loads and levels relevant to this assessment.

Table 4.1 Summary of relevant assessment criteria

| Pollutant | Air Quality standards (AQS)/ Environmental Assessment Level (EAL)/Target | Objective (UK) | Averaging Period |
|-------------------------------------|--|--|------------------|
| NO_x | AQS | 30 $\mu\text{g m}^{-3}$ | Annual Mean |
| | AQS | 200 $\mu\text{g m}^{-3}$ | Daily Mean |
| | EAL* | 75 $\mu\text{g m}^{-3}$ | Daily Mean |
| NH₃ | Target | 1 $\mu\text{g m}^{-3}$ where lichens or bryophytes (including mosses, landworts and hornworts) are present, where not present 3 $\mu\text{g m}^{-3}$ | Annual Mean |
| Nutrient Nitrogen deposition | Target | 10 – 20 kg N/ ha/ yr for European dry heaths as present in Ashdown Forest | Annual Mean |
| Acidity deposition | Target | MinCLminN:0.499 – MaxCLminN:0.714 for European dry heaths as present in Ashdown Forest | Annual mean |

Notes: * WHO report¹⁹ states that where SO₂ and O₃ are not present at their respective limits, a 200 $\mu\text{g m}^{-3}$ daily mean would be more appropriate.

In addition to NO_x concentrations and nitrogen deposition, ammonia (NH₃) has been calculated. This is not included in the DMRB assessment methodology for road-traffic emissions requiring assessment, but, due to recent developments in the Wealden judgement²⁰ and research that has shown relatively low concentrations of ammonia are harmful to vegetation, it has been modelled in this assessment for completeness. Modelled concentrations of ammonia have been assessed against 1 $\mu\text{g m}^{-3}$ as lichens or bryophytes, including mosses, landworts and hornworts, are present.

The Air Pollution Information Service (APIS) database²¹ is a comprehensive source of information on air pollution and the effects on specific habitats and species. It provides background deposition data and critical loads and levels for deposition assessments. Unlike for the AQS and EAL values, critical loads differ depending on species sensitivity. Critical loads and background concentrations have been obtained from the APIS database under consultation with the ecologists for the project, Footprint Ecology.

In addition, this assessment will determine increments (difference between Do Minimum and Do Something scenarios) of acid and nitrogen deposition. In Environment Agency permitting, an increment of less than 1%

¹⁹ World Health Organisation (WHO) regional Office for Europe (2000) Air Quality Guidelines – Second edition (Chapter 11).

²⁰ The South Downs National Park Authority (2018) Ashdown Forest Statement of Common Ground.

²¹ <http://www.apis.ac.uk/src1>

of the site-specific critical load is considered to be inconsequential. This indicative threshold has been used to define a negligible impact and insignificant effect.

4.2 Dispersion modelling methodology

The dispersion model

ADMS-Roads (v4.1) had been used to predict annual mean and daily mean concentrations of NO_x at modelled receptor locations within Ashdown Forest. Full details of the ADMS-Roads model used are provided in Appendix C.

Annual mean concentrations of nitrogen dioxide (NO₂) were derived from the model-predicted NO_x concentrations, through application of the NO_x to NO₂ conversion tool version 7.1 developed for LAQM purposes²².

The modelling assessment requires source, emissions, meteorological and other site-specific data. For modelling traffic impacts, one year of hourly sequential meteorological data is used and model verification is carried out following Defra guidance²³.

Model Scenarios

The modelled scenarios include:

- Model verification using 2015 background concentrations, emissions factors, monitoring data from a 2014 to 2016 diffusion tube campaign, and traffic flows from 2017 (which is the year in which the traffic counts were carried out and the baseline traffic model is validated for);
- 2017 Baseline using 2017 background concentrations, emissions factors and traffic flows;
- Scenario A – 2031 Projected Baseline using 2017 background concentrations and traffic flows, with 2030 emission factors;
- Scenario B – Do Minimum (2031 Baseline + in-combination) using 2017 background concentrations, 2030 emission factors and predicted traffic flows; and
- Scenario C – Do Something (2031 Baseline + in-combination + MSDC impact) using 2017 background concentrations, 2030 emissions factors and predicted traffic flows.

It should be noted that Scenario A is included for reference only as it represents an impossible 'no-growth' scenario whereby there is no traffic growth between 2017 and 2031, but is included to demonstrate the impact of improving emission factors in the future. In line with IAQM guidance, in Appendix F Scenario A has been used to calculate the in-combination process contribution for nitrogen and acid deposition.

Meteorology

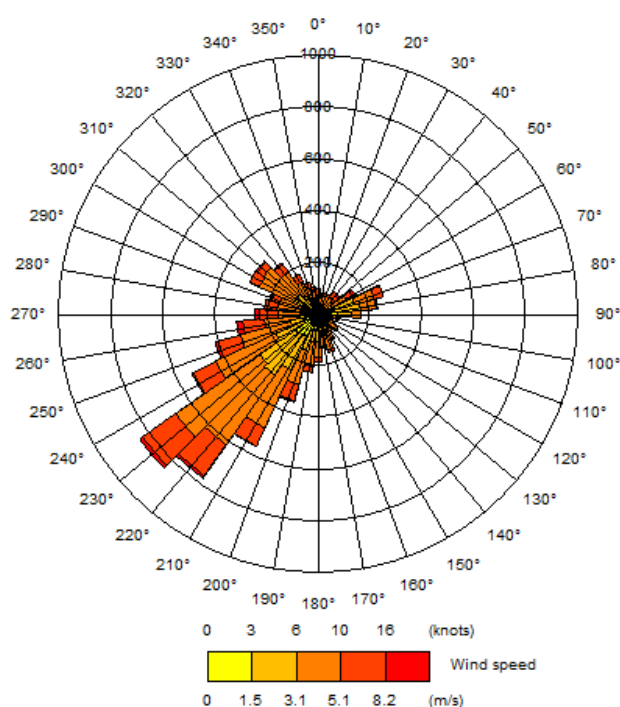
Detailed dispersion modelling requires hourly sequential meteorological data from a representative synoptic observing station. Hourly sequential meteorological data was obtained for the year 2017 using observations at Gatwick Airport, which is considered to provide representative data for the area of interest.

Figure 4.1 summarises the hourly wind speed and direction for the meteorological data used in this assessment.

²² AEA Technology (2019). *NO_x to NO₂ Calculator version 7.1*. <http://laqm.defra.gov.uk/review-and-assessment/tools/background-maps.html#NOxNO2calc>

²³ Defra (2016) Local Air Quality Management Technical Guidance (LAQM.TG(16)).

Figure 4.1 Windrose for Gatwick Airport (2017)



Surface roughness

Surface roughness is determined based on land use within the assessment area and at the appropriate weather station. For this assessment, a surface roughness of 0.5 m was selected for the assessment area and a surface roughness of 0.2 m was used for Gatwick Airport Weather Station²⁴.

Traffic data

Transport Consultants, Systra, developed the Mid Sussex Strategic Highway Model (MSSHM) in accordance with Department for Transport (DfT) transport analysis guidance (TAG). The modelling has been undertaken in collaboration with West Sussex County Council (WSCC) and Highways England (HE) and is considered to be suitable for the purposes of the Transport Study, and for providing inputs to wider work including air quality modelling. AADT flows for 2031 were based on traffic counts undertaken in 2017 (Baseline year) outlined in the model validation report²⁵ and Mid Sussex Transport Study²⁶. Traffic data for modelled links are provided in Appendix C.

Background concentrations

Defra has made estimates of background NO_x and NO₂ concentrations on a 1 km² grid for the UK for a base year of 2017 and provides projections for years 2017 to 2030 inclusive²⁷. Interpolation was carried out using ArcGIS to provide a better representation of background concentration at each transect point.

Table 4.2 shows the estimated background concentrations of NO_x for 2017 for the transects modelled.

²⁴ Gatwick Airport (2014) A Second Runway for Gatwick.

²⁵ Systra (2018) Local Model Validation Report – Mid Sussex Strategic Highway Model - Draft.

²⁶ Systra (2020) Mid Sussex Transport Study.

²⁷ <https://uk-air.defra.gov.uk/data/laqm-background-home>

Table 4.2 Defra mapped interpolated background annual mean NO_x concentrations (µgm⁻³) for 2017

| Transect | NO _x concentrations (µgm ⁻³) |
|----------|---|
| T1 | 10.6 |
| T2 | 10.1 |
| T3 | 10.1 |
| T4 | 10.1 |
| T5 | 10.3 |
| T6 | 10.2 |
| T7 | 10.6 |
| T8 | 11.2 |
| T9 | 11.3 |
| T10 | 11.4 |
| T11 | 10.6 |
| T12 | 10.4 |

Due to uncertainty in future predicted concentrations, background concentrations for 2017 will be used in all modelled scenarios as a conservative approach.

In line with LAQM.TG(16), the background NO_x concentration has been doubled to calculate the daily mean concentrations at all modelled receptor points as a conservative approach.

In addition, a background concentration specific to Ashdown Forest was obtained from the APIS website for NH₃ of 0.76 µgm⁻³. There has been very little research on future background concentrations of NH₃, therefore the same background concentration has been used for all scenarios, including future scenarios. Monitoring undertaken on behalf of Wealden District Council at background locations recorded a concentration of 0.6 µgm⁻³. For this assessment, the decision was taken to use the APIS concentration to remain consistent with the conservative approach adopted throughout.

The APIS resource was also used to determine deposition rates for both nitrogen and acid for Ashdown Forest. DMRB methodology suggests that to account for the decrease in deposition rates in future years, a reduction of 2% per year could be applied. Again, for this assessment, the decision was taken to use the APIS data to remain consistent with the conservative approach adopted throughout. Note: this does not follow the methodology whereby deposition rates will be reduced by 2% to the mid-assessment year outlined in the Statement of Common Ground²⁸ produced by the Sussex, Surrey and Kent Councils, in which MSDC reserved judgement on this issue.

Table 4.3 shows the deposition rates used in this assessment.

²⁸ The South Downs National Park Authority (2018) Ashdown Forest Statement of Common Ground.

Table 4.3 Nitrogen and acid deposition rates for all scenarios

| Deposition | 2017 deposition rate |
|-----------------|----------------------|
| Nitrogen | 14.20 kg N/ ha/year |
| Acid | 1.01 keq/ ha/ year |

Model verification

Model verification is a process by which modelled concentrations of air pollutants from road traffic emissions are adjusted based on actual measurement data. It enables an estimation of uncertainty and systematic errors associated with the dispersion modelling components of the air quality assessment to be considered. There are many explanations for these errors, which may stem from uncertainty in the modelled number of vehicles, speeds and vehicle fleet composition, as well as uncertainty associated with the emission factors. Defra has provided guidance in terms of preferred methods for undertaking dispersion model verification in LAQM.TG(16). Model verification involves the comparison of modelled concentrations and local monitoring data.

Full details of the model verification procedure are provided in Appendix D. In summary, the verification process led to the use of a modelled Road-NO_x adjustment factor of 1.626.

4.3 Pollutant Calculations

Oxides of nitrogen (NO_x)

The Calculator Using Realistic Emissions for Diesels²⁹ (CURED V3A) was used to predict emissions to import into ADMS-Roads. This tool was originally developed to overcome the disparity between future emissions factors predicted using Defra's Emissions Factor Toolkit (EFT) and real-world emissions testing and is considered to be a more conservative approach. In addition, the use of the CURED tool was accepted as appropriate by the Inspector for the Wealden Local plan¹⁰.

Road-NO_x concentrations were adjusted using the above factor.

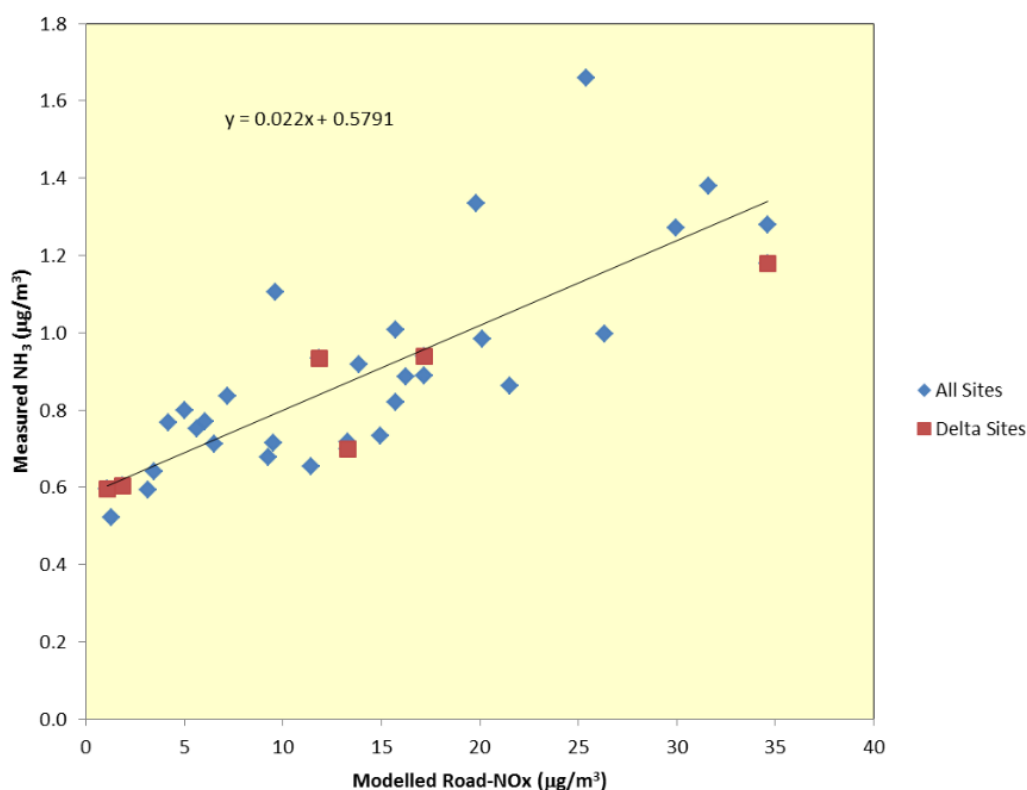
Defra's NO_x to NO₂ calculator³⁰ was then used to convert predicted concentrations of road-NO_x to road-NO₂ concentrations for use in calculating nitrogen deposition.

Ammonia (NH₃)

The requirement to assess the impact of NH₃ is relatively new, so there is no established reference method available. The decision was made to use a factor to convert concentrations of NO_x to NH₃, rather than modelling, especially due to the fact that it would not have been possible to undertake model verification due to the precise location of NH₃ monitors being redacted in the report prepared for Wealden District Council. This is considered to be a robust approach, as the factors affecting NO_x concentration, such as increase in vehicles, vehicle type and speed, also affect concentrations of NH₃. This relationship was demonstrated in the report prepared for Wealden District Council in plotting modelled road-NO_x against monitored concentrations of NH₃, as shown in Figure 4.2.

²⁹ Air Quality Consultants (2018) Calculator Using Realistic Emissions for Diesels (CURED V3A)
<http://www.aqconsultants.co.uk/News/January-2018/UPDATED-CURED-TO-V3A.aspx>

³⁰ <https://laqm.defra.gov.uk/review-and-assessment/tools/background-maps.html#NOxNO2calc>

Figure 4.2 Modelled Road-NO_x vs. Monitored NH₃ concentration³¹

Therefore, this assessment has used the factor 0.022 (i.e., 0.022 g of NH₃ to every 1 g of NO_x emitted) to calculate predicted road-NH₃ from adjusted road-NO_x concentrations in line with the methodology used by AQC and is considered to be a conservative approach.

A sensitivity test has also been carried out, details of which are included in Appendix G, using a factor calculated from the National Atmospheric Emissions Inventory³² (NAEI) of 0.007 (i.e., 0.007 g/km of NH₃ to 1 g/km of NO_x emitted).

Nitrogen deposition

To calculate nitrogen deposition the AQTAG³³ methodology was used as an alternative to the Design Manual for Roads and Bridges (DMRB) methodology as it allows for calculation of nitrogen deposition from ammonia.

Dry deposition flux was calculated for the NO₂ and NH₃ annual mean concentrations at each modelled receptor using the dry deposition velocities in Table 4.4. As there are a number of species present in Ashdown Forest, the dry deposition velocities for 'forest' area were selected as a conservative approach under direction of Footprint Ecology.

³¹ Air Quality Consultants (2018) Ashdown Forest SAC – Air Quality Monitoring and Modelling.

³² <http://naei.beis.gov.uk/data/>

³³ Air Quality Technical Advisory Group (AQTAG06) (2014) Technical guidance on detailed modelling approach for an appropriate assessment for emissions to air.

Table 4.4 Dry deposition velocities

| Pollutant | Area | Dry deposition velocity (m s ⁻¹) |
|-----------------|--------|--|
| NO ₂ | Forest | 0.003 |
| NH ₃ | Forest | 0.03 |

Dry deposition flux was then converted to kilograms of nitrogen per hectare per year (kg N ha⁻¹ yr⁻¹) deposition for both NO_x and NH₃ using the conversion factors shown in Table 4.5.

Table 4.5 Conversion factors: dry deposition flux to kilograms of nitrogen per hectare per year deposited

| Pollutant | Conversion factor |
|-----------------|-------------------|
| NO ₂ | 96 |
| NH ₃ | 259.7 |

Nitrogen deposition rates from both NO₂ and NH₃ were added together with the background nitrogen deposition rate to give total nitrogen deposition at all modelled transect points.

Acid deposition

Nitrogen and sulphur deposition both contribute to acid deposition and the Critical Load Function Tool provided by APIS³⁴ is used to determine the deposition that will not cause harmful effects. Dry deposition is the portion of total deposition that is deposited through processes such as settling, impaction and adsorption and is quantified in terms of flux, which is dependent on the dry deposition velocity and concentration of a pollutant in the air (in this case predicted NO₂ and NH₃ from road emissions). The dry flux deposition is multiplied by a conversion factor of 0.071428 to calculate the kilo- equivalent of acid deposition. As above, deposition values were added together with the background acid deposition to determine total acid deposition at all modelled transect points. The change in deposition between Scenario B Do Minimum and Scenario C Do Something is used alongside the Critical Load Function Tool to calculate the change as a percentage of the critical load.

4.4 Limitations

The main limitation to carrying out this assessment has been understanding the current conditions with regard to air quality in Ashdown Forest. There has been an extensive air quality monitoring programme undertaken across the area on behalf of Wealden District Council, however data availability is restricted. This led to the use of 2-year period mean NO₂ concentrations being compared to model predicted annual mean concentrations for model verification.

In addition, it was not clear which monitoring stations were at background locations, therefore it was necessary to use Defra mapped predicted background concentrations. To improve accuracy, background concentrations were interpolated and extracted at each transect point.

³⁴ <http://www.apis.ac.uk/critical-load-function-tool>

5. Baseline air quality

MSDC does not currently carry out any monitoring as part of local air quality management duties in the vicinity of Ashdown Forest. Wealden District Council commissioned extensive monitoring across Ashdown Forest³⁵. The results of this monitoring were published in a report that has since been heavily redacted with only limited information being made available to the public. All monitored concentrations included in this section are based on information made publicly available by Wealden District Council.

5.1 Nitrogen dioxide

Continuous monitoring

An automatic monitor was installed at Kingstanding, the details of which are shown in Table 5.1.

Table 5.1 Automatic monitor location and results October 2014 – August 2016

| Monitor ID | X | Y | Distance from road (m) | Data capture (%) | Period mean concentration (μgm^{-3}) |
|------------|--------|--------|------------------------|------------------|---|
| A1 | 547294 | 129153 | 1.7 | 95 | 17.6 |

Passive monitoring

Diffusion tubes were deployed in triplicate at a number of locations throughout Ashdown Forest. Table 5.2 includes those tubes where location data is available and that are located in an area of sensitive habitat, as reported by Wealden District Council

Table 5.2 Diffusion tube locations and period mean concentration (October 2014 to August 2016)

| Monitor ID | X | Y | Distance from road (m) | Period mean concentration of NO_x (μgm^{-3}) | Period mean concentration of NO_2 (μgm^{-3}) |
|------------|--------|--------|------------------------|--|--|
| T1 | 542199 | 134088 | 1.5 | 37.3 | 21.7 |
| T2 | 542041 | 133770 | 2.1 | 21.6 | 13.9 |
| T3 | 541849 | 133049 | 1.6 | 50.9 | 27.9 |
| T4 | 541953 | 132229 | 1.7 | 45.8 | 25.6 |
| T6 | 546890 | 131049 | 3.7 | 18.9 | 12.5 |
| T15 | 547401 | 130703 | 1.3 | 18.5 | 11.4 |
| T19 | 549090 | 128879 | 2.6 | 48.5 | 27.3 |
| T20 | 548709 | 128701 | 1.2 | 39.2 | 22.9 |

³⁵ Air Quality Consultants (2018) Ashdown Forest SAC: Air quality monitoring and modelling – Volume 1 (Redacted)

| Monitor ID | X | Y | Distance from road (m) | Period mean concentration of NO _x (µgm ⁻³) | Period mean concentration of NO ₂ (µgm ⁻³) |
|------------|--------|--------|------------------------|---|---|
| T21 | 548892 | 128852 | 1.3 | 63.6 | 34.1 |
| T22 | 549140 | 128880 | 2.6 | 49.1 | 27.6 |
| T23 | 547885 | 128514 | 3.5 | 23.8 | 15.1 |
| T24 | 546788 | 127981 | 4.8 | 19.9 | 13.0 |
| T25 | 546665 | 127421 | 1.4 | 23.5 | 14.9 |
| T29 | 544600 | 127196 | 1.5 | 28.1 | 17.0 |
| T31 | 544020 | 129316 | 2.7 | 40.6 | 23.2 |
| T32 | 544010 | 129312 | 1.2 | 44.1 | 24.9 |
| T33 | 543978 | 129407 | 1.3 | 50.3 | 27.7 |
| T34 | 542302 | 131412 | 1.7 | 26.0 | 16.0 |
| T35 | 542861 | 130963 | 2.9 | 33.5 | 19.7 |
| T36 | 543617 | 130337 | 2.0 | 39.1 | 22.4 |
| T37 | 543887 | 129685 | 1.2 | 37.3 | 21.7 |
| T38 | 545412 | 128806 | 1.0 | 18.3 | 12.2 |
| T42 | 547353 | 129600 | 1.4 | 19.2 | 12.7 |
| T48 | 541856 | 131411 | 1.4 | 22.8 | 14.4 |
| T49 | 541722 | 131040 | 2.3 | 19.8 | 12.9 |

Notes: ***Bold** denotes exceedance of the 30 µgm⁻³ annual mean AQO.

AQC monitors and MSDC transect locations have a similar nomenclature but are not in the same locations.

Figure 5.1 shows the location of monitors included in this section. It can be seen that across the assessment area concentrations of NO_x are generally above the annual mean 30 µgm⁻³ AQO at diffusion tubes located either on the A22 or A26, which have been identified by Natural England as the areas of concern when considering impacts to sensitive habitats in Ashdown Forest.

Figure 5.1 AQC monitor locations



Note: All monitors deployed by AQC on behalf of Wealden District Council.

5.2 Ammonia

The monitoring undertaken on behalf of Wealden District Council included six DELTA monitors (Defra reference method) and 29 ALPHA monitoring sites (passive monitoring) in Ashdown Forest. The results for ALPHA passive monitoring have not been included in this assessment as all locations were redacted and it is not clear which sites were set up as a transect from the road side. Table 5.3 shows the location and monitored concentration for ammonia from the DELTA monitors.

Table 5.3 DELTA monitoring results for ammonia – period mean between 2014 and 2016

| Monitor ID | X | Y | Distance from road (m) | Data capture (%) | Period mean concentration (μgm^{-3}) |
|------------------|--------|--------|------------------------|------------------|---|
| R1.3 (D1) | * | * | 5 | 91 | 0.94 |
| T46 (D2) | 542172 | 133039 | 660 | 100 | 0.60 |
| A1 (D3) | 547294 | 129153 | 1.7 | 96 | 0.70 |
| T71 (D4) | 547438 | 128711 | 5.5 | 91 | 0.93 |
| T41 (D5) | * | * | 390 | 53 | 0.60 |
| R4.3 (D6) | * | * | 5 | 95 | 1.18 |

*Location redacted in AQC report²⁹

Bold denotes exceedance of the $1\mu\text{gm}^{-3}$ EAL

Table 5.3 shows that a background concentration of NH_3 was monitored at $0.6\mu\text{gm}^{-3}$ at two locations, however the location of one monitor has been redacted. At roadside locations, the concentration was between $0.7\mu\text{gm}^{-3}$ and $1.18\mu\text{gm}^{-3}$.

6. Results

Pollutant concentrations

Oxides of nitrogen

Predicted annual mean concentrations of NO_x are below the 30 µgm⁻³ AQO in both Scenario B-Do Minimum and Scenario C-Do Something at all modelled transect points at 10 m from the roadside up to 200 m. There are no exceedances predicted across Transects T3, T4, T5, T6 and T11 which are generally located on unclassified or B-roads. As expected, the highest concentrations are predicted at the locations with the greatest traffic flow, including A22, A26, A275 and Hindleap Lane. The highest predicted concentration is at transect point T12Wa (0 m from the kerb) at 55.9 µgm⁻³ in Scenario C-Do Something, which reduces to 26.5 µgm⁻³ at 10 m.

The greatest increase in annual mean concentrations between Scenario B-Do Minimum and Scenario C-Do Something is an increase of 0.22 µgm⁻³ at the roadside at Transect T6, located on Crowborough Road. This is less than 1 % of the 30 µgm⁻³ AQO. Due to rerouting of traffic, pollutant concentrations decrease in some locations. The greatest decrease in annual mean concentration of NO_x is predicted at T7 at 0.41 µgm⁻³ on the A22.

The daily mean AQO of 200 µgm⁻³, which is indicative of potential harm to some plant species, is not predicted to be breached at any of the modelled transects.

Ammonia

With reference to the APIS website, which provides a list of sensitive species specific to Ashdown Forest, predicted annual mean concentrations of ammonia have been compared to the 1 µgm⁻³ critical level due to the presence of lichens and bryophytes.

In Scenario C-Do Something, predicted annual mean concentrations of NH₃ exceed the critical level at up to 5 m from the roadside at Transects T1, T2, T3, T4, T5, T8 and T9, and further than 10 m, but less than 25 m, from the roadside at Transect T7, T10 and T12. There are no exceedances of the critical level at a distance greater than 25 m from the kerb.

The greatest NH₃ annual mean concentration is predicted at Transects T12 at 1.8 µgm⁻³ in both Scenario B-Do Minimum and Scenario C-Do Something.

Deposition

Nitrogen

The minimum critical load of 10 kg N/ ha/ yr, as available from the APIS resource and based on the sensitivity of the species in Ashdown Forest, has been used for comparison against predicted nitrogen deposition rates. The background deposition rate used in this assessment is 14.2 kg N/ha /yr and as a result nitrogen deposition exceeds this threshold at all transects and at all modelled points across the transect in both Scenario B-Do Minimum and Scenario C-Do Something. It should be noted that the baseline year background nitrogen deposition was used throughout as a conservative approach.

It can be seen that nitrogen deposition returns to near background levels between 150 m to 200 m from the roadside. The change in nitrogen deposition between Scenario B Do-minimum and Scenario C Do-Something is below the 1% threshold at all modelled transects, indicating that impacts are insignificant.

Acid

The critical load minimum and maximum range for acid deposition from nitrogen is between 0.499 – 0.952 keq N/ ha/ yr with reference to APIS, which is the most conservative critical load for acid deposition at Ashdown Forest. In Scenario B-Do Minimum and Scenario C – Do Something this threshold is exceeded at all transect points at all modelled transects, due to the background concentration of 1.01 keq N/ ha/ yr.

The greatest increase in acid deposition between Scenario B - Do minimum and Scenario C - Do Something is expected to be at the kerbside on Transect T6 on Crowborough Road with an increase of 0.006 keq N/ ha/ yr with the MSDC site allocation additional traffic; this is below 1% of the CL function.

Summary

A summary of results is provided in Table 6.1.

Table 6.1 Summary of results

| Pollutant | Assessment criteria | Background* | Results summary |
|----------------------------|-------------------------|--|--|
| Annual mean NOx | 30 μgm^{-3} | 10.04 μgm^{-3} to 11.36 μgm^{-3} | Predicted annual mean concentrations of NOx exceed the critical level up to 10 m from the roadside, but reduce to less than 30 μgm^{-3} beyond this. |
| Daily mean NOx | 200 μgm^{-3} | 20.08 μgm^{-3} to 22.73 μgm^{-3} | No exceedance across any modelled transects. |
| NH₃ | 1 μgm^{-3} | 0.76 μgm^{-3} | There are no exceedances of the critical level greater than 25 m from the roadside at any modelled transects. |
| Nitrogen deposition | 10 kgN/ha/yr | 14.2 kgN/ha/yr | Minimum critical load is exceeded across Ashdown Forest due to high background nitrogen deposition rates. The increase in nitrogen deposition as a result of MSDC site allocations are not greater than 1 % of critical load at modelled transects. |
| Acid deposition | 0.499 keq N/ha/yr | 1.01 keq N/ha/yr | Minimum critical load is exceeded across Ashdown Forest due to high background acid deposition rates. The increase in acid deposition as a result of MSDC site allocations are not greater than 1 % of critical load function at modelled transects. |

Note: * Background concentrations of NOx vary dependent on transect location as shown in Table 6.1.

7. Conclusions

Wood Environment and Infrastructure Solutions Ltd. (Wood) has prepared an air quality assessment on behalf of Mid Sussex District Council (MSDC) to inform a Habitats Regulations Assessment (HRA) for preparation of the MSDC Site Allocations Development Plan Document. This assessment is based on the Sites DPD Scenario site allocations and considers the potential risk to sensitive species and habitats at Ashdown Forest SAC, SPA and SSSI.

ADMS-Roads dispersion model has been used to model pollutants from traffic emissions at transects up to 200 m from the roadside throughout Ashdown Forest. Concentrations of NO_x and NH_3 were predicted without and with traffic flows associated with MSDC site allocations, including consideration of in-combination traffic flows from adjoining local authorities' development plans. It should be noted that a conservative approach has been adopted throughout, including the use of baseline year background concentrations and deposition rates, as well as the use of the strictest appropriate critical loads and levels.

The assessment methodology is in accordance with all available guidance and is robust. It has been discussed and agreed with Natural England.

Predicted annual mean concentrations of NO_x exceed the $30 \mu\text{g m}^{-3}$ AQO up to 10 m from the roadside on busier A-roads for the Sites DPD Scenario.

Daily mean concentrations of NO_x were below the $200 \mu\text{g m}^{-3}$ daily mean AQO at all locations.

Annual mean concentrations of NH_3 are predicted to exceed the $1 \mu\text{g m}^{-3}$ critical level indicating potential harm to sensitive species at a number of transects across Ashdown Forest, however at all transects the concentration reduces to within the critical level within 25 m of the roadside.

Predicted nitrogen deposition rates exceed the critical load due to high background deposition rates before the contribution of MSDC is considered. The change in deposition values associated with the MSDC site allocations traffic is below the 1% of critical load change indicating insignificant impacts to sensitive species and habitats at all transect points for the Sites DPD Scenario.

In terms of acid deposition, the background deposition rate also exceeds the minimum critical load for the Sites DPD Scenario. The change in acid deposition as a result of the MSDC site allocation traffic is below 1 % of the critical load function.

The assessment concluded that the relevant air quality criteria are being breached as a result of road traffic associated with the MSDC site allocations and therefore assessment by a qualified ecologist is required to determine the potential for this representing a significant risk to sensitive species at Ashdown Forest.

Appendix A

ADMS-Roads dispersion model

Introduction

The ADMS-Roads dispersion model, developed by CERC³⁶, is a tool for investigating air pollution problems due to small networks of roads that may be in combination with industrial sites, for instance small towns or rural road networks. It calculates pollutant concentrations over specified domains at high spatial resolution (street scale) and in a format suitable for direct comparison with a wide variety of air quality standards for the UK and other countries. The latest version of the model, version 4.1, was used in this study.

ADMS-Roads is referred to as an advanced Gaussian or, new generation, dispersion model as it incorporates the latest understanding of the boundary layer structure. It differs from old generation models such as ISC, R91 and CALINE in two main respects:

- It characterises the boundary layer structure and stability using the boundary layer depth and Monin-Obukhov length to calculate height-dependent wind speed and turbulence, rather than using the simpler Pasquill-Gifford stability category approach; and
- It uses a skewed-Gaussian vertical concentration profile in convective meteorological conditions to represent the effect of thermally generated turbulence.

Model features

A description of the science used in ADMS-Roads and the supporting technical references can be found in the model's User Guide³⁶. The main features of ADMS-Roads are:

- It is an advanced Gaussian, "new generation" dispersion model;
- Includes a meteorological pre-processor which calculates boundary layer parameters from a variety of input data e.g. wind speed, day, time, cloud cover and air temperature;
- Models the full range of source types encountered in urban areas including industrial sources (up to 3 point sources, up to 3 lines sources, up to 4 area sources, up to 25 volume sources) and road sources (up to 150 roads, each with 50 vertices);
- Generates output in terms of average concentrations for averaging times from 15minutes to 1 year, percentile values and exceedances of threshold values. Averages can be specified as rolling (running) averages or maximum daily values;
- The option to calculate emissions from traffic count data, speed and fleet split (light duty/ heavy duty vehicles) using UK emission factors. Alternatively, road emissions may be entered directly as user specified values;
- Models plume rise by solving the integral conservation equations for mass, momentum and heat;
- Models the effect of street canyons on concentrations within the canyon and vehicle-induced turbulence using a formulation based on the Danish OSPM model. It is usually only important to model street canyons when the aspect ratio (ratio of the height of buildings along the road to the width of the road) is greater than 0.5;
- Models the effects of noise barriers on concentrations outside the road;
- Models NO_x chemistry using the 8 reaction Generic Reaction Set plus transformation of SO₂ to sulphate particles, which are added to the PM₁₀ concentration;

³⁶ CERC (2011) ADMS-Roads, an Air Quality Management System, Version 3.1 User Guide, http://www.cerc.co.uk/environmental-software/assets/data/doc_userguides/CERC_ADMS-Roads3.1_User_Guide.pdf Date of access: 19th October 2012.

- Models the effect of a small number of buildings on dispersion from point sources;
- Models the effect of complex terrain (hills) and spatially varying surface roughness. Terrain effects only become noticeable for gradients greater than 1:10, but for ground level sources in a built up area, such as urban roads, low gradients will have a negligible effect;
- Models concentrations in units of $\text{ou}_{\text{m}}^{-3}$ for odour studies;
- Link to MapInfo and ArcGIS for input of source geometry, display of sources, aggregation of emissions and plotting of contours; and
- Link to an emissions inventory in Microsoft Access for input and export of source and emissions data.

In this study, street canyons, noise barriers, buildings and complex terrain were not modelled.

Validation

ADMS-Roads has been validated using UK and US data and has been compared with the DMRB spreadsheet model and the US model, CALINE. Validation of the ADMS and ADMS-Urban models are also applicable to the performance of ADMS-Roads as they test common features: basic dispersion, modelling of roads and street canyons, the effect of buildings and the effect of complex terrain. These validation studies are all reported on the CERC web site³⁷. In addition, ADMS-Urban has been validated during its use in modelling many urban areas in the UK for local authorities as part of LAQM, Heathrow Airport for the Department for Transport³⁸ and all of Greater London for a Defra model inter-comparison exercise³⁹.

³⁷ <http://www.cerc.co.uk/environmental-software/model-documentation.html#validation> Date of access: 19 October 2012

³⁸ CERC (2007) Air Quality Studies for Heathrow: Base Case, Segregated Mode, Mixed Mode and Third Runway Scenarios Modelled Using ADMS-Airport, prepared for the Department for Transport, HMSO Product code 78APD02904CERC

³⁹ Carslaw, D. (2011), Defra urban model evaluation analysis – Phase 1, a report to Defra and the Devolved Authorities. http://uk-air.defra.gov.uk/library/reports?report_id=654 Date of access: 19 October 2012

Appendix B

Modelled Transects

Table B.1 Modelled transect points

| Road ID | Transect point | Distance from kerb (m) | X | Y | Height (m) |
|---------|----------------|------------------------|--------|--------|------------|
| B2026 | T1Ea | 0 | 546585 | 127072 | 0 |
| | T1Wa | 0 | 546578 | 127073 | 0 |
| | T1Eb | 2 | 546587 | 127072 | 0 |
| | T1Wb | 2 | 546576 | 127074 | 0 |
| | T1Ec | 5 | 546590 | 127071 | 0 |
| | T1Wc | 5 | 546574 | 127075 | 0 |
| | T1Ed | 10 | 546595 | 127070 | 0 |
| | T1Wd | 10 | 546569 | 127076 | 0 |
| | T1Ee | 25 | 546609 | 127067 | 0 |
| | T1We | 25 | 546554 | 127079 | 0 |
| | T1Ef | 50 | 546634 | 127062 | 0 |
| | T1Wf | 50 | 546529 | 127084 | 0 |
| | T1Eg | 100 | 546683 | 127051 | 0 |
| | T1Wg | 100 | 546480 | 127094 | 0 |
| | T1Eh | 150 | 546731 | 127042 | 0 |
| | T1Wh | 150 | 546431 | 127105 | 0 |
| | T1Ei | 200 | 546780 | 127030 | 0 |
| | T1Wi | 180 | 546403 | 127108 | 0 |
| B2026 | T2Ea | 0 | 547345 | 129673 | 0 |
| | T2Wa | 0 | 547339 | 129672 | 0 |
| | T2Eb | 2 | 547347 | 129673 | 0 |
| | T2Wb | 2 | 547337 | 129672 | 0 |
| | T2Ec | 5 | 547350 | 129673 | 0 |
| | T2Wc | 5 | 547334 | 129672 | 0 |
| | T2Ed | 10 | 547355 | 129674 | 0 |
| | T2Wd | 10 | 547329 | 129671 | 0 |
| | T2Ee | 25 | 547370 | 129675 | 0 |
| | T2We | 25 | 547314 | 129670 | 0 |
| | T2Ef | 50 | 547395 | 129677 | 0 |

| Road ID | Transect point | Distance from kerb (m) | X | Y | Height (m) |
|--------------|----------------|------------------------|--------|--------|------------|
| | T2Wf | 50 | 547289 | 129668 | 0 |
| | T2Eg | 100 | 547445 | 129681 | 0 |
| | T2Wg | 100 | 547239 | 129664 | 0 |
| | T2Eh | 150 | 547494 | 129685 | 0 |
| | T2Wh | 150 | 547189 | 129659 | 0 |
| | T2Ei | 180 | 547545 | 129690 | 0 |
| | T2Wi | 180 | 547139 | 129656 | 0 |
| B2026 | T3Ea | 0 | 546919 | 130942 | 0 |
| | T3Wa | 0 | 546913 | 130940 | 0 |
| | T3Eb | 2 | 546921 | 130942 | 0 |
| | T3Wb | 2 | 546911 | 130939 | 0 |
| | T3Ec | 5 | 546924 | 130943 | 0 |
| | T3Wc | 5 | 546908 | 130939 | 0 |
| | T3Ed | 10 | 546929 | 130944 | 0 |
| | T3Wd | 10 | 546903 | 130937 | 0 |
| | T3Ee | 25 | 546943 | 130948 | 0 |
| | T3We | 25 | 546888 | 130934 | 0 |
| | T3Ef | 50 | 546967 | 130954 | 0 |
| | T3Wf | 50 | 546864 | 130927 | 0 |
| | T3Eg | 100 | 547015 | 130967 | 0 |
| | T3Wg | 100 | 546816 | 130914 | 0 |
| | T3Eh | 150 | 547064 | 130980 | 0 |
| | T3Wh | 150 | 546767 | 130901 | 0 |
| | T3Ei | 200 | 547112 | 130993 | 0 |
| | T3Wi | 200 | 546719 | 130889 | 0 |
| B2026 | T4Ea | 0 | 546970 | 131859 | 0 |
| | T4Wa | 0 | 546965 | 131863 | 0 |
| | T4Eb | 2 | 546972 | 131858 | 0 |
| | T4Wb | 2 | 546964 | 131864 | 0 |
| | T4Ec | 5 | 546975 | 131856 | 0 |

| Road ID | Transect point | Distance from kerb (m) | X | Y | Height (m) |
|-----------------|----------------|------------------------|--------|--------|------------|
| | T4Wc | 5 | 546961 | 131866 | 0 |
| | T4Ed | 10 | 546979 | 131854 | 0 |
| | T4Wd | 10 | 546957 | 131869 | 0 |
| | T4Ee | 25 | 546991 | 131845 | 0 |
| | T4We | 25 | 546945 | 131877 | 0 |
| | T4Ef | 50 | 547012 | 131831 | 0 |
| | T4Wf | 50 | 546924 | 131892 | 0 |
| | T4Eg | 100 | 547053 | 131802 | 0 |
| | T4Wg | 100 | 546883 | 131920 | 0 |
| | T4Eh | 150 | 547094 | 131773 | 0 |
| | T4Wh | 150 | 546842 | 131949 | 0 |
| | T4Ei | 200 | 547135 | 131745 | 0 |
| | T4Wi | 200 | 546801 | 131977 | 0 |
| New Road | T5Ea | 0 | 547916 | 128522 | 0 |
| | T5Wa | 0 | 547915 | 128516 | 0 |
| | T5Eb | 2 | 547917 | 128524 | 0 |
| | T5Wb | 2 | 547915 | 128514 | 0 |
| | T5Ec | 5 | 547917 | 128527 | 0 |
| | T5Wc | 5 | 547914 | 128511 | 0 |
| | T5Ed | 10 | 547918 | 128532 | 0 |
| | T5Wd | 10 | 547913 | 128506 | 0 |
| | T5Ee | 25 | 547921 | 128547 | 0 |
| | T5We | 25 | 547911 | 128491 | 0 |
| | T5Ef | 50 | 547925 | 128572 | 0 |
| | T5Wf | 50 | 547906 | 128466 | 0 |
| | T5Eg | 100 | 547934 | 128622 | 0 |
| | T5Wg | 100 | 547897 | 128417 | 0 |
| | T5Eh | 150 | 547944 | 128671 | 0 |
| | T5Wh | 150 | 547888 | 128367 | 0 |
| | T5Ei | 200 | 547954 | 128723 | 0 |

| Road ID | Transect point | Distance from kerb (m) | X | Y | Height (m) |
|------------------|----------------|------------------------|--------|--------|------------|
| | T5Wi | 200 | 547885 | 128350 | 0 |
| Crowborough Road | T6Ea | 0 | 546083 | 128718 | 0 |
| | T6Wa | 0 | 546079 | 128713 | 0 |
| | T6Eb | 2 | 546084 | 128720 | 0 |
| | T6Wb | 2 | 546078 | 128712 | 0 |
| | T6Ec | 5 | 546086 | 128722 | 0 |
| | T6Wc | 5 | 546076 | 128709 | 0 |
| | T6Ed | 10 | 546089 | 128727 | 0 |
| | T6Wd | 10 | 546074 | 128705 | 0 |
| | T6Ee | 25 | 546098 | 128739 | 0 |
| | T6We | 25 | 546065 | 128693 | 0 |
| | T6Ef | 50 | 546112 | 128758 | 0 |
| | T6Wf | 50 | 546050 | 128673 | 0 |
| | T6Eg | 100 | 546141 | 128799 | 0 |
| | T6Wg | 100 | 546021 | 128632 | 0 |
| | T6Eh | 150 | 546171 | 128840 | 0 |
| | T6Wh | 150 | 545992 | 128591 | 0 |
| | T6Ei | 200 | 546199 | 128880 | 0 |
| | T6Wi | 200 | 545963 | 128551 | 0 |
| A22 | T7Ea | 0 | 544047 | 129223 | 0 |
| | T7Wa | 0 | 544041 | 129222 | 0 |
| | T7Eb | 2 | 544049 | 129224 | 0 |
| | T7Wb | 2 | 544039 | 129221 | 0 |
| | T7Ec | 5 | 544052 | 129225 | 0 |
| | T7Wc | 5 | 544036 | 129220 | 0 |
| | T7Ed | 10 | 544057 | 129226 | 0 |
| | T7Wd | 10 | 544032 | 129219 | 0 |
| | T7Ee | 25 | 544071 | 129231 | 0 |
| | T7We | 25 | 544017 | 129214 | 0 |

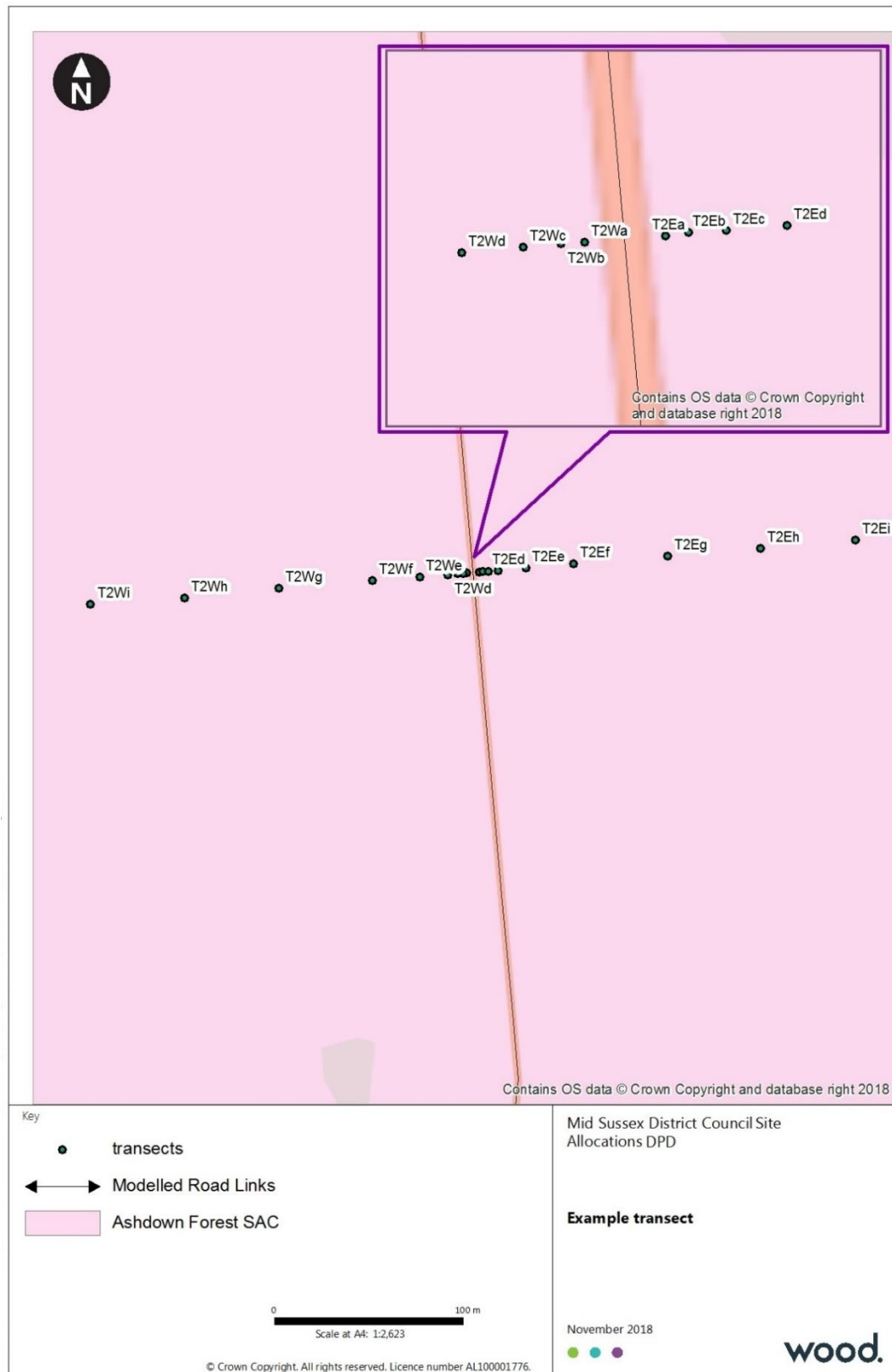
| Road ID | Transect point | Distance from kerb (m) | X | Y | Height (m) |
|-------------|----------------|------------------------|--------|--------|------------|
| | T7Ef | 50 | 544095 | 129238 | 0 |
| | T7Wf | 50 | 543993 | 129207 | 0 |
| | T7Eg | 100 | 544144 | 129250 | 0 |
| | T7Wg | 100 | 543945 | 129193 | 0 |
| | T7Eh | 150 | 544191 | 129268 | 0 |
| | T7Wh | 150 | 543898 | 129178 | 0 |
| | T7Ei | 200 | 544239 | 129281 | 0 |
| | T7Wi | 175 | 543850 | 129162 | 0 |
| A22 | T8Wa | 0 | 542395 | 131342 | 0 |
| | T8Wb | 2 | 542393 | 131340 | 0 |
| | T8Wc | 5 | 542391 | 131338 | 0 |
| | T8Wd | 10 | 542387 | 131335 | 0 |
| | T8We | 25 | 542376 | 131324 | 0 |
| | T8Wf | 50 | 542358 | 131307 | 0 |
| | T8Wg | 100 | 542321 | 131272 | 0 |
| | T8Wh | 150 | 542284 | 131238 | 0 |
| | T8Wi | 200 | 542247 | 131203 | 0 |
| A275 | T9Ea | 0 | 541707 | 131005 | 0 |
| | T9Wa | 0 | 541700 | 131007 | 0 |
| | T9Eb | 2 | 541709 | 131004 | 0 |
| | T9Wb | 2 | 541698 | 131007 | 0 |
| | T9Ec | 5 | 541711 | 131004 | 0 |
| | T9Wc | 5 | 541695 | 131008 | 0 |
| | T9Ed | 10 | 541716 | 131002 | 0 |
| | T9Wd | 10 | 541691 | 131009 | 0 |
| | T9Ee | 25 | 541731 | 130998 | 0 |
| | T9We | 25 | 541676 | 131013 | 0 |
| | T9Ef | 50 | 541755 | 130992 | 0 |
| | T9Wf | 50 | 541652 | 131020 | 0 |
| | T9Eg | 100 | 541804 | 130979 | 0 |

| Road ID | Transect point | Distance from kerb (m) | X | Y | Height (m) |
|----------------------------|----------------|------------------------|--------|--------|------------|
| | T9Wg | 100 | 541603 | 131033 | 0 |
| | T9Eh | 150 | 541852 | 130966 | 0 |
| | T9Wh | 150 | 541554 | 131046 | 0 |
| | T9Ei | 200 | 541901 | 130953 | 0 |
| | T9Wi | 200 | 541506 | 131059 | 0 |
| Hindleap Lane | T10Ea | 0 | 541008 | 132098 | 0 |
| | T10Wa | 0 | 541006 | 132092 | 0 |
| | T10Eb | 2 | 541009 | 132099 | 0 |
| | T10Wb | 2 | 541005 | 132091 | 0 |
| | T10Ec | 5 | 541010 | 132102 | 0 |
| | T10Wc | 5 | 541004 | 132088 | 0 |
| | T10Ed | 10 | 541012 | 132107 | 0 |
| | T10Wd | 10 | 541002 | 132083 | 0 |
| | T10Ee | 25 | 541018 | 132121 | 0 |
| | T10We | 25 | 540996 | 132069 | 0 |
| | T10Ef | 50 | 541027 | 132144 | 0 |
| | T10Wf | 50 | 540986 | 132046 | 0 |
| | T10Eg | 100 | 541047 | 132190 | 0 |
| | T10Wg | 100 | 540966 | 132000 | 0 |
| | T10Eh | 150 | 541066 | 132237 | 0 |
| | T10Wh | 150 | 540947 | 131954 | 0 |
| | T10Wi | 200 | 540934 | 131924 | 0 |
| Colemans Hatch Road | T11Ea | 0 | 541734 | 133412 | 0 |
| | T11Wa | 0 | 541728 | 133417 | 0 |
| | T11Eb | 2 | 541736 | 133411 | 0 |
| | T11Wb | 2 | 541726 | 133418 | 0 |
| | T11Ec | 5 | 541738 | 133409 | 0 |
| | T11Wc | 5 | 541723 | 133420 | 0 |
| | T11Ed | 10 | 541742 | 133406 | 0 |

| Road ID | Transect point | Distance from kerb (m) | X | Y | Height (m) |
|------------|----------------|------------------------|--------|--------|------------|
| | T11Wd | 10 | 541719 | 133423 | 0 |
| | T11Ee | 25 | 541755 | 133397 | 0 |
| | T11We | 25 | 541707 | 133432 | 0 |
| | T11Ef | 50 | 541775 | 133383 | 0 |
| | T11Wf | 50 | 541687 | 133446 | 0 |
| | T11Eg | 100 | 541815 | 133353 | 0 |
| | T11Wg | 100 | 541646 | 133476 | 0 |
| | T11Eh | 150 | 541858 | 133323 | 0 |
| | T11Wh | 150 | 541606 | 133505 | 0 |
| | T11Ei | 200 | 541915 | 133281 | 0 |
| | T11Wi | 200 | 541565 | 133534 | 0 |
| A26 | T12Wa | 0 | 548790 | 128796 | 0 |
| | T12Wb | 2 | 548789 | 128797 | 0 |
| | T12Wc | 5 | 548787 | 128800 | 0 |
| | T12Wd | 12 | 548784 | 128804 | 0 |
| | T12We | 25 | 548775 | 128816 | 0 |
| | T12Wf | 50 | 548761 | 128837 | 0 |
| | T12Wg | 100 | 548733 | 128878 | 0 |
| | T12Wh | 150 | 548704 | 128918 | 0 |
| | T12Wi | 200 | 548676 | 128960 | 0 |

Notes: E – East of road / W – West of road.

Figure B.1 Transect examples





Appendix C

ADMS-Roads input

Traffic data

Table C.1 shows the combined two-ways traffic data provided by Systra for all modelled scenarios in the Sites DPD Scenario. The speed provided by Systra is the average speed during the AM and PM peak hours. Figure C.1 shows all modelled road links.

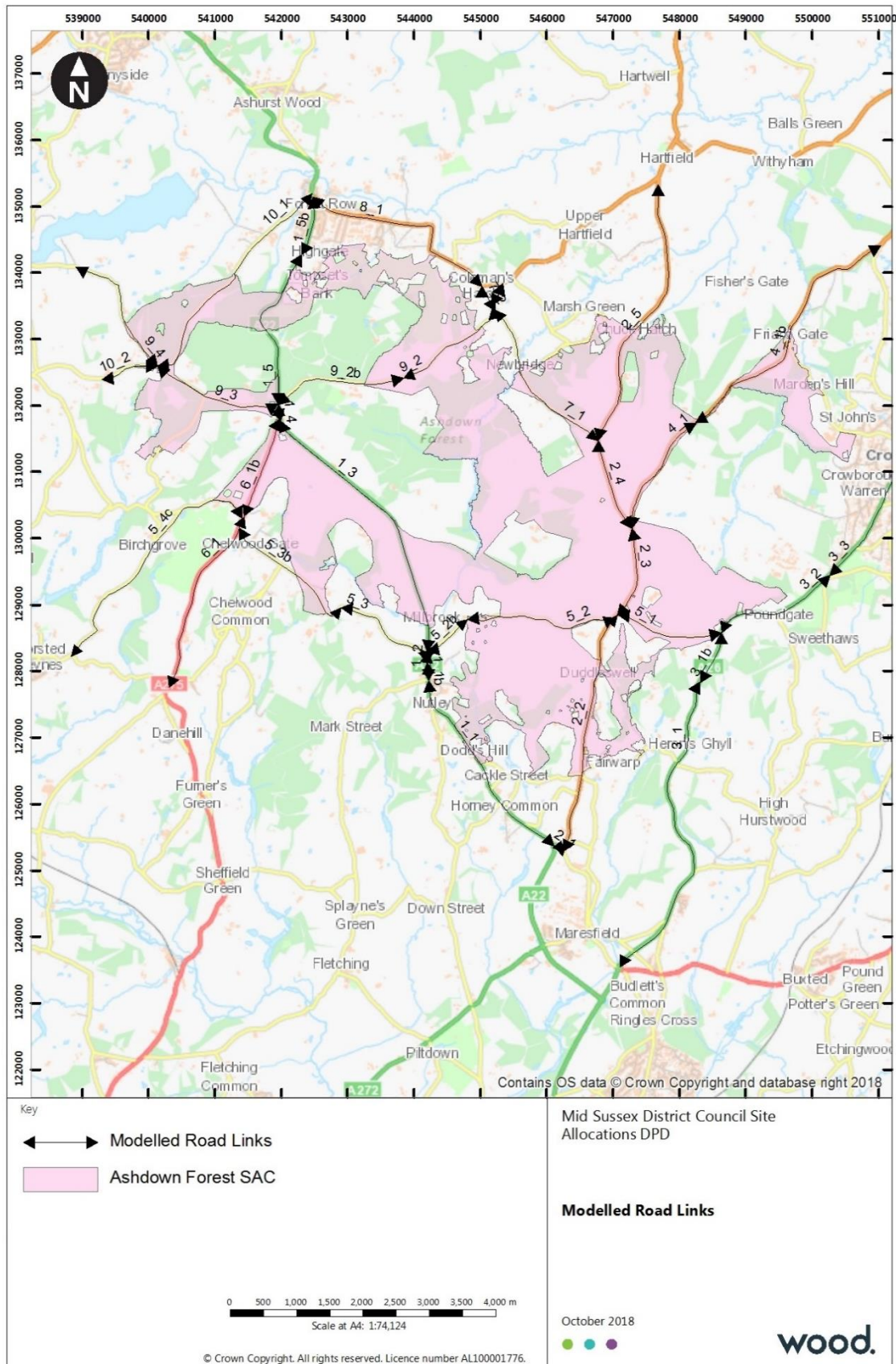
Table C.1 Annual Average Daily Traffic (AADT) flows for modelled scenarios – Sites DPD Scenario site allocations

| Link ID | 2017 Base / Scenario A - 2031 Projected Baseline | | | Scenario B – Do Minimum - 2031 Base + in-combination | | | Scenario C – Do Something - 2031 Base + in-combination + MSDC flows | | |
|---------|--|-------|-------------|--|-------|-------------|---|-------|-------------|
| | AADT | % HDV | Speed (kph) | AADT | % HDV | Speed (kph) | AADT | % HDV | Speed (kph) |
| 1_1 | 16380 | 1.86% | 66 | 18263 | 1.83% | 66 | 18109 | 1.84% | 66 |
| 1_1b | 16380 | 1.96% | 66 | 18263 | 1.83% | 66 | 18109 | 1.84% | 66 |
| 1_2 | 15804 | 2.00% | 52 | 17308 | 1.99% | 58 | 17274 | 1.99% | 58 |
| 1_3 | 19420 | 2.06% | 54 | 20280 | 2.11% | 54 | 20060 | 2.12% | 54 |
| 1_4 | 25484 | 2.31% | 38 | 27161 | 2.28% | 37 | 26972 | 2.28% | 22 |
| 1_5 | 14166 | 2.83% | 63 | 15344 | 2.78% | 59 | 15416 | 2.75% | 59 |
| 1_5b | 14166 | 2.83% | 45 | 15344 | 2.78% | 45 | 15416 | 2.75% | 45 |
| 2_1 | 12358 | 1.01% | 30 | 15536 | 2.74% | 34 | 15604 | 2.72% | 34 |
| 2_2 | 9731 | 0.78% | 38 | 9602 | 0.93% | 38 | 9549 | 0.94% | 38 |
| 2_3 | 11104 | 1.18% | 43 | 11342 | 1.31% | 42 | 11261 | 1.34% | 42 |
| 2_4 | 8271 | 1.26% | 43 | 8130 | 1.48% | 45 | 8089 | 1.52% | 43 |
| 2_5 | 8574 | 0.77% | 42 | 8507 | 0.94% | 43 | 8428 | 0.94% | 43 |
| 3_1 | 19145 | 2.46% | 53 | 19854 | 2.44% | 53 | 19728 | 2.44% | 52 |
| 3_1b | 19145 | 2.46% | 53 | 19854 | 2.44% | 53 | 19728 | 2.44% | 52 |
| 3_2 | 24286 | 2.62% | 52 | 24906 | 2.66% | 52 | 24889 | 2.65% | 52 |
| 3_3 | 15253 | 3.10% | 37 | 15737 | 3.10% | 40 | 15745 | 3.09% | 40 |
| 4_1 | 2833 | 0.94% | 43 | 3212 | 0.88% | 43 | 3172 | 0.90% | 43 |
| 4_1b | 2833 | 0.94% | 43 | 3212 | 0.88% | 43 | 3172 | 0.90% | 43 |
| 5_1 | 5596 | 2.93% | 40 | 6017 | 2.92% | 40 | 6091 | 2.88% | 40 |
| 5_2 | 4495 | 2.38% | 41 | 4764 | 2.44% | 41 | 4874 | 2.33% | 41 |
| 5_2b | 4495 | 2.38% | 41 | 4764 | 2.44% | 41 | 4874 | 2.33% | 41 |
| 5_3 | 1676 | 1.29% | 43 | 2893 | 0.98% | 43 | 3065 | 0.93% | 43 |
| 5_3b | 1676 | 1.29% | 43 | 2893 | 0.98% | 43 | 3065 | 0.93% | 43 |

| Link ID | 2017 Base / Scenario A - 2031 Projected Baseline | | | Scenario B – Do Minimum - 2031 Base + in-combination | | | Scenario C – Do Something - 2031 Base + in-combination + MSDC flows | | |
|---------|--|-------|-------------|--|-------|-------------|---|-------|-------------|
| | AADT | % HDV | Speed (kph) | AADT | % HDV | Speed (kph) | AADT | % HDV | Speed (kph) |
| 5_4 | 1814 | 1.36% | 61 | 2609 | 1.20% | 51 | 2753 | 1.11% | 61 |
| 5_4b | 1814 | 1.36% | 61 | 2609 | 1.20% | 51 | 2753 | 1.11% | 61 |
| 5_4c | 3627 | 1.36% | 61 | 5218 | 1.18% | 51 | 5506 | 1.16% | 61 |
| 6_1 | 8801 | 2.83% | 41 | 10170 | 2.52% | 42 | 10208 | 2.51% | 42 |
| 6_1b | 8801 | 2.83% | 41 | 10170 | 2.52% | 42 | 10208 | 2.51% | 42 |
| 7_1 | 2207 | 3.79% | 42 | 2349 | 3.79% | 42 | 2377 | 3.84% | 42 |
| 7_2 | 5587 | 2.54% | 42 | 6020 | 2.50% | 40 | 6060 | 2.51% | 40 |
| 8_1 | 9099 | 1.95% | 32 | 9528 | 1.97% | 32 | 9521 | 2.00% | 32 |
| 9_1 | 3799 | 1.56% | 43 | 4174 | 1.50% | 42 | 4251 | 1.46% | 42 |
| 9_2 | 3799 | 1.56% | 43 | 4174 | 1.50% | 42 | 4251 | 1.46% | 42 |
| 9_2b | 3799 | 1.56% | 43 | 4174 | 1.50% | 42 | 4251 | 1.46% | 42 |
| 9_3 | 12356 | 0.85% | 27 | 13112 | 0.87% | 33 | 13166 | 0.86% | 33 |
| 10_1 | 12356 | 0.85% | 61 | 12356 | 0.85% | 61 | 12356 | 0.85% | 61 |
| 10_2 | 12356 | 0.85% | 61 | 12356 | 0.85% | 61 | 12356 | 0.85% | 61 |

Note: HDV= Heavy Duty Vehicle.

Figure C.1 Modelled road links



Appendix D

ADMS-Roads model verification

The ADMS-Roads dispersion model has been widely validated for this type of assessment and is specifically listed in the Defra's LAQM.TG(16) guidance as an accepted dispersion model.

Model validation undertaken by the software developer (CERC) will not have included validation in the vicinity of the proposed Development Site. It is therefore necessary to perform a comparison of modelled results with local monitoring data at relevant locations. This process of verification attempts to minimise modelling uncertainty and systematic error by correcting modelled results by an adjustment factor to gain greater confidence in the final results.

The predicted results from a dispersion model may differ from measured concentrations for a large number of reasons, including uncertainties associated with:

- Background concentration estimates;
- Meteorological data;
- Source activity data such as traffic flows and emissions factors;
- Model input parameters such as surface roughness length, minimum Monin-Obukhov length;
- Monitoring data, including locations; and
- Overall model limitations.

Model verification is the process by which these and other uncertainties are investigated and where possible minimised. In reality, the differences between modelled and monitored results are likely to be a combination of all of these aspects.

Model setup parameters and input data were checked prior to running the models in order to reduce these uncertainties. The following were checked to the extent possible to ensure accuracy:

- Traffic data;
- Road widths;
- Distance between sources and monitoring as represented in the model;
- Speed estimates on roads;
- Source types, such as elevated roads and street canyons;
- Selection of representative meteorological data;
- Background monitoring and background estimates; and
- Monitoring data.

NO₂ Verification

Table D.1 below shows the diffusion tubes available for model verification. The decision was made to use data collected in Ashdown Forest by Air Quality Consultants (AQC) on behalf of Wealden District Council in the period between October 2014 and August 2016. It was felt that even though this data was collected over a two-year period, the monitoring locations were the most relevant to this assessment. AQC installed monitoring equipment in 72 locations across Ashdown Forest. Of these sites, 24 monitoring stations were used for model verification. The publicly available AQC report has been redacted, so coordinates are unavailable for some monitoring locations. Sites were also screened to only include 'roadside' (between 1 m and 5 m from the kerb) with reference to LAQM.TG(16) and, as the height of the monitors is not provided by AQC, only sites that could be located using Google Streetview were included. Also, monitoring sites were discounted if they were located on a road not identified by Footprint Ecology as a location that should

include a transect. Tube T2 and tube T42 met these criteria, however were discounted as the recorded concentrations were not consistent with other monitors in the same areas.

Table D.1 Local monitoring data suitable for ADMS-Roads model verification

| AQC monitoring location | Oct 2014 – Aug 2016 period mean NO ₂ (µgm ⁻³) | Interpolated background NO _x concentration (µgm ⁻³) | X (m) | Y (m) | Height (m) |
|-------------------------|--|--|--------|--------|------------|
| A1 | 17.6 | 9.8 | 547294 | 129153 | 1.5 |
| T1 | 21.7 | 11.2 | 542199 | 134088 | 2.0 |
| T3 | 27.9 | 10.9 | 541849 | 133049 | 2.0 |
| T4 | 25.6 | 10.7 | 541953 | 132229 | 2.0 |
| T6 | 12.5 | 9.6 | 546890 | 131049 | 2.0 |
| T15 | 11.4 | 9.6 | 547401 | 130703 | 2.0 |
| T19 | 27.3 | 10.1 | 549090 | 128879 | 1.8 |
| T20 | 22.9 | 10.1 | 548709 | 128701 | 1.5 |
| T21 | 34.1 | 10.1 | 548892 | 128852 | 2.0 |
| T22 | 27.6 | 10.1 | 549140 | 128880 | 1.5 |
| T23 | 15.1 | 10.0 | 547885 | 128514 | 1.5 |
| T24 | 13.0 | 10.1 | 546788 | 127981 | 2.0 |
| T25 | 14.9 | 10.3 | 546665 | 127421 | 1.5 |
| T29 | 17.0 | 10.4 | 544600 | 127196 | 2.0 |
| T31 | 23.2 | 10.3 | 544020 | 129316 | 1.5 |
| T32 | 24.9 | 10.3 | 544010 | 129312 | 1.5 |
| T33 | 27.7 | 10.2 | 543978 | 129407 | 1.5 |
| T34 | 16.0 | 10.7 | 542302 | 131412 | 1.5 |
| T35 | 19.7 | 10.5 | 542861 | 130963 | 1.5 |
| T36 | 22.4 | 10.3 | 543617 | 130337 | 1.5 |
| T37 | 21.7 | 10.2 | 543887 | 129685 | 1.5 |
| T38 | 12.2 | 10.0 | 545412 | 128806 | 2.0 |
| T48 | 14.4 | 10.7 | 541856 | 131411 | 1.5 |
| T49 | 12.9 | 10.7 | 541722 | 131040 | 1.5 |

Verification calculations

The verification of the modelling output was performed in accordance with the methodology provided in Chapter 7 of LAQM.TG(16). Table D.2 shows variation in the over and under prediction of monitored concentrations at the monitoring sites.

Table D.2 Verification, modelled versus monitored concentrations

| AQC monitoring location | 2015 Modelled Annual Mean Total NO ₂ (µgm ⁻³) | Monitored 2014-2016 Period Mean NO ₂ (µgm ⁻³) | % (Modelled-Monitored)/ Monitored |
|-------------------------|--|--|-----------------------------------|
| A1 | 15.4 | 17.6 | -12% |
| T1 | 15.9 | 21.7 | -27% |
| T3 | 15.9 | 27.9 | -43% |
| T4 | 15.5 | 25.6 | -40% |
| T6 | 12.3 | 12.5 | -1% |
| T15 | 10.3 | 11.4 | -10% |
| T19 | 20.4 | 27.3 | -25% |
| T20 | 21.7 | 22.9 | -5% |
| T21 | 22.7 | 34.1 | -33% |
| T22 | 20.4 | 27.6 | -26% |
| T23 | 10.8 | 15.1 | -28% |
| T24 | 12.3 | 13 | -5% |
| T25 | 13.7 | 14.9 | -8% |
| T29 | 17.2 | 17 | 1% |
| T31 | 18.7 | 23.2 | -20% |
| T32 | 17.6 | 24.9 | -29% |
| T33 | 16.8 | 27.7 | -39% |
| T34 | 15.1 | 16 | -5% |
| T35 | 15.0 | 19.7 | -24% |
| T36 | 13.0 | 22.4 | -42% |
| T37 | 18.2 | 21.7 | -16% |
| T38 | 10.3 | 12.2 | -16% |
| T48 | 14.8 | 14.4 | 3% |
| T49 | 14.5 | 12.9 | 12% |

Table D.3 shows the comparison of modelled road-NO_x, a direct output from the ADMS-Roads modelling, with the monitored road-NO_x, determined from the LAQM NO_x to NO₂ conversion tool. The adjustment factor used in this assessment is 1.626.

Table D.3 Comparison of modelled and monitored road-NO_x to determine verification factor

| AQC monitoring location | 2015 Modelled Annual Mean Road NO _x (µgm ⁻³) | 2014-2016 Monitored Period Mean Road NO _x (µgm ⁻³) | Ratio |
|-------------------------|---|---|-------|
| A1 | 13.3 | 17.5 | 1.31 |
| T1 | 12.9 | 24.3 | 1.89 |
| T3 | 13.1 | 37.5 | 2.86 |
| T4 | 12.5 | 32.8 | 2.62 |
| T6 | 7.8 | 8.1 | 1.04 |
| T15 | 3.9 | 6.0 | 1.55 |
| T19 | 22.7 | 37.1 | 1.63 |
| T20 | 25.4 | 27.9 | 1.10 |
| T21 | 27.5 | 52.2 | 1.90 |
| T22 | 22.8 | 37.8 | 1.66 |
| T23 | 4.4 | 12.4 | 2.84 |
| T24 | 7.2 | 8.5 | 1.18 |
| T25 | 9.5 | 11.9 | 1.24 |
| T29 | 16.1 | 15.8 | 0.98 |
| T31 | 19.2 | 28.4 | 1.48 |
| T32 | 17.2 | 31.9 | 1.86 |
| T33 | 15.6 | 37.9 | 2.42 |
| T34 | 11.9 | 13.6 | 1.14 |
| T35 | 11.8 | 21.1 | 1.78 |
| T36 | 8.4 | 26.7 | 3.19 |
| T37 | 18.4 | 25.4 | 1.38 |
| T38 | 3.4 | 6.9 | 2.06 |
| T48 | 11.3 | 10.5 | 0.93 |
| T49 | 10.7 | 7.7 | 0.72 |

Table D.4 shows the comparison of the modelled NO₂ concentration calculated by multiplying the modelled road NO_x by the adjustment factor and using the LAQM's NO_x to NO₂ conversion tool to calculate the total adjusted modelled NO₂.

Table D.4 Comparison of adjusted modelled NO₂ and monitored NO₂

| AQC monitoring location | 2015 Adjusted Modelled Annual Mean Total NO ₂ (µgm ⁻³) | 2014-2016 Monitored Period Mean NO ₂ (µgm ⁻³) | % (modelled/ monitored) / monitored |
|-------------------------|---|--|-------------------------------------|
| A1 | 19.7 | 17.6 | 12% |
| T1 | 20.0 | 21.7 | -8% |
| T3 | 20.1 | 27.9 | -28% |
| T4 | 19.5 | 25.6 | -24% |
| T6 | 14.9 | 12.5 | 19% |
| T15 | 11.6 | 11.4 | 1% |
| T19 | 27.2 | 27.3 | 0% |
| T20 | 29.3 | 22.9 | 28% |
| T21 | 30.8 | 34.1 | -10% |
| T22 | 27.3 | 27.6 | -1% |
| T23 | 12.3 | 15.1 | -19% |
| T24 | 14.7 | 13 | 13% |
| T25 | 16.8 | 14.9 | 13% |
| T29 | 22.2 | 17 | 31% |
| T31 | 24.6 | 23.2 | 6% |
| T32 | 23.0 | 24.9 | -8% |
| T33 | 21.8 | 27.7 | -21% |
| T34 | 19.0 | 16 | 19% |
| T35 | 18.8 | 19.7 | -5% |
| T36 | 15.8 | 22.4 | -29% |
| T37 | 23.9 | 21.7 | 10% |
| T38 | 11.4 | 12.2 | -6% |
| T48 | 18.4 | 14.4 | 28% |
| T49 | 18.0 | 12.9 | 39% |

The majority of modelled NO₂ concentrations are within 25% of monitored concentrations as specified by LAQM.TG(16), which is considered acceptable given the high number of monitoring sites used in verification and broad area covered, therefore NO₂ concentrations have been amended using this adjustment factor of 1.626.

Model uncertainty

In line with LAQM.TG(16), statistical procedures have been carried out to assess the uncertainties within the model as shown in Table D.5.

Table D.5 Assessment of model uncertainty

| Statistical parameter | Ideal value | Calculated value | Comment |
|-------------------------------|-------------|------------------|---|
| Correlation coefficient | 1 | 0.792 | Model shows a relationship between monitored and modelled concentrations. |
| Root mean square error (RMSE) | 0 | 3.8 | Within the 10 $\mu\text{g m}^{-3}$ value indicated by LAQM.TG(16) to revisit model inputs and verification, so no further action taken. |
| Fractional bias | 0 | 0 | Model shows no overall tendency to over or under predict after adjustment |

Appendix E

ADMS-Roads result

Table E.1 Predicted annual mean NO_x concentrations (µgm⁻³)

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T1Ea | 43.9 | 31.2 | 30.9 | 30.8 | -0.14 |
| T1Wa | 35.5 | 25.9 | 25.6 | 25.5 | -0.10 |
| T1Eb | 35.2 | 25.7 | 25.5 | 25.4 | -0.10 |
| T1Wb | 27.8 | 21.1 | 20.9 | 20.9 | -0.07 |
| T1Ec | 28.5 | 21.6 | 21.4 | 21.4 | -0.07 |
| T1Wc | 22.6 | 17.9 | 17.8 | 17.8 | -0.05 |
| T1Ed | 23.1 | 18.3 | 18.2 | 18.1 | -0.05 |
| T1Wd | 18.7 | 15.5 | 15.5 | 15.4 | -0.03 |
| T1Ee | 17.4 | 14.7 | 14.7 | 14.7 | -0.03 |
| T1We | 14.9 | 13.2 | 13.2 | 13.2 | -0.02 |
| T1Ef | 14.6 | 13.1 | 13.1 | 13.0 | -0.02 |
| T1Wf | 13.1 | 12.1 | 12.1 | 12.1 | -0.01 |
| T1Eg | 13.0 | 12.1 | 12.1 | 12.1 | -0.01 |
| T1Wg | 12.2 | 11.5 | 11.6 | 11.6 | -0.01 |
| T1Eh | 12.5 | 11.7 | 11.7 | 11.7 | -0.01 |
| T1Wh | 11.8 | 11.3 | 11.4 | 11.4 | <0.01 |
| T1Ei | 12.2 | 11.5 | 11.6 | 11.6 | -0.01 |
| T1Wi | 11.7 | 11.3 | 11.3 | 11.3 | <0.01 |
| T2Ea | 47.8 | 33.5 | 33.9 | 33.8 | -0.14 |
| T2Wa | 34.0 | 24.7 | 25.0 | 24.9 | -0.09 |
| T2Eb | 38.3 | 27.6 | 27.9 | 27.8 | -0.11 |
| T2Wb | 26.3 | 20.0 | 20.2 | 20.1 | -0.06 |
| T2Ec | 30.7 | 22.8 | 23.1 | 23.0 | -0.08 |
| T2Wc | 21.5 | 17.0 | 17.2 | 17.1 | -0.04 |
| T2Ed | 24.6 | 19.0 | 19.2 | 19.2 | -0.05 |
| T2Wd | 17.9 | 14.8 | 14.9 | 14.9 | -0.03 |
| T2Ee | 18.1 | 15.0 | 15.1 | 15.1 | -0.03 |
| T2We | 14.3 | 12.7 | 12.7 | 12.7 | -0.01 |
| T2Ef | 14.9 | 13.0 | 13.1 | 13.1 | -0.02 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T2Wf | 12.7 | 11.7 | 11.7 | 11.7 | -0.01 |
| T2Eg | 13.0 | 11.9 | 11.9 | 11.9 | -0.01 |
| T2Wg | 11.8 | 11.1 | 11.1 | 11.1 | <0.01 |
| T2Eh | 12.3 | 11.5 | 11.5 | 11.5 | -0.01 |
| T2Wh | 11.4 | 10.9 | 10.9 | 10.9 | <0.01 |
| T2Ei | 12.0 | 11.2 | 11.3 | 11.3 | <0.01 |
| T2Wi | 11.2 | 10.8 | 10.8 | 10.8 | <0.01 |
| T3Ea | 38.1 | 27.4 | 27.1 | 27.0 | -0.07 |
| T3Wa | 25.6 | 19.6 | 19.5 | 19.4 | -0.04 |
| T3Eb | 31.2 | 23.1 | 22.9 | 22.9 | -0.05 |
| T3Wb | 21.1 | 16.8 | 16.7 | 16.7 | -0.03 |
| T3Ec | 25.7 | 19.7 | 19.5 | 19.5 | -0.04 |
| T3Wc | 17.9 | 14.9 | 14.8 | 14.8 | -0.02 |
| T3Ed | 21.1 | 16.9 | 16.8 | 16.7 | -0.03 |
| T3Wd | 15.5 | 13.4 | 13.4 | 13.4 | -0.01 |
| T3Ee | 16.1 | 13.8 | 13.8 | 13.7 | -0.01 |
| T3We | 13.1 | 11.9 | 11.9 | 11.9 | -0.01 |
| T3Ef | 13.7 | 12.3 | 12.3 | 12.3 | -0.01 |
| T3Wf | 12.0 | 11.2 | 11.2 | 11.2 | <0.01 |
| T3Eg | 12.3 | 11.4 | 11.4 | 11.4 | <0.01 |
| T3Wg | 11.3 | 10.8 | 10.8 | 10.8 | <0.01 |
| T3Eh | 11.8 | 11.1 | 11.1 | 11.1 | <0.01 |
| T3Wh | 11.1 | 10.7 | 10.7 | 10.7 | <0.01 |
| T3Ei | 11.5 | 11.0 | 11.0 | 11.0 | <0.01 |
| T3Wi | 11.0 | 10.6 | 10.6 | 10.6 | <0.01 |
| T4Ea | 37.9 | 27.3 | 27.3 | 27.1 | -0.13 |
| T4Wa | 36.7 | 26.6 | 26.6 | 26.5 | -0.13 |
| T4Eb | 29.6 | 22.1 | 22.1 | 22.0 | -0.09 |
| T4Wb | 28.6 | 21.5 | 21.5 | 21.4 | -0.09 |
| T4Ec | 24.1 | 18.7 | 18.7 | 18.7 | -0.07 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T4Wc | 23.2 | 18.2 | 18.2 | 18.1 | -0.06 |
| T4Ed | 19.8 | 16.0 | 16.1 | 16.0 | -0.04 |
| T4Wd | 19.1 | 15.6 | 15.6 | 15.6 | -0.04 |
| T4Ee | 15.3 | 13.3 | 13.3 | 13.3 | -0.02 |
| T4We | 14.9 | 13.0 | 13.1 | 13.0 | -0.02 |
| T4Ef | 13.2 | 12.0 | 12.0 | 12.0 | -0.01 |
| T4Wf | 12.9 | 11.8 | 11.9 | 11.8 | -0.01 |
| T4Eg | 12.0 | 11.3 | 11.3 | 11.3 | -0.01 |
| T4Wg | 11.8 | 11.2 | 11.2 | 11.2 | <0.01 |
| T4Eh | 11.6 | 11.0 | 11.0 | 11.0 | <0.01 |
| T4Wh | 11.4 | 10.9 | 11.0 | 11.0 | <0.01 |
| T4Ei | 11.4 | 10.9 | 10.9 | 10.9 | <0.01 |
| T4Wi | 11.2 | 10.8 | 10.8 | 10.8 | <0.01 |
| T5Ea | 32.9 | 24.2 | 25.2 | 25.4 | 0.16 |
| T5Wa | 24.5 | 19.0 | 19.6 | 19.7 | 0.10 |
| T5Eb | 26.3 | 20.1 | 20.8 | 21.0 | 0.11 |
| T5Wb | 19.8 | 16.1 | 16.5 | 16.6 | 0.06 |
| T5Ec | 21.8 | 17.4 | 17.9 | 18.0 | 0.08 |
| T5Wc | 17.2 | 14.5 | 14.8 | 14.8 | 0.04 |
| T5Ed | 18.4 | 15.2 | 15.6 | 15.6 | 0.05 |
| T5Wd | 15.1 | 13.3 | 13.5 | 13.5 | 0.03 |
| T5Ee | 14.9 | 13.1 | 13.3 | 13.3 | 0.03 |
| T5We | 13.2 | 12.1 | 12.2 | 12.2 | 0.01 |
| T5Ef | 13.2 | 12.1 | 12.2 | 12.2 | 0.01 |
| T5Wf | 12.3 | 11.5 | 11.6 | 11.6 | 0.01 |
| T5Eg | 12.3 | 11.5 | 11.6 | 11.6 | 0.01 |
| T5Wg | 11.8 | 11.2 | 11.3 | 11.3 | <0.01 |
| T5Eh | 11.9 | 11.3 | 11.3 | 11.3 | <0.01 |
| T5Wh | 11.6 | 11.1 | 11.2 | 11.2 | <0.01 |
| T5Ei | 11.7 | 11.2 | 11.2 | 11.2 | <0.01 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T5Wi | 11.6 | 11.1 | 11.1 | 11.1 | <0.01 |
| T6Ea | 26.4 | 20.1 | 20.7 | 20.9 | 0.22 |
| T6Wa | 19.4 | 15.8 | 16.1 | 16.3 | 0.12 |
| T6Eb | 22.4 | 17.7 | 18.1 | 18.3 | 0.16 |
| T6Wb | 16.7 | 14.2 | 14.4 | 14.5 | 0.08 |
| T6Ec | 19.3 | 15.8 | 16.1 | 16.2 | 0.12 |
| T6Wc | 15.0 | 13.1 | 13.3 | 13.4 | 0.06 |
| T6Ed | 16.7 | 14.2 | 14.4 | 14.5 | 0.08 |
| T6Wd | 13.7 | 12.3 | 12.4 | 12.5 | 0.04 |
| T6Ee | 13.9 | 12.4 | 12.6 | 12.6 | 0.04 |
| T6We | 12.3 | 11.5 | 11.6 | 11.6 | 0.02 |
| T6Ef | 12.6 | 11.6 | 11.7 | 11.7 | 0.02 |
| T6Wf | 11.7 | 11.1 | 11.2 | 11.2 | 0.01 |
| T6Eg | 11.7 | 11.1 | 11.2 | 11.2 | 0.01 |
| T6Wg | 11.4 | 10.9 | 11.0 | 11.0 | 0.01 |
| T6Eh | 11.5 | 10.9 | 11.0 | 11.0 | 0.01 |
| T6Wh | 11.2 | 10.9 | 10.9 | 10.9 | <0.01 |
| T6Ei | 11.3 | 10.8 | 10.9 | 10.9 | 0.01 |
| T6Wi | 11.2 | 10.8 | 10.9 | 10.9 | <0.01 |
| T7Ea | 69.5 | 47.8 | 49.4 | 49.0 | -0.41 |
| T7Wa | 45.6 | 32.3 | 33.3 | 33.0 | -0.24 |
| T7Eb | 55.4 | 38.8 | 40.1 | 39.7 | -0.31 |
| T7Wb | 34.2 | 25.2 | 25.9 | 25.7 | -0.16 |
| T7Ec | 43.6 | 31.3 | 32.3 | 32.0 | -0.23 |
| T7Wc | 27.2 | 20.9 | 21.3 | 21.2 | -0.11 |
| T7Ed | 33.8 | 25.1 | 25.8 | 25.6 | -0.16 |
| T7Wd | 21.9 | 17.6 | 17.9 | 17.8 | -0.07 |
| T7Ee | 23.1 | 18.4 | 18.8 | 18.7 | -0.08 |
| T7We | 16.5 | 14.2 | 14.4 | 14.4 | -0.04 |
| T7Ef | 17.8 | 15.1 | 15.3 | 15.3 | -0.05 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T7Wf | 14.0 | 12.7 | 12.8 | 12.8 | -0.02 |
| T7Eg | 14.7 | 13.1 | 13.3 | 13.3 | -0.02 |
| T7Wg | 12.5 | 11.8 | 11.9 | 11.9 | -0.01 |
| T7Eh | 13.5 | 12.4 | 12.5 | 12.5 | -0.02 |
| T7Wh | 12.1 | 11.5 | 11.6 | 11.6 | <0.01 |
| T7Ei | 12.9 | 12.0 | 12.1 | 12.1 | -0.01 |
| T7Wi | 11.8 | 11.3 | 11.4 | 11.4 | <0.01 |
| T8Wa | 44.3 | 31.9 | 32.9 | 32.6 | -0.23 |
| T8Wb | 34.4 | 25.7 | 26.4 | 26.2 | -0.16 |
| T8Wc | 27.9 | 21.6 | 22.1 | 22.0 | -0.11 |
| T8Wd | 22.7 | 18.4 | 18.7 | 18.7 | -0.07 |
| T8We | 17.4 | 15.0 | 15.3 | 15.2 | -0.03 |
| T8Wf | 14.9 | 13.5 | 13.7 | 13.6 | -0.02 |
| T8Wg | 13.5 | 12.6 | 12.7 | 12.7 | -0.01 |
| T8Wh | 13.0 | 12.3 | 12.4 | 12.4 | <0.01 |
| T8Wi | 12.8 | 12.2 | 12.3 | 12.3 | <0.01 |
| T9Ea | 41.7 | 30.1 | 33.2 | 33.2 | 0.08 |
| T9Wa | 36.0 | 26.5 | 29.0 | 29.1 | 0.06 |
| T9Eb | 32.4 | 24.3 | 26.4 | 26.5 | 0.05 |
| T9Wb | 28.1 | 21.6 | 23.3 | 23.3 | 0.04 |
| T9Ec | 26.7 | 20.8 | 22.3 | 22.4 | 0.04 |
| T9Wc | 23.1 | 18.5 | 19.7 | 19.7 | 0.03 |
| T9Ed | 22.0 | 17.9 | 19.0 | 19.0 | 0.03 |
| T9Wd | 19.4 | 16.3 | 17.1 | 17.1 | 0.02 |
| T9Ee | 17.1 | 14.9 | 15.5 | 15.5 | 0.02 |
| T9We | 15.6 | 13.9 | 14.4 | 14.4 | 0.01 |
| T9Ef | 14.8 | 13.4 | 13.8 | 13.8 | 0.01 |
| T9Wf | 13.9 | 12.9 | 13.2 | 13.2 | 0.01 |
| T9Eg | 13.4 | 12.6 | 12.8 | 12.8 | 0.01 |
| T9Wg | 12.9 | 12.3 | 12.5 | 12.5 | 0.01 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T9Eh | 12.9 | 12.3 | 12.5 | 12.5 | 0.01 |
| T9Wh | 12.6 | 12.1 | 12.2 | 12.2 | 0.01 |
| T9Ei | 12.7 | 12.1 | 12.3 | 12.3 | 0.01 |
| T9Wi | 12.4 | 12.0 | 12.1 | 12.1 | 0.01 |
| T10Ea | 60.0 | 41.2 | 45.2 | 45.4 | 0.15 |
| T10Wa | 40.9 | 29.5 | 32.0 | 32.1 | 0.09 |
| T10Eb | 47.6 | 33.6 | 36.6 | 36.7 | 0.12 |
| T10Wb | 30.6 | 23.2 | 24.8 | 24.9 | 0.06 |
| T10Ec | 37.1 | 27.1 | 29.3 | 29.3 | 0.08 |
| T10Wc | 25.0 | 19.7 | 20.8 | 20.9 | 0.04 |
| T10Ed | 29.1 | 22.2 | 23.7 | 23.7 | 0.06 |
| T10Wd | 20.7 | 17.1 | 17.9 | 17.9 | 0.03 |
| T10Ee | 20.7 | 17.0 | 17.8 | 17.8 | 0.03 |
| T10We | 16.4 | 14.4 | 14.8 | 14.9 | 0.02 |
| T10Ef | 16.8 | 14.7 | 15.1 | 15.1 | 0.02 |
| T10Wf | 14.4 | 13.2 | 13.4 | 13.4 | 0.01 |
| T10Eg | 14.5 | 13.3 | 13.5 | 13.5 | 0.01 |
| T10Wg | 13.2 | 12.5 | 12.6 | 12.6 | 0.01 |
| T10Eh | 13.7 | 12.8 | 12.9 | 13.0 | 0.01 |
| T10Wh | 12.7 | 12.2 | 12.3 | 12.3 | 0.01 |
| T10Wi | 12.5 | 12.1 | 12.2 | 12.2 | <0.01 |
| T11Ea | 23.7 | 18.7 | 19.3 | 19.5 | 0.14 |
| T11Wa | 25.4 | 19.8 | 20.6 | 20.7 | 0.16 |
| T11Eb | 19.0 | 15.7 | 16.2 | 16.3 | 0.09 |
| T11Wb | 20.7 | 16.9 | 17.4 | 17.5 | 0.11 |
| T11Ec | 16.6 | 14.3 | 14.6 | 14.6 | 0.06 |
| T11Wc | 17.9 | 15.1 | 15.5 | 15.6 | 0.07 |
| T11Ed | 14.6 | 13.0 | 13.2 | 13.3 | 0.04 |
| T11Wd | 15.7 | 13.7 | 14.0 | 14.1 | 0.05 |
| T11Ee | 12.8 | 11.9 | 12.0 | 12.1 | 0.02 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T11We | 13.6 | 12.4 | 12.6 | 12.6 | 0.03 |
| T11Ef | 12.0 | 11.5 | 11.5 | 11.5 | 0.01 |
| T11Wf | 12.6 | 11.8 | 12.0 | 12.0 | 0.02 |
| T11Eg | 11.6 | 11.2 | 11.3 | 11.3 | <0.01 |
| T11Wg | 12.0 | 11.5 | 11.6 | 11.6 | 0.01 |
| T11Eh | 11.5 | 11.1 | 11.2 | 11.2 | <0.01 |
| T11Wh | 11.8 | 11.3 | 11.4 | 11.4 | 0.01 |
| T11Ei | 11.4 | 11.1 | 11.1 | 11.1 | <0.01 |
| T11Wi | 11.7 | 11.3 | 11.3 | 11.3 | <0.01 |
| T12Wa | 80.0 | 54.9 | 56.0 | 55.9 | -0.06 |
| T12Wb | 65.1 | 45.2 | 46.1 | 46.0 | -0.05 |
| T12Wc | 46.5 | 33.2 | 33.8 | 33.8 | -0.03 |
| T12Wd | 35.4 | 26.1 | 26.5 | 26.5 | -0.02 |
| T12We | 23.6 | 18.6 | 18.8 | 18.8 | -0.01 |
| T12Wf | 17.7 | 14.9 | 15.1 | 15.1 | -0.01 |
| T12Wg | 14.2 | 12.7 | 12.8 | 12.8 | <0.01 |
| T12Wh | 13.0 | 12.0 | 12.0 | 12.0 | <0.01 |
| T12Wi | 12.4 | 11.6 | 11.6 | 11.6 | <0.01 |

Notes: **Bold** denotes exceedance of the 30 $\mu\text{g m}^{-3}$ annual mean NO_x AQO.

Table E.2 Predicted daily mean concentration of NO_x ($\mu\text{g m}^{-3}$)

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|--------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T1Ea | 100.7 | 70.8 | 70.1 | 69.8 | -0.33 |
| T1Wa | 106.0 | 73.6 | 72.8 | 72.5 | -0.35 |
| T1Eb | 77.7 | 56.2 | 55.7 | 55.5 | -0.23 |
| T1Wb | 82.1 | 58.8 | 58.2 | 58.0 | -0.25 |
| T1Ec | 61.9 | 46.3 | 46.0 | 45.8 | -0.16 |
| T1Wc | 64.0 | 47.6 | 47.2 | 47.0 | -0.18 |
| T1Ed | 49.9 | 38.8 | 38.7 | 38.5 | -0.11 |
| T1Wd | 51.1 | 39.6 | 39.3 | 39.2 | -0.12 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|--------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T1Ee | 37.3 | 31.1 | 31.0 | 31.0 | -0.06 |
| T1We | 37.7 | 31.4 | 31.2 | 31.2 | -0.07 |
| T1Ef | 31.3 | 27.4 | 27.4 | 27.3 | -0.03 |
| T1Wf | 31.3 | 27.4 | 27.3 | 27.3 | -0.04 |
| T1Eg | 27.5 | 25.1 | 25.1 | 25.1 | -0.02 |
| T1Wg | 27.3 | 25.0 | 25.0 | 24.9 | -0.02 |
| T1Eh | 26.1 | 24.2 | 24.3 | 24.3 | -0.01 |
| T1Wh | 25.9 | 24.1 | 24.1 | 24.1 | -0.02 |
| T1Ei | 25.4 | 23.8 | 23.8 | 23.8 | -0.01 |
| T1Wi | 25.5 | 23.8 | 23.9 | 23.8 | -0.01 |
| T2Ea | 112.1 | 77.4 | 78.5 | 78.2 | -0.34 |
| T2Wa | 111.1 | 76.5 | 77.5 | 77.2 | -0.34 |
| T2Eb | 86.0 | 61.0 | 61.9 | 61.6 | -0.24 |
| T2Wb | 84.8 | 60.1 | 60.8 | 60.5 | -0.24 |
| T2Ec | 65.8 | 48.6 | 49.1 | 49.0 | -0.16 |
| T2Wc | 66.8 | 48.9 | 49.4 | 49.2 | -0.18 |
| T2Ed | 52.6 | 40.4 | 40.8 | 40.6 | -0.11 |
| T2Wd | 52.7 | 40.2 | 40.6 | 40.4 | -0.12 |
| T2Ee | 38.8 | 31.7 | 32.0 | 31.9 | -0.06 |
| T2We | 37.8 | 31.0 | 31.2 | 31.1 | -0.07 |
| T2Ef | 31.9 | 27.3 | 27.5 | 27.5 | -0.03 |
| T2Wf | 30.6 | 26.6 | 26.7 | 26.7 | -0.04 |
| T2Eg | 27.8 | 24.8 | 25.0 | 24.9 | -0.02 |
| T2Wg | 26.2 | 23.9 | 24.0 | 23.9 | -0.02 |
| T2Eh | 26.2 | 23.9 | 24.0 | 24.0 | -0.02 |
| T2Wh | 24.9 | 23.0 | 23.1 | 23.1 | -0.01 |
| T2Ei | 25.3 | 23.3 | 23.5 | 23.5 | -0.01 |
| T2Wi | 24.2 | 22.6 | 22.7 | 22.7 | -0.01 |
| T3Ea | 89.5 | 63.1 | 62.5 | 62.3 | -0.17 |
| T3Wa | 83.9 | 59.6 | 58.9 | 58.8 | -0.17 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------------|-----------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T3Eb | 69.7 | 50.8 | 50.4 | 50.3 | -0.12 |
| T3Wb | 66.9 | 49.0 | 48.5 | 48.4 | -0.12 |
| T3Ec | 55.1 | 41.7 | 41.5 | 41.4 | -0.08 |
| T3Wc | 54.5 | 41.3 | 41.0 | 40.9 | -0.09 |
| T3Ed | 44.5 | 35.3 | 35.1 | 35.0 | -0.06 |
| T3Wd | 44.4 | 35.0 | 34.8 | 34.7 | -0.06 |
| T3Ee | 34.2 | 28.8 | 28.8 | 28.7 | -0.03 |
| T3We | 33.4 | 28.3 | 28.2 | 28.1 | -0.04 |
| T3Ef | 29.1 | 25.7 | 25.7 | 25.6 | -0.02 |
| T3Wf | 28.0 | 25.0 | 24.9 | 24.9 | -0.02 |
| T3Eg | 26.0 | 23.7 | 23.8 | 23.8 | -0.01 |
| T3Wg | 24.8 | 23.0 | 23.0 | 23.0 | -0.01 |
| T3Eh | 24.9 | 23.0 | 23.1 | 23.1 | <0.01 |
| T3Wh | 23.7 | 22.3 | 22.4 | 22.3 | -0.01 |
| T3Ei | 24.3 | 22.7 | 22.8 | 22.8 | <0.01 |
| T3Wi | 23.3 | 22.0 | 22.1 | 22.1 | -0.01 |
| T4Ea | 87.0 | 62.5 | 62.5 | 62.2 | -0.31 |
| T4Wa | 95.0 | 66.9 | 66.8 | 66.5 | -0.37 |
| T4Eb | 65.9 | 48.4 | 48.5 | 48.3 | -0.20 |
| T4Wb | 73.6 | 53.5 | 53.4 | 53.1 | -0.26 |
| T4Ec | 52.9 | 40.2 | 40.3 | 40.2 | -0.14 |
| T4Wc | 58.0 | 43.7 | 43.7 | 43.5 | -0.18 |
| T4Ed | 43.0 | 34.3 | 34.3 | 34.2 | -0.09 |
| T4Wd | 46.2 | 36.3 | 36.3 | 36.2 | -0.13 |
| T4Ee | 33.1 | 28.1 | 28.3 | 28.3 | -0.04 |
| T4We | 34.3 | 29.0 | 29.0 | 28.9 | -0.07 |
| T4Ef | 28.5 | 25.3 | 25.5 | 25.5 | -0.02 |
| T4Wf | 28.8 | 25.5 | 25.6 | 25.5 | -0.04 |
| T4Eg | 25.8 | 23.6 | 23.8 | 23.8 | -0.01 |
| T4Wg | 25.7 | 23.6 | 23.6 | 23.6 | -0.02 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------------|-----------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T4Eh | 24.8 | 23.0 | 23.2 | 23.2 | <0.01 |
| T4Wh | 24.6 | 22.9 | 23.0 | 22.9 | -0.02 |
| T4Ei | 24.3 | 22.7 | 22.9 | 22.9 | <0.01 |
| T4Wi | 24.0 | 22.6 | 22.6 | 22.6 | -0.01 |
| T5Ea | 73.4 | 53.1 | 55.5 | 55.9 | 0.38 |
| T5Wa | 69.1 | 51.1 | 53.2 | 53.6 | 0.33 |
| T5Eb | 57.9 | 43.6 | 45.3 | 45.5 | 0.26 |
| T5Wb | 53.3 | 41.0 | 42.4 | 42.6 | 0.21 |
| T5Ec | 46.8 | 36.7 | 37.9 | 38.1 | 0.18 |
| T5Wc | 44.7 | 35.5 | 36.5 | 36.7 | 0.15 |
| T5Ed | 38.7 | 31.7 | 32.5 | 32.6 | 0.12 |
| T5Wd | 37.8 | 31.2 | 31.9 | 32.0 | 0.10 |
| T5Ee | 30.9 | 26.9 | 27.3 | 27.4 | 0.06 |
| T5We | 30.9 | 26.9 | 27.3 | 27.4 | 0.05 |
| T5Ef | 27.2 | 24.6 | 24.9 | 24.9 | 0.03 |
| T5Wf | 27.4 | 24.7 | 25.0 | 25.0 | 0.02 |
| T5Eg | 25.1 | 23.3 | 23.5 | 23.5 | 0.02 |
| T5Wg | 25.4 | 23.6 | 23.7 | 23.7 | 0.01 |
| T5Eh | 24.5 | 22.9 | 23.1 | 23.1 | 0.01 |
| T5Wh | 24.8 | 23.2 | 23.3 | 23.3 | <0.01 |
| T5Ei | 24.3 | 22.8 | 22.9 | 22.9 | <0.01 |
| T5Wi | 24.7 | 23.1 | 23.3 | 23.3 | <0.01 |
| T6Ea | 60.5 | 45.2 | 46.6 | 47.2 | 0.55 |
| T6Wa | 61.2 | 45.7 | 47.1 | 47.6 | 0.53 |
| T6Eb | 48.7 | 37.8 | 38.9 | 39.3 | 0.38 |
| T6Wb | 50.8 | 39.2 | 40.2 | 40.6 | 0.39 |
| T6Ec | 40.7 | 32.9 | 33.7 | 33.9 | 0.27 |
| T6Wc | 43.6 | 34.7 | 35.5 | 35.8 | 0.29 |
| T6Ed | 34.6 | 29.1 | 29.7 | 29.9 | 0.19 |
| T6Wd | 37.7 | 31.1 | 31.7 | 31.9 | 0.21 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|--------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T6Ee | 28.7 | 25.4 | 25.8 | 25.9 | 0.10 |
| T6We | 31.4 | 27.2 | 27.5 | 27.7 | 0.12 |
| T6Ef | 25.8 | 23.7 | 24.0 | 24.0 | 0.06 |
| T6Wf | 28.1 | 25.2 | 25.4 | 25.5 | 0.07 |
| T6Eg | 24.5 | 22.9 | 23.0 | 23.0 | 0.02 |
| T6Wg | 25.9 | 23.8 | 23.9 | 24.0 | 0.04 |
| T6Eh | 24.1 | 22.6 | 22.8 | 22.8 | 0.01 |
| T6Wh | 24.8 | 23.2 | 23.3 | 23.3 | 0.02 |
| T6Ei | 23.9 | 22.5 | 22.6 | 22.6 | 0.01 |
| T6Wi | 24.2 | 22.8 | 22.9 | 22.9 | 0.01 |
| T7Ea | 164.2 | 111.5 | 115.5 | 114.5 | -0.99 |
| T7Wa | 157.4 | 107.0 | 110.6 | 109.7 | -0.94 |
| T7Eb | 124.1 | 86.2 | 89.0 | 88.3 | -0.71 |
| T7Wb | 123.7 | 85.4 | 88.2 | 87.4 | -0.72 |
| T7Ec | 92.8 | 66.3 | 68.3 | 67.8 | -0.49 |
| T7Wc | 96.1 | 68.1 | 70.1 | 69.6 | -0.52 |
| T7Ed | 71.0 | 52.9 | 54.3 | 54.0 | -0.33 |
| T7Wd | 73.9 | 54.2 | 55.6 | 55.2 | -0.36 |
| T7Ee | 49.7 | 39.1 | 40.0 | 39.8 | -0.18 |
| T7We | 49.9 | 39.2 | 39.9 | 39.7 | -0.19 |
| T7Ef | 39.0 | 32.3 | 32.9 | 32.8 | -0.11 |
| T7Wf | 38.3 | 31.9 | 32.4 | 32.2 | -0.11 |
| T7Eg | 32.2 | 28.0 | 28.4 | 28.3 | -0.06 |
| T7Wg | 31.3 | 27.5 | 27.8 | 27.7 | -0.06 |
| T7Eh | 29.4 | 26.3 | 26.6 | 26.5 | -0.04 |
| T7Wh | 28.8 | 25.9 | 26.1 | 26.1 | -0.04 |
| T7Ei | 27.9 | 25.3 | 25.6 | 25.5 | -0.03 |
| T7Wi | 27.4 | 25.1 | 25.2 | 25.2 | -0.03 |
| T8Wa | 156.5 | 108.1 | 111.7 | 110.8 | -0.93 |
| T8Wb | 120.5 | 85.0 | 87.6 | 86.9 | -0.68 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|--------------|--------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T8Wc | 93.8 | 67.9 | 69.8 | 69.3 | -0.50 |
| T8Wd | 72.7 | 54.3 | 55.7 | 55.3 | -0.35 |
| T8We | 50.1 | 39.8 | 40.6 | 40.4 | -0.19 |
| T8Wf | 38.9 | 32.7 | 33.2 | 33.1 | -0.11 |
| T8Wg | 32.1 | 28.5 | 28.7 | 28.6 | -0.06 |
| T8Wh | 29.5 | 26.9 | 27.1 | 27.0 | -0.05 |
| T8Wi | 28.2 | 26.0 | 26.2 | 26.1 | -0.04 |
| T9Ea | 95.1 | 68.0 | 75.2 | 75.4 | 0.19 |
| T9Wa | 99.3 | 70.3 | 77.7 | 77.9 | 0.17 |
| T9Eb | 70.1 | 52.1 | 56.9 | 57.0 | 0.13 |
| T9Wb | 78.3 | 57.1 | 62.4 | 62.6 | 0.12 |
| T9Ec | 56.9 | 43.8 | 47.3 | 47.4 | 0.09 |
| T9Wc | 62.2 | 47.1 | 50.8 | 50.9 | 0.08 |
| T9Ed | 47.0 | 37.7 | 40.1 | 40.2 | 0.07 |
| T9Wd | 50.4 | 39.7 | 42.3 | 42.4 | 0.05 |
| T9Ee | 36.0 | 30.9 | 32.3 | 32.3 | 0.05 |
| T9We | 38.5 | 32.4 | 33.8 | 33.8 | 0.02 |
| T9Ef | 30.6 | 27.5 | 28.3 | 28.4 | 0.03 |
| T9Wf | 32.9 | 28.9 | 29.8 | 29.8 | 0.01 |
| T9Eg | 27.4 | 25.5 | 26.0 | 26.0 | 0.02 |
| T9Wg | 29.6 | 26.9 | 27.4 | 27.4 | <0.01 |
| T9Eh | 26.8 | 25.1 | 25.4 | 25.4 | 0.01 |
| T9Wh | 28.4 | 26.1 | 26.5 | 26.5 | <0.01 |
| T9Ei | 26.5 | 24.9 | 25.2 | 25.2 | 0.01 |
| T9Wi | 27.7 | 25.7 | 26.1 | 26.0 | 0.00 |
| T10Ea | 135.5 | 92.2 | 101.2 | 101.6 | 0.34 |
| T10Wa | 132.4 | 92.6 | 101.4 | 101.7 | 0.33 |
| T10Eb | 108.2 | 75.2 | 82.3 | 82.6 | 0.28 |
| T10Wb | 98.9 | 70.9 | 77.0 | 77.2 | 0.23 |
| T10Ec | 81.6 | 58.8 | 63.8 | 64.0 | 0.20 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|--------------|-------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T10Wc | 78.2 | 57.5 | 62.0 | 62.1 | 0.17 |
| T10Ed | 62.8 | 47.3 | 50.7 | 50.8 | 0.14 |
| T10Wd | 62.4 | 47.5 | 50.7 | 50.8 | 0.12 |
| T10Ee | 43.9 | 35.7 | 37.5 | 37.6 | 0.08 |
| T10We | 45.6 | 36.8 | 38.7 | 38.8 | 0.07 |
| T10Ef | 35.0 | 30.3 | 31.3 | 31.4 | 0.05 |
| T10Wf | 37.3 | 31.7 | 32.8 | 32.9 | 0.04 |
| T10Eg | 30.2 | 27.3 | 27.9 | 27.9 | 0.02 |
| T10Wg | 32.1 | 28.5 | 29.2 | 29.2 | 0.03 |
| T10Eh | 28.6 | 26.3 | 26.8 | 26.8 | 0.01 |
| T10Wh | 30.0 | 27.2 | 27.8 | 27.8 | 0.02 |
| T10Wi | 29.2 | 26.6 | 27.2 | 27.2 | 0.01 |
| T11Ea | 53.7 | 41.5 | 43.3 | 43.6 | 0.34 |
| T11Wa | 58.9 | 44.6 | 46.5 | 46.9 | 0.39 |
| T11Eb | 41.9 | 33.9 | 35.0 | 35.2 | 0.21 |
| T11Wb | 46.7 | 37.0 | 38.3 | 38.6 | 0.26 |
| T11Ec | 36.6 | 30.7 | 31.5 | 31.6 | 0.15 |
| T11Wc | 39.3 | 32.4 | 33.3 | 33.4 | 0.18 |
| T11Ed | 32.1 | 27.9 | 28.5 | 28.6 | 0.10 |
| T11Wd | 33.7 | 28.9 | 29.5 | 29.7 | 0.11 |
| T11Ee | 27.9 | 25.3 | 25.6 | 25.7 | 0.05 |
| T11We | 28.6 | 25.8 | 26.1 | 26.2 | 0.06 |
| T11Ef | 25.8 | 24.0 | 24.3 | 24.3 | 0.03 |
| T11Wf | 26.3 | 24.4 | 24.6 | 24.6 | 0.03 |
| T11Eg | 24.5 | 23.2 | 23.4 | 23.4 | 0.02 |
| T11Wg | 24.9 | 23.5 | 23.7 | 23.7 | 0.02 |
| T11Eh | 24.0 | 22.9 | 23.1 | 23.1 | 0.01 |
| T11Wh | 24.4 | 23.2 | 23.4 | 23.4 | 0.01 |
| T11Ei | 23.7 | 22.7 | 22.9 | 22.9 | 0.01 |
| T11Wi | 24.2 | 23.1 | 23.2 | 23.2 | 0.01 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|--------------|--------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T12Wa | 191.7 | 132.1 | 134.8 | 134.6 | -0.16 |
| T12Wb | 157.0 | 109.1 | 111.2 | 111.1 | -0.13 |
| T12Wc | 111.3 | 79.0 | 80.4 | 80.3 | -0.09 |
| T12Wd | 84.1 | 61.3 | 62.3 | 62.2 | -0.06 |
| T12We | 56.3 | 43.1 | 43.7 | 43.7 | -0.04 |
| T12Wf | 42.3 | 34.1 | 34.5 | 34.5 | -0.03 |
| T12Wg | 33.0 | 28.2 | 28.5 | 28.5 | -0.02 |
| T12Wh | 29.2 | 25.9 | 26.1 | 26.0 | -0.01 |
| T12Wi | 27.2 | 24.7 | 24.8 | 24.8 | -0.01 |

Notes: **Bold** denotes exceedance of the 75 µg^m⁻³ daily mean NO_x AQO.

Table E.3 Predicted annual mean concentrations of NH₃ (µg^m⁻³)

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------------|------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T1Ea | 1.5 | 1.2 | 1.2 | 1.2 | -0.003 |
| T1Wa | 1.3 | 1.1 | 1.1 | 1.1 | -0.002 |
| T1Eb | 1.3 | 1.1 | 1.1 | 1.1 | -0.002 |
| T1Wb | 1.1 | 1.0 | 1.0 | 1.0 | -0.002 |
| T1Ec | 1.2 | 1.0 | 1.0 | 1.0 | -0.002 |
| T1Wc | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T1Ed | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T1Wd | 0.9 | 0.9 | 0.9 | 0.9 | -0.001 |
| T1Ee | 0.9 | 0.9 | 0.9 | 0.8 | -0.001 |
| T1We | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T1Ef | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T1Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T1Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T1Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T1Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T1Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|-----------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T1Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T1Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Ea | 1.6 | 1.3 | 1.3 | 1.3 | -0.003 |
| T2Wa | 1.3 | 1.1 | 1.1 | 1.1 | -0.002 |
| T2Eb | 1.4 | 1.1 | 1.2 | 1.2 | -0.002 |
| T2Wb | 1.1 | 1.0 | 1.0 | 1.0 | -0.001 |
| T2Ec | 1.2 | 1.0 | 1.0 | 1.0 | -0.002 |
| T2Wc | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T2Ed | 1.1 | 1.0 | 1.0 | 1.0 | -0.001 |
| T2Wd | 0.9 | 0.9 | 0.9 | 0.9 | -0.001 |
| T2Ee | 0.9 | 0.9 | 0.9 | 0.9 | -0.001 |
| T2We | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Ef | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T2Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Ea | 1.4 | 1.1 | 1.1 | 1.1 | -0.002 |
| T3Wa | 1.1 | 1.0 | 1.0 | 1.0 | -0.001 |
| T3Eb | 1.2 | 1.0 | 1.0 | 1.0 | -0.001 |
| T3Wb | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T3Ec | 1.1 | 1.0 | 1.0 | 1.0 | -0.001 |
| T3Wc | 0.9 | 0.9 | 0.9 | 0.9 | 0.000 |
| T3Ed | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T3Wd | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Ee | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3We | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|-----------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T3Ef | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T3Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Ea | 1.4 | 1.1 | 1.1 | 1.1 | -0.003 |
| T4Wa | 1.3 | 1.1 | 1.1 | 1.1 | -0.003 |
| T4Eb | 1.2 | 1.0 | 1.0 | 1.0 | -0.002 |
| T4Wb | 1.2 | 1.0 | 1.0 | 1.0 | -0.002 |
| T4Ec | 1.1 | 0.9 | 0.9 | 0.9 | -0.001 |
| T4Wc | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T4Ed | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T4Wd | 1.0 | 0.9 | 0.9 | 0.9 | -0.001 |
| T4Ee | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4We | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Ef | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T4Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Ea | 1.3 | 1.1 | 1.1 | 1.1 | 0.004 |
| T5Wa | 1.1 | 1.0 | 1.0 | 1.0 | 0.002 |
| T5Eb | 1.1 | 1.0 | 1.0 | 1.0 | 0.002 |
| T5Wb | 1.0 | 0.9 | 0.9 | 0.9 | 0.001 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------------|------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T5Ec | 1.0 | 0.9 | 0.9 | 0.9 | 0.002 |
| T5Wc | 0.9 | 0.9 | 0.9 | 0.9 | 0.001 |
| T5Ed | 0.9 | 0.9 | 0.9 | 0.9 | 0.001 |
| T5Wd | 0.9 | 0.8 | 0.8 | 0.8 | 0.001 |
| T5Ee | 0.9 | 0.8 | 0.8 | 0.8 | 0.001 |
| T5We | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Ef | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T5Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T6Ea | 1.1 | 1.0 | 1.0 | 1.0 | 0.005 |
| T6Wa | 1.0 | 0.9 | 0.9 | 0.9 | 0.003 |
| T6Eb | 1.0 | 0.9 | 0.9 | 0.9 | 0.004 |
| T6Wb | 0.9 | 0.8 | 0.9 | 0.9 | 0.002 |
| T6Ec | 1.0 | 0.9 | 0.9 | 0.9 | 0.003 |
| T6Wc | 0.9 | 0.8 | 0.8 | 0.8 | 0.001 |
| T6Ed | 0.9 | 0.8 | 0.9 | 0.9 | 0.002 |
| T6Wd | 0.8 | 0.8 | 0.8 | 0.8 | 0.001 |
| T6Ee | 0.8 | 0.8 | 0.8 | 0.8 | 0.001 |
| T6We | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T6Ef | 0.8 | 0.8 | 0.8 | 0.8 | 0.001 |
| T6Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T6Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T6Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T6Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T6Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|------|-----------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T6Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T6Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T7Ea | 2.1 | 1.6 | 1.6 | 1.6 | -0.009 |
| T7Wa | 1.5 | 1.2 | 1.3 | 1.3 | -0.005 |
| T7Eb | 1.7 | 1.4 | 1.4 | 1.4 | -0.007 |
| T7Wb | 1.3 | 1.1 | 1.1 | 1.1 | -0.004 |
| T7Ec | 1.5 | 1.2 | 1.2 | 1.2 | -0.005 |
| T7Wc | 1.1 | 1.0 | 1.0 | 1.0 | -0.002 |
| T7Ed | 1.3 | 1.1 | 1.1 | 1.1 | -0.003 |
| T7Wd | 1.0 | 0.9 | 0.9 | 0.9 | -0.002 |
| T7Ee | 1.0 | 0.9 | 0.9 | 0.9 | -0.002 |
| T7We | 0.9 | 0.8 | 0.8 | 0.8 | -0.001 |
| T7Ef | 0.9 | 0.9 | 0.9 | 0.9 | -0.001 |
| T7Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T7Eg | 0.9 | 0.8 | 0.8 | 0.8 | -0.001 |
| T7Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T7Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T7Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T7Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T7Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T8Wa | 1.5 | 1.2 | 1.2 | 1.2 | -0.005 |
| T8Wb | 1.3 | 1.1 | 1.1 | 1.1 | -0.003 |
| T8Wc | 1.1 | 1.0 | 1.0 | 1.0 | -0.002 |
| T8Wd | 1.0 | 0.9 | 0.9 | 0.9 | -0.002 |
| T8We | 0.9 | 0.8 | 0.8 | 0.8 | -0.001 |
| T8Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T8Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T8Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T8Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Ea | 1.4 | 1.2 | 1.2 | 1.2 | 0.002 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|-------|-----------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T9Wa | 1.3 | 1.1 | 1.2 | 1.2 | 0.001 |
| T9Eb | 1.2 | 1.0 | 1.1 | 1.1 | 0.001 |
| T9Wb | 1.1 | 1.0 | 1.0 | 1.0 | 0.001 |
| T9Ec | 1.1 | 1.0 | 1.0 | 1.0 | 0.001 |
| T9Wc | 1.0 | 0.9 | 0.9 | 0.9 | 0.001 |
| T9Ed | 1.0 | 0.9 | 0.9 | 0.9 | 0.001 |
| T9Wd | 0.9 | 0.9 | 0.9 | 0.9 | 0.001 |
| T9Ee | 0.9 | 0.8 | 0.9 | 0.9 | <0.001 |
| T9We | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Ef | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T9Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T10Ea | 1.8 | 1.4 | 1.5 | 1.5 | 0.003 |
| T10Wa | 1.4 | 1.2 | 1.2 | 1.2 | 0.002 |
| T10Eb | 1.6 | 1.2 | 1.3 | 1.3 | 0.003 |
| T10Wb | 1.2 | 1.0 | 1.1 | 1.1 | 0.001 |
| T10Ec | 1.3 | 1.1 | 1.2 | 1.2 | 0.002 |
| T10Wc | 1.1 | 0.9 | 1.0 | 1.0 | 0.001 |
| T10Ed | 1.2 | 1.0 | 1.0 | 1.0 | 0.001 |
| T10Wd | 1.0 | 0.9 | 0.9 | 0.9 | 0.001 |
| T10Ee | 1.0 | 0.9 | 0.9 | 0.9 | 0.001 |
| T10We | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T10Ef | 0.9 | 0.8 | 0.8 | 0.8 | <0.001 |
| T10Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T10Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|--------------|------------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T10Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T10Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T10Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T10Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Ea | 1.0 | 0.9 | 1.0 | 1.0 | 0.003 |
| T11Wa | 1.1 | 1.0 | 1.0 | 1.0 | 0.003 |
| T11Eb | 0.9 | 0.9 | 0.9 | 0.9 | 0.002 |
| T11Wb | 1.0 | 0.9 | 0.9 | 0.9 | 0.002 |
| T11Ec | 0.9 | 0.8 | 0.8 | 0.8 | 0.001 |
| T11Wc | 0.9 | 0.9 | 0.9 | 0.9 | 0.002 |
| T11Ed | 0.8 | 0.8 | 0.8 | 0.8 | 0.001 |
| T11Wd | 0.9 | 0.8 | 0.8 | 0.8 | 0.001 |
| T11Ee | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11We | 0.8 | 0.8 | 0.8 | 0.8 | 0.001 |
| T11Ef | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Wf | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Eg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Eh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Ei | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T11Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T12Wa | 2.3 | 1.7 | 1.8 | 1.8 | -0.001 |
| T12Wb | 2.0 | 1.5 | 1.5 | 1.5 | -0.001 |
| T12Wc | 1.6 | 1.3 | 1.3 | 1.3 | -0.001 |
| T12Wd | 1.3 | 1.1 | 1.1 | 1.1 | -0.001 |
| T12We | 1.1 | 0.9 | 0.9 | 0.9 | <0.001 |
| T12Wf | 0.9 | 0.9 | 0.9 | 0.9 | <0.001 |
| T12Wg | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |
| T12Wh | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B –2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
|--------------|-----------|-------------------------------------|--------------------------------|-----------------------------------|------------------|
| T12Wi | 0.8 | 0.8 | 0.8 | 0.8 | <0.001 |

Note: **Bold** denotes exceedance of the 1 µgm⁻³ target concentration where certain species are present.

Table E.4 Total nitrogen deposition at each transect point (kg N/ha/yr)

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the 10 kgN/ha/yr min critical load |
|-------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T1Ea | 24.83 | 20.79 | 20.71 | 20.67 | -0.044 | 0% |
| T1Wa | 22.21 | 19.11 | 19.06 | 19.02 | -0.032 | 0% |
| T1Eb | 22.10 | 19.07 | 19.01 | 18.98 | -0.032 | 0% |
| T1Wb | 19.77 | 17.59 | 17.56 | 17.53 | -0.024 | 0% |
| T1Ec | 19.98 | 17.75 | 17.71 | 17.69 | -0.024 | 0% |
| T1Wc | 18.11 | 16.58 | 16.55 | 16.54 | -0.014 | 0% |
| T1Ed | 18.27 | 16.69 | 16.67 | 16.65 | -0.017 | 0% |
| T1Wd | 16.85 | 15.80 | 15.79 | 15.78 | -0.011 | 0% |
| T1Ee | 16.41 | 15.55 | 15.54 | 15.53 | -0.008 | 0% |
| T1We | 15.60 | 15.05 | 15.05 | 15.04 | -0.006 | 0% |
| T1Ef | 15.52 | 15.00 | 15.00 | 15.00 | -0.006 | 0% |
| T1Wf | 15.03 | 14.70 | 14.71 | 14.71 | -0.002 | 0% |
| T1Eg | 14.99 | 14.68 | 14.69 | 14.68 | -0.004 | 0% |
| T1Wg | 14.71 | 14.51 | 14.52 | 14.51 | -0.001 | 0% |
| T1Eh | 14.81 | 14.57 | 14.57 | 14.57 | -0.001 | 0% |
| T1Wh | 14.60 | 14.44 | 14.45 | 14.45 | -0.001 | 0% |
| T1Ei | 14.70 | 14.51 | 14.51 | 14.51 | -0.001 | 0% |
| T1Wi | 14.56 | 14.42 | 14.43 | 14.43 | -0.001 | 0% |
| T2Ea | 26.19 | 21.66 | 21.82 | 21.77 | -0.044 | 0% |
| T2Wa | 21.92 | 18.92 | 19.03 | 19.00 | -0.030 | 0% |
| T2Eb | 23.27 | 19.82 | 19.94 | 19.91 | -0.033 | 0% |
| T2Wb | 19.48 | 17.41 | 17.48 | 17.47 | -0.019 | 0% |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the 10 kgN/ha/yr min critical load |
|------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T2Ec | 20.87 | 18.32 | 18.40 | 18.38 | -0.025 | 0% |
| T2Wc | 17.92 | 16.46 | 16.51 | 16.50 | -0.013 | 0% |
| T2Ed | 18.94 | 17.11 | 17.18 | 17.16 | -0.015 | 0% |
| T2Wd | 16.76 | 15.75 | 15.79 | 15.78 | -0.008 | 0% |
| T2Ee | 16.83 | 15.81 | 15.85 | 15.84 | -0.008 | 0% |
| T2We | 15.60 | 15.05 | 15.07 | 15.07 | -0.002 | 0% |
| T2Ef | 15.78 | 15.17 | 15.19 | 15.19 | -0.006 | 0% |
| T2Wf | 15.06 | 14.73 | 14.74 | 14.74 | -0.001 | 0% |
| T2Eg | 15.16 | 14.79 | 14.80 | 14.80 | -0.001 | 0% |
| T2Wg | 14.76 | 14.54 | 14.56 | 14.55 | -0.004 | 0% |
| T2Eh | 14.94 | 14.65 | 14.67 | 14.66 | -0.001 | 0% |
| T2Wh | 14.65 | 14.47 | 14.48 | 14.48 | <0.001 | 0% |
| T2Ei | 14.82 | 14.58 | 14.59 | 14.59 | -0.004 | 0% |
| T2Wi | 14.59 | 14.44 | 14.45 | 14.45 | <0.001 | 0% |
| T3Ea | 23.19 | 19.76 | 19.69 | 19.67 | -0.027 | 0% |
| T3Wa | 19.27 | 17.29 | 17.25 | 17.24 | -0.015 | 0% |
| T3Eb | 21.03 | 18.42 | 18.37 | 18.34 | -0.021 | 0% |
| T3Wb | 17.79 | 16.39 | 16.36 | 16.35 | -0.011 | 0% |
| T3Ec | 19.27 | 17.32 | 17.28 | 17.27 | -0.013 | 0% |
| T3Wc | 16.78 | 15.77 | 15.75 | 15.75 | -0.006 | 0% |
| T3Ed | 17.80 | 16.41 | 16.39 | 16.38 | -0.011 | 0% |
| T3Wd | 15.99 | 15.29 | 15.28 | 15.28 | -0.005 | 0% |
| T3Ee | 16.19 | 15.42 | 15.41 | 15.41 | -0.005 | 0% |
| T3We | 15.19 | 14.81 | 14.81 | 14.80 | -0.001 | 0% |
| T3Ef | 15.41 | 14.94 | 14.94 | 14.94 | -0.001 | 0% |
| T3Wf | 14.82 | 14.58 | 14.59 | 14.59 | -0.001 | 0% |
| T3Eg | 14.94 | 14.65 | 14.66 | 14.66 | -0.001 | 0% |
| T3Wg | 14.61 | 14.45 | 14.46 | 14.46 | <0.001 | 0% |
| T3Eh | 14.77 | 14.55 | 14.56 | 14.56 | -0.001 | 0% |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the 10 kgN/ha/yr min critical load |
|------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T3Wh | 14.53 | 14.41 | 14.41 | 14.41 | <0.001 | 0% |
| T3Ei | 14.68 | 14.50 | 14.50 | 14.50 | -0.001 | 0% |
| T3Wi | 14.49 | 14.38 | 14.39 | 14.39 | <0.001 | 0% |
| T4Ea | 23.12 | 19.71 | 19.70 | 19.66 | -0.035 | 0% |
| T4Wa | 22.75 | 19.51 | 19.49 | 19.46 | -0.031 | 0% |
| T4Eb | 20.50 | 18.07 | 18.06 | 18.04 | -0.022 | 0% |
| T4Wb | 20.18 | 17.89 | 17.88 | 17.86 | -0.024 | 0% |
| T4Ec | 18.76 | 16.99 | 16.99 | 16.97 | -0.017 | 0% |
| T4Wc | 18.47 | 16.82 | 16.82 | 16.81 | -0.013 | 0% |
| T4Ed | 17.35 | 16.13 | 16.13 | 16.12 | -0.011 | 0% |
| T4Wd | 17.13 | 15.99 | 15.99 | 15.98 | -0.010 | 0% |
| T4Ee | 15.90 | 15.23 | 15.24 | 15.23 | -0.007 | 0% |
| T4We | 15.76 | 15.15 | 15.15 | 15.15 | -0.003 | 0% |
| T4Ef | 15.21 | 14.82 | 14.83 | 14.82 | -0.002 | 0% |
| T4Wf | 15.12 | 14.76 | 14.77 | 14.76 | -0.002 | 0% |
| T4Eg | 14.82 | 14.58 | 14.59 | 14.59 | -0.001 | 0% |
| T4Wg | 14.75 | 14.54 | 14.55 | 14.54 | -0.001 | 0% |
| T4Eh | 14.68 | 14.50 | 14.50 | 14.50 | -0.001 | 0% |
| T4Wh | 14.63 | 14.46 | 14.47 | 14.47 | <0.001 | 0% |
| T4Ei | 14.61 | 14.45 | 14.46 | 14.46 | -0.001 | 0% |
| T4Wi | 14.56 | 14.42 | 14.43 | 14.43 | -0.003 | 0% |
| T5Ea | 21.50 | 18.69 | 19.01 | 19.08 | 0.070 | 0% |
| T5Wa | 18.83 | 17.04 | 17.24 | 17.28 | 0.043 | 0% |
| T5Eb | 19.42 | 17.40 | 17.62 | 17.67 | 0.051 | 0% |
| T5Wb | 17.32 | 16.11 | 16.24 | 16.27 | 0.028 | 0% |
| T5Ec | 17.98 | 16.51 | 16.68 | 16.71 | 0.036 | 0% |
| T5Wc | 16.47 | 15.59 | 15.68 | 15.70 | 0.022 | 0% |
| T5Ed | 16.86 | 15.82 | 15.93 | 15.96 | 0.026 | 0% |
| T5Wd | 15.81 | 15.18 | 15.25 | 15.26 | 0.013 | 0% |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the 10 kgN/ha/yr min critical load |
|-------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T5Ee | 15.73 | 15.13 | 15.20 | 15.21 | 0.013 | 0% |
| T5We | 15.16 | 14.79 | 14.82 | 14.83 | 0.005 | 0% |
| T5Ef | 15.18 | 14.80 | 14.84 | 14.85 | 0.008 | 0% |
| T5Wf | 14.86 | 14.60 | 14.63 | 14.63 | 0.004 | 0% |
| T5Eg | 14.87 | 14.61 | 14.63 | 14.64 | 0.001 | 0% |
| T5Wg | 14.69 | 14.50 | 14.51 | 14.51 | <0.001 | 0% |
| T5Eh | 14.76 | 14.54 | 14.56 | 14.56 | 0.003 | 0% |
| T5Wh | 14.62 | 14.46 | 14.47 | 14.47 | <0.001 | 0% |
| T5Ei | 14.69 | 14.50 | 14.52 | 14.52 | <0.001 | 0% |
| T5Wi | 14.61 | 14.45 | 14.47 | 14.46 | <0.001 | 0% |
| T6Ea | 19.46 | 17.43 | 17.62 | 17.70 | 0.078 | 0% |
| T6Wa | 17.20 | 16.03 | 16.15 | 16.19 | 0.043 | 0% |
| T6Eb | 18.18 | 16.63 | 16.78 | 16.84 | 0.059 | 0% |
| T6Wb | 16.34 | 15.51 | 15.58 | 15.61 | 0.028 | 0% |
| T6Ec | 17.19 | 16.03 | 16.14 | 16.18 | 0.043 | 0% |
| T6Wc | 15.78 | 15.17 | 15.23 | 15.25 | 0.021 | 0% |
| T6Ed | 16.33 | 15.50 | 15.58 | 15.61 | 0.028 | 0% |
| T6Wd | 15.35 | 14.90 | 14.94 | 14.96 | 0.012 | 0% |
| T6Ee | 15.42 | 14.95 | 14.99 | 15.00 | 0.016 | 0% |
| T6We | 14.90 | 14.63 | 14.65 | 14.66 | 0.006 | 0% |
| T6Ef | 14.99 | 14.68 | 14.71 | 14.72 | 0.010 | 0% |
| T6Wf | 14.69 | 14.50 | 14.52 | 14.53 | 0.005 | 0% |
| T6Eg | 14.72 | 14.52 | 14.54 | 14.54 | 0.005 | 0% |
| T6Wg | 14.57 | 14.43 | 14.44 | 14.44 | 0.001 | 0% |
| T6Eh | 14.63 | 14.46 | 14.48 | 14.48 | 0.004 | 0% |
| T6Wh | 14.52 | 14.40 | 14.41 | 14.41 | 0.001 | 0% |
| T6Ei | 14.58 | 14.43 | 14.45 | 14.45 | 0.001 | 0% |
| T6Wi | 14.49 | 14.38 | 14.39 | 14.39 | <0.001 | 0% |
| T7Ea | 32.53 | 25.87 | 26.35 | 26.24 | -0.111 | 0% |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the 10 kgN/ha/yr min critical load |
|------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T7Wa | 25.33 | 21.12 | 21.43 | 21.36 | -0.068 | 0% |
| T7Eb | 28.32 | 23.14 | 23.52 | 23.44 | -0.085 | 0% |
| T7Wb | 21.80 | 18.90 | 19.11 | 19.07 | -0.045 | 0% |
| T7Ec | 24.72 | 20.82 | 21.11 | 21.05 | -0.065 | 0% |
| T7Wc | 19.58 | 17.52 | 17.67 | 17.64 | -0.031 | 0% |
| T7Ed | 21.67 | 18.88 | 19.09 | 19.04 | -0.044 | 0% |
| T7Wd | 17.88 | 16.46 | 16.57 | 16.55 | -0.021 | 0% |
| T7Ee | 18.26 | 16.73 | 16.85 | 16.82 | -0.026 | 0% |
| T7We | 16.12 | 15.38 | 15.44 | 15.43 | -0.012 | 0% |
| T7Ef | 16.57 | 15.67 | 15.74 | 15.73 | -0.014 | 0% |
| T7Wf | 15.30 | 14.88 | 14.92 | 14.91 | -0.003 | 0% |
| T7Eg | 15.55 | 15.03 | 15.08 | 15.07 | -0.004 | 0% |
| T7Wg | 14.84 | 14.59 | 14.62 | 14.62 | -0.001 | 0% |
| T7Eh | 15.17 | 14.80 | 14.84 | 14.83 | -0.005 | 0% |
| T7Wh | 14.67 | 14.49 | 14.52 | 14.52 | -0.001 | 0% |
| T7Ei | 14.98 | 14.68 | 14.71 | 14.71 | -0.002 | 0% |
| T7Wi | 14.59 | 14.44 | 14.46 | 14.46 | <0.001 | 0% |
| T8Wa | 24.77 | 20.82 | 21.11 | 21.05 | -0.062 | 0% |
| T8Wb | 21.69 | 18.87 | 19.08 | 19.04 | -0.044 | 0% |
| T8Wc | 19.62 | 17.56 | 17.72 | 17.69 | -0.030 | 0% |
| T8Wd | 17.97 | 16.53 | 16.64 | 16.63 | -0.018 | 0% |
| T8We | 16.24 | 15.45 | 15.53 | 15.52 | -0.009 | 0% |
| T8Wf | 15.42 | 14.95 | 15.00 | 15.00 | -0.003 | 0% |
| T8Wg | 14.95 | 14.66 | 14.70 | 14.70 | -0.001 | 0% |
| T8Wh | 14.78 | 14.56 | 14.59 | 14.59 | 0.000 | 0% |
| T8Wi | 14.70 | 14.51 | 14.54 | 14.54 | 0.003 | 0% |
| T9Ea | 23.94 | 20.24 | 21.12 | 21.17 | 0.048 | 0% |
| T9Wa | 22.16 | 19.10 | 19.83 | 19.87 | 0.043 | 0% |
| T9Eb | 21.03 | 18.41 | 19.03 | 19.06 | 0.035 | 0% |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the 10 kgN/ha/yr min critical load |
|--------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T9Wb | 19.64 | 17.54 | 18.03 | 18.06 | 0.031 | 0% |
| T9Ec | 19.21 | 17.28 | 17.73 | 17.76 | 0.027 | 0% |
| T9Wc | 18.06 | 16.55 | 16.91 | 16.93 | 0.020 | 0% |
| T9Ed | 17.71 | 16.35 | 16.67 | 16.69 | 0.017 | 0% |
| T9Wd | 16.87 | 15.82 | 16.07 | 16.08 | 0.013 | 0% |
| T9Ee | 16.13 | 15.38 | 15.55 | 15.57 | 0.012 | 0% |
| T9We | 15.64 | 15.07 | 15.20 | 15.21 | 0.008 | 0% |
| T9Ef | 15.37 | 14.92 | 15.02 | 15.03 | 0.005 | 0% |
| T9Wf | 15.07 | 14.73 | 14.81 | 14.82 | 0.008 | 0% |
| T9Eg | 14.92 | 14.64 | 14.70 | 14.71 | 0.004 | 0% |
| T9Wg | 14.75 | 14.53 | 14.59 | 14.59 | 0.001 | 0% |
| T9Eh | 14.76 | 14.54 | 14.59 | 14.59 | 0.004 | 0% |
| T9Wh | 14.63 | 14.46 | 14.51 | 14.51 | 0.001 | 0% |
| T9Ei | 14.67 | 14.49 | 14.53 | 14.53 | 0.001 | 0% |
| T9Wi | 14.57 | 14.43 | 14.46 | 14.46 | 0.001 | 0% |
| T10Ea | 29.46 | 23.63 | 24.52 | 24.56 | 0.038 | 0% |
| T10Wa | 23.64 | 20.01 | 20.57 | 20.59 | 0.022 | 0% |
| T10Eb | 25.73 | 21.28 | 21.96 | 21.99 | 0.029 | 0% |
| T10Wb | 20.43 | 18.02 | 18.38 | 18.40 | 0.016 | 0% |
| T10Ec | 22.48 | 19.26 | 19.75 | 19.77 | 0.020 | 0% |
| T10Wc | 18.63 | 16.91 | 17.17 | 17.18 | 0.010 | 0% |
| T10Ed | 19.95 | 17.70 | 18.04 | 18.05 | 0.016 | 0% |
| T10Wd | 17.27 | 16.07 | 16.25 | 16.25 | 0.008 | 0% |
| T10Ee | 17.24 | 16.05 | 16.22 | 16.23 | 0.008 | 0% |
| T10We | 15.85 | 15.20 | 15.30 | 15.30 | 0.003 | 0% |
| T10Ef | 15.98 | 15.28 | 15.38 | 15.39 | 0.006 | 0% |
| T10Wf | 15.19 | 14.80 | 14.86 | 14.86 | 0.005 | 0% |
| T10Eg | 15.22 | 14.82 | 14.88 | 14.89 | 0.005 | 0% |
| T10Wg | 14.79 | 14.56 | 14.59 | 14.60 | 0.001 | 0% |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the 10 kgN/ha/yr min critical load |
|-------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T10Eh | 14.95 | 14.66 | 14.70 | 14.70 | 0.001 | 0% |
| T10Wh | 15.64 | 14.47 | 14.50 | 14.50 | 0.001 | 0% |
| T10Wi | 16.59 | 14.44 | 14.46 | 14.46 | 0.001 | 0% |
| T11Ea | 21.46 | 16.80 | 17.03 | 17.07 | 0.047 | 0% |
| T11Wa | 23.01 | 17.17 | 17.42 | 17.47 | 0.053 | 0% |
| T11Eb | 21.93 | 15.86 | 16.01 | 16.04 | 0.029 | 0% |
| T11Wb | 23.49 | 16.22 | 16.40 | 16.43 | 0.035 | 0% |
| T11Ec | 23.15 | 15.39 | 15.49 | 15.51 | 0.022 | 0% |
| T11Wc | 24.58 | 15.66 | 15.79 | 15.81 | 0.024 | 0% |
| T11Ed | 24.49 | 14.98 | 15.05 | 15.07 | 0.012 | 0% |
| T11Wd | 25.86 | 15.22 | 15.31 | 15.32 | 0.017 | 0% |
| T11Ee | 25.90 | 14.63 | 14.67 | 14.67 | 0.006 | 0% |
| T11We | 27.17 | 14.80 | 14.85 | 14.86 | 0.007 | 0% |
| T11Ef | 27.65 | 14.48 | 14.50 | 14.50 | 0.001 | 0% |
| T11Wf | 28.85 | 14.60 | 14.63 | 14.64 | 0.006 | 0% |
| T11Eg | 29.52 | 14.40 | 14.42 | 14.42 | 0.001 | 0% |
| T11Wg | 30.65 | 14.48 | 14.50 | 14.50 | 0.001 | 0% |
| T11Eh | 31.48 | 14.37 | 14.39 | 14.39 | <0.001 | 0% |
| T11Wh | 32.58 | 14.43 | 14.45 | 14.46 | 0.001 | 0% |
| T11Ei | 33.46 | 14.36 | 14.38 | 14.38 | <0.001 | 0% |
| T11Wi | 34.54 | 14.41 | 14.43 | 14.43 | 0.004 | 0% |
| T12Wa | 56.64 | 28.05 | 28.39 | 28.38 | -0.008 | 0% |
| T12Wb | 53.29 | 25.15 | 25.42 | 25.42 | -0.003 | 0% |
| T12Wc | 48.70 | 21.48 | 21.67 | 21.67 | -0.003 | 0% |
| T12Wd | 46.24 | 19.25 | 19.38 | 19.38 | -0.004 | 0% |
| T12We | 43.50 | 16.87 | 16.94 | 16.94 | -0.002 | 0% |
| T12Wf | 42.62 | 15.69 | 15.73 | 15.73 | -0.001 | 0% |
| T12Wg | 42.48 | 14.98 | 15.01 | 15.01 | -0.001 | 0% |
| T12Wh | 43.07 | 14.73 | 14.75 | 14.75 | <0.001 | 0% |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) | As a % of the 10 kgN/ha/yr min critical load |
|--------------|-----------|----------------------------------|------------------------------|--------------------------------|------------------|--|
| T12Wi | 43.87 | 14.61 | 14.63 | 14.63 | <0.001 | 0% |

Notes: **Bold** denotes change of greater than 1% of critical load.

Table E.5 Total acid deposition at modelled transect points (keq N / ha/yr)

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) | As a % of the CL Function |
|-------------|-----------|----------------------------------|------------------------------|--------------------------------|------------------|---------------------------|
| T1Ea | 1.77 | 1.48 | 1.47 | 1.47 | -0.003 | 0 |
| T1Wa | 1.58 | 1.36 | 1.36 | 1.35 | -0.002 | 0 |
| T1Eb | 1.57 | 1.36 | 1.35 | 1.35 | -0.002 | 0 |
| T1Wb | 1.41 | 1.25 | 1.25 | 1.25 | -0.002 | 0 |
| T1Ec | 1.42 | 1.26 | 1.26 | 1.26 | -0.002 | 0 |
| T1Wc | 1.29 | 1.18 | 1.18 | 1.18 | -0.001 | 0 |
| T1Ed | 1.30 | 1.19 | 1.19 | 1.18 | -0.001 | 0 |
| T1Wd | 1.20 | 1.12 | 1.12 | 1.12 | -0.001 | 0 |
| T1Ee | 1.17 | 1.11 | 1.11 | 1.10 | -0.001 | 0 |
| T1We | 1.11 | 1.07 | 1.07 | 1.07 | <0.001 | 0 |
| T1Ef | 1.10 | 1.07 | 1.07 | 1.07 | <0.001 | 0 |
| T1Wf | 1.07 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |
| T1Eg | 1.07 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T1Wg | 1.05 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T1Eh | 1.05 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T1Wh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T1Ei | 1.05 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T1Wi | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T2Ea | 1.86 | 1.54 | 1.55 | 1.55 | -0.003 | 0 |
| T2Wa | 1.56 | 1.35 | 1.35 | 1.35 | -0.002 | 0 |
| T2Eb | 1.66 | 1.41 | 1.42 | 1.42 | -0.002 | 0 |
| T2Wb | 1.39 | 1.24 | 1.24 | 1.24 | -0.001 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the CL Function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T2Ec | 1.49 | 1.30 | 1.31 | 1.31 | -0.002 | 0 |
| T2Wc | 1.27 | 1.17 | 1.17 | 1.17 | -0.001 | 0 |
| T2Ed | 1.35 | 1.22 | 1.22 | 1.22 | -0.001 | 0 |
| T2Wd | 1.19 | 1.12 | 1.12 | 1.12 | -0.001 | 0 |
| T2Ee | 1.20 | 1.12 | 1.13 | 1.13 | -0.001 | 0 |
| T2We | 1.11 | 1.07 | 1.07 | 1.07 | <0.001 | 0 |
| T2Ef | 1.12 | 1.08 | 1.08 | 1.08 | <0.001 | 0 |
| T2Wf | 1.07 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |
| T2Eg | 1.08 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |
| T2Wg | 1.05 | 1.03 | 1.04 | 1.04 | <0.001 | 0 |
| T2Eh | 1.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T2Wh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T2Ei | 1.05 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T2Wi | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T3Ea | 1.65 | 1.41 | 1.40 | 1.40 | -0.002 | 0 |
| T3Wa | 1.37 | 1.23 | 1.23 | 1.23 | -0.001 | 0 |
| T3Eb | 1.50 | 1.31 | 1.31 | 1.31 | -0.001 | 0 |
| T3Wb | 1.27 | 1.17 | 1.16 | 1.16 | -0.001 | 0 |
| T3Ec | 1.37 | 1.23 | 1.23 | 1.23 | -0.001 | 0 |
| T3Wc | 1.19 | 1.12 | 1.12 | 1.12 | <0.001 | 0 |
| T3Ed | 1.27 | 1.17 | 1.17 | 1.17 | -0.001 | 0 |
| T3Wd | 1.14 | 1.09 | 1.09 | 1.09 | <0.001 | 0 |
| T3Ee | 1.15 | 1.10 | 1.10 | 1.10 | <0.001 | 0 |
| T3We | 1.08 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |
| T3Ef | 1.10 | 1.06 | 1.06 | 1.06 | <0.001 | 0 |
| T3Wf | 1.05 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T3Eg | 1.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T3Wg | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T3Eh | 1.05 | 1.03 | 1.04 | 1.04 | <0.001 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the CL Function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T3Wh | 1.03 | 1.02 | 1.03 | 1.03 | <0.001 | 0 |
| T3Ei | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T3Wi | 1.03 | 1.02 | 1.02 | 1.02 | <0.001 | 0 |
| T4Ea | 1.65 | 1.40 | 1.40 | 1.40 | -0.002 | 0 |
| T4Wa | 1.62 | 1.39 | 1.39 | 1.38 | -0.002 | 0 |
| T4Eb | 1.46 | 1.29 | 1.29 | 1.28 | -0.002 | 0 |
| T4Wb | 1.44 | 1.27 | 1.27 | 1.27 | -0.002 | 0 |
| T4Ec | 1.33 | 1.21 | 1.21 | 1.21 | -0.001 | 0 |
| T4Wc | 1.31 | 1.20 | 1.20 | 1.20 | -0.001 | 0 |
| T4Ed | 1.23 | 1.15 | 1.15 | 1.15 | -0.001 | 0 |
| T4Wd | 1.22 | 1.14 | 1.14 | 1.14 | -0.001 | 0 |
| T4Ee | 1.13 | 1.08 | 1.08 | 1.08 | <0.001 | 0 |
| T4We | 1.12 | 1.08 | 1.08 | 1.08 | <0.001 | 0 |
| T4Ef | 1.08 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |
| T4Wf | 1.08 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |
| T4Eg | 1.05 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T4Wg | 1.05 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T4Eh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T4Wh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T4Ei | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T4Wi | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T5Ea | 1.53 | 1.33 | 1.35 | 1.36 | 0.005 | 0 |
| T5Wa | 1.34 | 1.21 | 1.23 | 1.23 | 0.003 | 0 |
| T5Eb | 1.38 | 1.24 | 1.25 | 1.26 | 0.004 | 0 |
| T5Wb | 1.23 | 1.15 | 1.16 | 1.16 | 0.002 | 0 |
| T5Ec | 1.28 | 1.17 | 1.19 | 1.19 | 0.003 | 0 |
| T5Wc | 1.17 | 1.11 | 1.12 | 1.12 | 0.002 | 0 |
| T5Ed | 1.20 | 1.13 | 1.13 | 1.14 | 0.002 | 0 |
| T5Wd | 1.12 | 1.08 | 1.08 | 1.09 | 0.001 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the CL Function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T5Ee | 1.12 | 1.08 | 1.08 | 1.08 | 0.001 | 0 |
| T5We | 1.08 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |
| T5Ef | 1.08 | 1.05 | 1.06 | 1.06 | 0.001 | 0 |
| T5Wf | 1.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T5Eg | 1.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T5Wg | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T5Eh | 1.05 | 1.03 | 1.04 | 1.04 | <0.001 | 0 |
| T5Wh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T5Ei | 1.05 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T5Wi | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T6Ea | 1.38 | 1.24 | 1.25 | 1.26 | 0.006 | 0 |
| T6Wa | 1.22 | 1.14 | 1.15 | 1.15 | 0.003 | 0 |
| T6Eb | 1.29 | 1.18 | 1.19 | 1.20 | 0.004 | 0 |
| T6Wb | 1.16 | 1.10 | 1.11 | 1.11 | 0.002 | 0 |
| T6Ec | 1.22 | 1.14 | 1.15 | 1.15 | 0.003 | 0 |
| T6Wc | 1.12 | 1.08 | 1.08 | 1.08 | 0.002 | 0 |
| T6Ed | 1.16 | 1.10 | 1.11 | 1.11 | 0.002 | 0 |
| T6Wd | 1.09 | 1.06 | 1.06 | 1.06 | 0.001 | 0 |
| T6Ee | 1.10 | 1.06 | 1.07 | 1.07 | 0.001 | 0 |
| T6We | 1.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T6Ef | 1.07 | 1.04 | 1.05 | 1.05 | 0.001 | 0 |
| T6Wf | 1.05 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T6Eg | 1.05 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T6Wg | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T6Eh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T6Wh | 1.03 | 1.02 | 1.03 | 1.03 | <0.001 | 0 |
| T6Ei | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T6Wi | 1.03 | 1.02 | 1.02 | 1.02 | <0.001 | 0 |
| T7Ea | 2.32 | 1.84 | 1.88 | 1.87 | -0.008 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the CL Function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T7Wa | 1.80 | 1.50 | 1.53 | 1.52 | -0.005 | 0 |
| T7Eb | 2.02 | 1.65 | 1.67 | 1.67 | -0.006 | 0 |
| T7Wb | 1.55 | 1.34 | 1.36 | 1.36 | -0.003 | 0 |
| T7Ec | 1.76 | 1.48 | 1.50 | 1.50 | -0.005 | 0 |
| T7Wc | 1.39 | 1.25 | 1.26 | 1.25 | -0.002 | 0 |
| T7Ed | 1.54 | 1.34 | 1.36 | 1.35 | -0.003 | 0 |
| T7Wd | 1.27 | 1.17 | 1.18 | 1.18 | -0.002 | 0 |
| T7Ee | 1.30 | 1.19 | 1.20 | 1.20 | -0.002 | 0 |
| T7We | 1.15 | 1.09 | 1.10 | 1.10 | -0.001 | 0 |
| T7Ef | 1.18 | 1.11 | 1.12 | 1.12 | -0.001 | 0 |
| T7Wf | 1.09 | 1.06 | 1.06 | 1.06 | <0.001 | 0 |
| T7Eg | 1.11 | 1.07 | 1.07 | 1.07 | <0.001 | 0 |
| T7Wg | 1.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T7Eh | 1.08 | 1.05 | 1.06 | 1.05 | <0.001 | 0 |
| T7Wh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T7Ei | 1.07 | 1.04 | 1.05 | 1.05 | <0.001 | 0 |
| T7Wi | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T8Wa | 1.76 | 1.48 | 1.50 | 1.50 | -0.004 | 0 |
| T8Wb | 1.54 | 1.34 | 1.36 | 1.35 | -0.003 | 0 |
| T8Wc | 1.40 | 1.25 | 1.26 | 1.26 | -0.002 | 0 |
| T8Wd | 1.28 | 1.18 | 1.18 | 1.18 | -0.001 | 0 |
| T8We | 1.16 | 1.10 | 1.10 | 1.10 | -0.001 | 0 |
| T8Wf | 1.10 | 1.06 | 1.07 | 1.07 | <0.001 | 0 |
| T8Wg | 1.06 | 1.04 | 1.05 | 1.05 | <0.001 | 0 |
| T8Wh | 1.05 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T8Wi | 1.05 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T9Ea | 1.70 | 1.44 | 1.50 | 1.51 | 0.003 | 0 |
| T9Wa | 1.58 | 1.36 | 1.41 | 1.41 | 0.003 | 0 |
| T9Eb | 1.50 | 1.31 | 1.35 | 1.36 | 0.003 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the CL Function |
|-------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T9Wb | 1.40 | 1.25 | 1.28 | 1.29 | 0.002 | 0 |
| T9Ec | 1.37 | 1.23 | 1.26 | 1.26 | 0.002 | 0 |
| T9Wc | 1.28 | 1.18 | 1.20 | 1.20 | 0.001 | 0 |
| T9Ed | 1.26 | 1.16 | 1.19 | 1.19 | 0.001 | 0 |
| T9Wd | 1.20 | 1.13 | 1.14 | 1.14 | 0.001 | 0 |
| T9Ee | 1.15 | 1.09 | 1.11 | 1.11 | 0.001 | 0 |
| T9We | 1.11 | 1.07 | 1.08 | 1.08 | 0.001 | 0 |
| T9Ef | 1.09 | 1.06 | 1.07 | 1.07 | <0.001 | 0 |
| T9Wf | 1.07 | 1.05 | 1.05 | 1.05 | 0.001 | 0 |
| T9Eg | 1.06 | 1.04 | 1.05 | 1.05 | <0.001 | 0 |
| T9Wg | 1.05 | 1.03 | 1.04 | 1.04 | <0.001 | 0 |
| T9Eh | 1.05 | 1.03 | 1.04 | 1.04 | <0.001 | 0 |
| T9Wh | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T9Ei | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T9Wi | 1.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T10Ea | 2.10 | 1.68 | 1.75 | 1.75 | 0.003 | 0 |
| T10Wa | 1.68 | 1.42 | 1.46 | 1.47 | 0.002 | 0 |
| T10Eb | 1.83 | 1.51 | 1.56 | 1.56 | 0.002 | 0 |
| T10Wb | 1.45 | 1.28 | 1.31 | 1.31 | 0.001 | 0 |
| T10Ec | 1.60 | 1.37 | 1.41 | 1.41 | 0.001 | 0 |
| T10Wc | 1.33 | 1.20 | 1.22 | 1.22 | 0.001 | 0 |
| T10Ed | 1.42 | 1.26 | 1.28 | 1.28 | 0.001 | 0 |
| T10Wd | 1.23 | 1.14 | 1.16 | 1.16 | 0.001 | 0 |
| T10Ee | 1.23 | 1.14 | 1.15 | 1.15 | 0.001 | 0 |
| T10We | 1.13 | 1.08 | 1.09 | 1.09 | <0.001 | 0 |
| T10Ef | 1.14 | 1.09 | 1.09 | 1.09 | <0.001 | 0 |
| T10Wf | 1.08 | 1.05 | 1.06 | 1.06 | <0.001 | 0 |
| T10Eg | 1.08 | 1.05 | 1.06 | 1.06 | <0.001 | 0 |
| T10Wg | 1.05 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the CL Function |
|-------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T10Eh | 1.06 | 1.04 | 1.05 | 1.05 | <0.001 | 0 |
| T10Wh | 2.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T10Wi | 3.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T11Ea | 4.31 | 1.20 | 1.21 | 1.21 | 0.003 | 0 |
| T11Wa | 5.35 | 1.22 | 1.24 | 1.24 | 0.004 | 0 |
| T11Eb | 6.20 | 1.13 | 1.14 | 1.14 | 0.002 | 0 |
| T11Wb | 7.24 | 1.15 | 1.17 | 1.17 | 0.003 | 0 |
| T11Ec | 8.15 | 1.09 | 1.10 | 1.10 | 0.002 | 0 |
| T11Wc | 9.18 | 1.11 | 1.12 | 1.12 | 0.002 | 0 |
| T11Ed | 10.10 | 1.07 | 1.07 | 1.07 | 0.001 | 0 |
| T11Wd | 11.13 | 1.08 | 1.09 | 1.09 | 0.001 | 0 |
| T11Ee | 12.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T11We | 13.08 | 1.05 | 1.06 | 1.06 | 0.001 | 0 |
| T11Ef | 14.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T11Wf | 15.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |
| T11Eg | 16.03 | 1.02 | 1.03 | 1.03 | <0.001 | 0 |
| T11Wg | 17.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T11Eh | 18.03 | 1.02 | 1.02 | 1.02 | <0.001 | 0 |
| T11Wh | 19.04 | 1.03 | 1.03 | 1.03 | <0.001 | 0 |
| T11Ei | 20.03 | 1.02 | 1.02 | 1.02 | <0.001 | 0 |
| T11Wi | 21.03 | 1.02 | 1.03 | 1.03 | <0.001 | 0 |
| T12Wa | 23.54 | 2.00 | 2.02 | 2.02 | -0.001 | 0 |
| T12Wb | 24.23 | 1.79 | 1.81 | 1.81 | <0.001 | 0 |
| T12Wc | 24.83 | 1.53 | 1.54 | 1.54 | <0.001 | 0 |
| T12Wd | 25.58 | 1.37 | 1.38 | 1.38 | <0.001 | 0 |
| T12We | 26.32 | 1.20 | 1.21 | 1.21 | <0.001 | 0 |
| T12Wf | 27.18 | 1.12 | 1.12 | 1.12 | <0.001 | 0 |
| T12Wg | 28.10 | 1.07 | 1.07 | 1.07 | <0.001 | 0 |
| T12Wh | 29.07 | 1.05 | 1.05 | 1.05 | <0.001 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | As a % of the CL Function |
|--------------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T12Wi | 30.06 | 1.04 | 1.04 | 1.04 | <0.001 | 0 |

Note: **Bold** denotes a change in deposition of 1% of the critical load.

Appendix F

In-combination process contribution (IAQM guidance approach)

Methodology

As stated in Section 3.2, the IAQM suggests the in-combination contribution from local traffic associated with surrounding local authorities plans and projects to nitrogen and acid deposition may be accounted for by looking at the difference between a future 'no-growth' scenario and the 'Do-Something Scenario'. The 'no growth' scenario assumes baseline (2017) traffic flows with future emission factors and the 'Do-Something Scenario' assumes future traffic flows with future emission factors.

The in-combination contribution from local traffic has been calculated as the difference between Scenarios A and C, as can be seen in Table F.1 and Table F.2.

This in-combination contribution from local traffic is generated as a result of projects and plans within and outside Ashdown Forest and not solely as a result of the MSDC Site Allocations.

Results

Nitrogen deposition

The change in nitrogen deposition between Scenario A and Scenario C is less than 1% of the minimum critical load at Transect points T1, T3 and T4, which suggests there is negligible risk of significant change in potential air quality impacts on sensitive species at Ashdown Forest. The greatest increase in nitrogen deposition is predicted at $0.93 \text{ kgN ha}^{-1} \text{ yr}^{-1}$ at the roadside on Hindleap Lane (T10Ea), which is greater than 1 % of the minimum critical load and requires further consideration by an ecologist to determine whether species at this location are likely to be adversely impacted. The increase in nitrogen deposition exceeds the 1 % indication of potential risk between 50 m to 100 m from the roadside at transects T9 and T10; up to 25 m from the roadside at transects T5, T6, T7, T11 and T12, and up to 10m at transect T8.

Acid deposition

The change in acid deposition between Scenario A and Scenario C is less than 1 % of the critical load function at Transect points T1, T2, T3, T4 and T8, which suggests there will be negligible risk of significant change in potential air quality impacts on sensitive species within Ashdown Forest. Exceedance of the critical load function is predicted up to 10 m from the roadside at Transect T5, T6, T11 and T12; up to 25 m from the roadside at Transects T7, and up to 50 m at Transects T9 and T10. Exceedance of the critical load function at a distance greater than 2 m from the roadside should be investigated further by a qualified ecologist to determine the potential impact to sensitive species.

Summary

As expected, the potential for increased nitrogen and acid deposition as a result of traffic associated with surrounding local authorities proposed plans and projects, including MSDC, to adversely impact sensitive species at Ashdown Forest is greater than the risk that the predicted change in deposition due to traffic associated with the MSDC Sites DPD Scenario only. The assessment of the in-combination contribution from local councils' traffic results in a change greater than 1 % of the critical load, however Mid Sussex traffic only is not expected to lead to a change of greater than 1 % at any modelled receptor points (Section 6, Table E.4 and Table E.5).

This does not necessarily mean that the in-combination contribution to nitrogen and acid deposition will adversely impact sensitive species at Ashdown Forest, but that a qualified ecologist should be consulted.

Table F.1 Total nitrogen deposition at each transect point (kg N/ha/yr)

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the 10 kgN/ha/yr min critical load |
|-------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T1Ea | 24.83 | 20.79 | 20.71 | 20.67 | -0.12 | 0 |
| T1Wa | 22.21 | 19.11 | 19.06 | 19.02 | -0.09 | 0 |
| T1Eb | 22.10 | 19.07 | 19.01 | 18.98 | -0.08 | 0 |
| T1Wb | 19.77 | 17.59 | 17.56 | 17.53 | -0.06 | 0 |
| T1Ec | 19.98 | 17.75 | 17.71 | 17.69 | -0.06 | 0 |
| T1Wc | 18.11 | 16.58 | 16.55 | 16.54 | -0.04 | 0 |
| T1Ed | 18.27 | 16.69 | 16.67 | 16.65 | -0.04 | 0 |
| T1Wd | 16.85 | 15.80 | 15.79 | 15.78 | -0.02 | 0 |
| T1Ee | 16.41 | 15.55 | 15.54 | 15.53 | -0.02 | 0 |
| T1We | 15.60 | 15.05 | 15.05 | 15.04 | -0.01 | 0 |
| T1Ef | 15.52 | 15.00 | 15.00 | 15.00 | 0.00 | 0 |
| T1Wf | 15.03 | 14.70 | 14.71 | 14.71 | 0.00 | 0 |
| T1Eg | 14.99 | 14.68 | 14.69 | 14.68 | 0.00 | 0 |
| T1Wg | 14.71 | 14.51 | 14.52 | 14.51 | 0.00 | 0 |
| T1Eh | 14.81 | 14.57 | 14.57 | 14.57 | 0.00 | 0 |
| T1Wh | 14.60 | 14.44 | 14.45 | 14.45 | 0.01 | 0 |
| T1Ei | 14.70 | 14.51 | 14.51 | 14.51 | 0.00 | 0 |
| T1Wi | 14.56 | 14.42 | 14.43 | 14.43 | 0.01 | 0 |
| T2Ea | 26.19 | 21.66 | 21.82 | 21.77 | 0.11 | 1 |
| T2Wa | 21.92 | 18.92 | 19.03 | 19.00 | 0.07 | 0 |
| T2Eb | 23.27 | 19.82 | 19.94 | 19.91 | 0.09 | 0 |
| T2Wb | 19.48 | 17.41 | 17.48 | 17.47 | 0.05 | 0 |
| T2Ec | 20.87 | 18.32 | 18.40 | 18.38 | 0.06 | 0 |
| T2Wc | 17.92 | 16.46 | 16.51 | 16.50 | 0.04 | 0 |
| T2Ed | 18.94 | 17.11 | 17.18 | 17.16 | 0.05 | 0 |
| T2Wd | 16.76 | 15.75 | 15.79 | 15.78 | 0.03 | 0 |
| T2Ee | 16.83 | 15.81 | 15.85 | 15.84 | 0.03 | 0 |
| T2We | 15.60 | 15.05 | 15.07 | 15.07 | 0.02 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the 10 kgN/ha/yr min critical load |
|------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T2Ef | 15.78 | 15.17 | 15.19 | 15.19 | 0.02 | 0 |
| T2Wf | 15.06 | 14.73 | 14.74 | 14.74 | 0.02 | 0 |
| T2Eg | 15.16 | 14.79 | 14.80 | 14.80 | 0.02 | 0 |
| T2Wg | 14.76 | 14.54 | 14.56 | 14.55 | 0.01 | 0 |
| T2Eh | 14.94 | 14.65 | 14.67 | 14.66 | 0.01 | 0 |
| T2Wh | 14.65 | 14.47 | 14.48 | 14.48 | 0.01 | 0 |
| T2Ei | 14.82 | 14.58 | 14.59 | 14.59 | 0.01 | 0 |
| T2Wi | 14.59 | 14.44 | 14.45 | 14.45 | 0.01 | 0 |
| T3Ea | 23.19 | 19.76 | 19.69 | 19.67 | -0.10 | 0 |
| T3Wa | 19.27 | 17.29 | 17.25 | 17.24 | -0.05 | 0 |
| T3Eb | 21.03 | 18.42 | 18.37 | 18.34 | -0.07 | 0 |
| T3Wb | 17.79 | 16.39 | 16.36 | 16.35 | -0.03 | 0 |
| T3Ec | 19.27 | 17.32 | 17.28 | 17.27 | -0.05 | 0 |
| T3Wc | 16.78 | 15.77 | 15.75 | 15.75 | -0.02 | 0 |
| T3Ed | 17.80 | 16.41 | 16.39 | 16.38 | -0.03 | 0 |
| T3Wd | 15.99 | 15.29 | 15.28 | 15.28 | -0.01 | 0 |
| T3Ee | 16.19 | 15.42 | 15.41 | 15.41 | -0.01 | 0 |
| T3We | 15.19 | 14.81 | 14.81 | 14.80 | 0.00 | 0 |
| T3Ef | 15.41 | 14.94 | 14.94 | 14.94 | 0.00 | 0 |
| T3Wf | 14.82 | 14.58 | 14.59 | 14.59 | 0.00 | 0 |
| T3Eg | 14.94 | 14.65 | 14.66 | 14.66 | 0.00 | 0 |
| T3Wg | 14.61 | 14.45 | 14.46 | 14.46 | 0.01 | 0 |
| T3Eh | 14.77 | 14.55 | 14.56 | 14.56 | 0.00 | 0 |
| T3Wh | 14.53 | 14.41 | 14.41 | 14.41 | 0.01 | 0 |
| T3Ei | 14.68 | 14.50 | 14.50 | 14.50 | 0.01 | 0 |
| T3Wi | 14.49 | 14.38 | 14.39 | 14.39 | 0.01 | 0 |
| T4Ea | 23.12 | 19.71 | 19.70 | 19.66 | -0.05 | 0 |
| T4Wa | 22.75 | 19.51 | 19.49 | 19.46 | -0.04 | 0 |
| T4Eb | 20.50 | 18.07 | 18.06 | 18.04 | -0.03 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the 10 kgN/ha/yr min critical load |
|-------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T4Wb | 20.18 | 17.89 | 17.88 | 17.86 | -0.03 | 0 |
| T4Ec | 18.76 | 16.99 | 16.99 | 16.97 | -0.02 | 0 |
| T4Wc | 18.47 | 16.82 | 16.82 | 16.81 | -0.02 | 0 |
| T4Ed | 17.35 | 16.13 | 16.13 | 16.12 | -0.01 | 0 |
| T4Wd | 17.13 | 15.99 | 15.99 | 15.98 | -0.01 | 0 |
| T4Ee | 15.90 | 15.23 | 15.24 | 15.23 | 0.00 | 0 |
| T4We | 15.76 | 15.15 | 15.15 | 15.15 | 0.00 | 0 |
| T4Ef | 15.21 | 14.82 | 14.83 | 14.82 | 0.00 | 0 |
| T4Wf | 15.12 | 14.76 | 14.77 | 14.76 | 0.00 | 0 |
| T4Eg | 14.82 | 14.58 | 14.59 | 14.59 | 0.01 | 0 |
| T4Wg | 14.75 | 14.54 | 14.55 | 14.54 | 0.01 | 0 |
| T4Eh | 14.68 | 14.50 | 14.50 | 14.50 | 0.01 | 0 |
| T4Wh | 14.63 | 14.46 | 14.47 | 14.47 | 0.01 | 0 |
| T4Ei | 14.61 | 14.45 | 14.46 | 14.46 | 0.01 | 0 |
| T4Wi | 14.56 | 14.42 | 14.43 | 14.43 | 0.01 | 0 |
| T5Ea | 21.50 | 18.69 | 19.01 | 19.08 | 0.39 | 1 |
| T5Wa | 18.83 | 17.04 | 17.24 | 17.28 | 0.24 | 1 |
| T5Eb | 19.42 | 17.40 | 17.62 | 17.67 | 0.28 | 1 |
| T5Wb | 17.32 | 16.11 | 16.24 | 16.27 | 0.16 | 1 |
| T5Ec | 17.98 | 16.51 | 16.68 | 16.71 | 0.20 | 1 |
| T5Wc | 16.47 | 15.59 | 15.68 | 15.70 | 0.12 | 1 |
| T5Ed | 16.86 | 15.82 | 15.93 | 15.96 | 0.14 | 1 |
| T5Wd | 15.81 | 15.18 | 15.25 | 15.26 | 0.08 | 0 |
| T5Ee | 15.73 | 15.13 | 15.20 | 15.21 | 0.07 | 0 |
| T5We | 15.16 | 14.79 | 14.82 | 14.83 | 0.04 | 0 |
| T5Ef | 15.18 | 14.80 | 14.84 | 14.85 | 0.05 | 0 |
| T5Wf | 14.86 | 14.60 | 14.63 | 14.63 | 0.02 | 0 |
| T5Eg | 14.87 | 14.61 | 14.63 | 14.64 | 0.02 | 0 |
| T5Wg | 14.69 | 14.50 | 14.51 | 14.51 | 0.02 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the 10 kgN/ha/yr min critical load |
|-------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T5Eh | 14.76 | 14.54 | 14.56 | 14.56 | 0.02 | 0 |
| T5Wh | 14.62 | 14.46 | 14.47 | 14.47 | 0.01 | 0 |
| T5Ei | 14.69 | 14.50 | 14.52 | 14.52 | 0.02 | 0 |
| T5Wi | 14.61 | 14.45 | 14.47 | 14.46 | 0.01 | 0 |
| T6Ea | 19.46 | 17.43 | 17.62 | 17.70 | 0.27 | 2 |
| T6Wa | 17.20 | 16.03 | 16.15 | 16.19 | 0.15 | 1 |
| T6Eb | 18.18 | 16.63 | 16.78 | 16.84 | 0.20 | 2 |
| T6Wb | 16.34 | 15.51 | 15.58 | 15.61 | 0.11 | 1 |
| T6Ec | 17.19 | 16.03 | 16.14 | 16.18 | 0.15 | 1 |
| T6Wc | 15.78 | 15.17 | 15.23 | 15.25 | 0.08 | 0 |
| T6Ed | 16.33 | 15.50 | 15.58 | 15.61 | 0.11 | 1 |
| T6Wd | 15.35 | 14.90 | 14.94 | 14.96 | 0.06 | 0 |
| T6Ee | 15.42 | 14.95 | 14.99 | 15.00 | 0.06 | 0 |
| T6We | 14.90 | 14.63 | 14.65 | 14.66 | 0.03 | 0 |
| T6Ef | 14.99 | 14.68 | 14.71 | 14.72 | 0.04 | 0 |
| T6Wf | 14.69 | 14.50 | 14.52 | 14.53 | 0.02 | 0 |
| T6Eg | 14.72 | 14.52 | 14.54 | 14.54 | 0.02 | 0 |
| T6Wg | 14.57 | 14.43 | 14.44 | 14.44 | 0.01 | 0 |
| T6Eh | 14.63 | 14.46 | 14.48 | 14.48 | 0.02 | 0 |
| T6Wh | 14.52 | 14.40 | 14.41 | 14.41 | 0.01 | 0 |
| T6Ei | 14.58 | 14.43 | 14.45 | 14.45 | 0.02 | 0 |
| T6Wi | 14.49 | 14.38 | 14.39 | 14.39 | 0.01 | 0 |
| T7Ea | 32.53 | 25.87 | 26.35 | 26.24 | 0.37 | 3 |
| T7Wa | 25.33 | 21.12 | 21.43 | 21.36 | 0.24 | 2 |
| T7Eb | 28.32 | 23.14 | 23.52 | 23.44 | 0.29 | 3 |
| T7Wb | 21.80 | 18.90 | 19.11 | 19.07 | 0.17 | 1 |
| T7Ec | 24.72 | 20.82 | 21.11 | 21.05 | 0.22 | 2 |
| T7Wc | 19.58 | 17.52 | 17.67 | 17.64 | 0.12 | 1 |
| T7Ed | 21.67 | 18.88 | 19.09 | 19.04 | 0.16 | 1 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-A) | As a % of the 10 kgN/ha/yr min critical load |
|-------------|-----------|----------------------------------|------------------------------|--------------------------------|------------------|--|
| T7Wd | 17.88 | 16.46 | 16.57 | 16.55 | 0.09 | 0 |
| T7Ee | 18.26 | 16.73 | 16.85 | 16.82 | 0.09 | 0 |
| T7We | 16.12 | 15.38 | 15.44 | 15.43 | 0.05 | 0 |
| T7Ef | 16.57 | 15.67 | 15.74 | 15.73 | 0.06 | 0 |
| T7Wf | 15.30 | 14.88 | 14.92 | 14.91 | 0.04 | 0 |
| T7Eg | 15.55 | 15.03 | 15.08 | 15.07 | 0.04 | 0 |
| T7Wg | 14.84 | 14.59 | 14.62 | 14.62 | 0.03 | 0 |
| T7Eh | 15.17 | 14.80 | 14.84 | 14.83 | 0.03 | 0 |
| T7Wh | 14.67 | 14.49 | 14.52 | 14.52 | 0.02 | 0 |
| T7Ei | 14.98 | 14.68 | 14.71 | 14.71 | 0.03 | 0 |
| T7Wi | 14.59 | 14.44 | 14.46 | 14.46 | 0.02 | 0 |
| T8Wa | 24.77 | 20.82 | 21.11 | 21.05 | 0.23 | 2 |
| T8Wb | 21.69 | 18.87 | 19.08 | 19.04 | 0.17 | 1 |
| T8Wc | 19.62 | 17.56 | 17.72 | 17.69 | 0.13 | 1 |
| T8Wd | 17.97 | 16.53 | 16.64 | 16.63 | 0.10 | 0 |
| T8We | 16.24 | 15.45 | 15.53 | 15.52 | 0.06 | 0 |
| T8Wf | 15.42 | 14.95 | 15.00 | 15.00 | 0.04 | 0 |
| T8Wg | 14.95 | 14.66 | 14.70 | 14.70 | 0.03 | 0 |
| T8Wh | 14.78 | 14.56 | 14.59 | 14.59 | 0.03 | 0 |
| T8Wi | 14.70 | 14.51 | 14.54 | 14.54 | 0.03 | 0 |
| T9Ea | 23.94 | 20.24 | 21.12 | 21.17 | 0.93 | 9 |
| T9Wa | 22.16 | 19.10 | 19.83 | 19.87 | 0.77 | 7 |
| T9Eb | 21.03 | 18.41 | 19.03 | 19.06 | 0.66 | 6 |
| T9Wb | 19.64 | 17.54 | 18.03 | 18.06 | 0.53 | 5 |
| T9Ec | 19.21 | 17.28 | 17.73 | 17.76 | 0.48 | 4 |
| T9Wc | 18.06 | 16.55 | 16.91 | 16.93 | 0.38 | 3 |
| T9Ed | 17.71 | 16.35 | 16.67 | 16.69 | 0.34 | 3 |
| T9Wd | 16.87 | 15.82 | 16.07 | 16.08 | 0.26 | 2 |
| T9Ee | 16.13 | 15.38 | 15.55 | 15.57 | 0.19 | 1 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the 10 kgN/ha/yr min critical load |
|--------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T9We | 15.64 | 15.07 | 15.20 | 15.21 | 0.14 | 1 |
| T9Ef | 15.37 | 14.92 | 15.02 | 15.03 | 0.11 | 1 |
| T9Wf | 15.07 | 14.73 | 14.81 | 14.82 | 0.09 | 0 |
| T9Eg | 14.92 | 14.64 | 14.70 | 14.71 | 0.07 | 0 |
| T9Wg | 14.75 | 14.53 | 14.59 | 14.59 | 0.05 | 0 |
| T9Eh | 14.76 | 14.54 | 14.59 | 14.59 | 0.05 | 0 |
| T9Wh | 14.63 | 14.46 | 14.51 | 14.51 | 0.04 | 0 |
| T9Ei | 14.67 | 14.49 | 14.53 | 14.53 | 0.04 | 0 |
| T9Wi | 14.57 | 14.43 | 14.46 | 14.46 | 0.04 | 0 |
| T10Ea | 29.46 | 23.63 | 24.52 | 24.56 | 0.94 | 9 |
| T10Wa | 23.64 | 20.01 | 20.57 | 20.59 | 0.57 | 5 |
| T10Eb | 25.73 | 21.28 | 21.96 | 21.99 | 0.70 | 7 |
| T10Wb | 20.43 | 18.02 | 18.38 | 18.40 | 0.38 | 3 |
| T10Ec | 22.48 | 19.26 | 19.75 | 19.77 | 0.51 | 5 |
| T10Wc | 18.63 | 16.91 | 17.17 | 17.18 | 0.27 | 2 |
| T10Ed | 19.95 | 17.70 | 18.04 | 18.05 | 0.35 | 3 |
| T10Wd | 17.27 | 16.07 | 16.25 | 16.25 | 0.19 | 1 |
| T10Ee | 17.24 | 16.05 | 16.22 | 16.23 | 0.18 | 1 |
| T10We | 15.85 | 15.20 | 15.30 | 15.30 | 0.10 | 0 |
| T10Ef | 15.98 | 15.28 | 15.38 | 15.39 | 0.11 | 1 |
| T10Wf | 15.19 | 14.80 | 14.86 | 14.86 | 0.06 | 0 |
| T10Eg | 15.22 | 14.82 | 14.88 | 14.89 | 0.06 | 0 |
| T10Wg | 14.79 | 14.56 | 14.59 | 14.60 | 0.04 | 0 |
| T10Eh | 14.95 | 14.66 | 14.70 | 14.70 | 0.05 | 0 |
| T10Wh | 15.64 | 14.47 | 14.50 | 14.50 | 0.03 | 0 |
| T10Wi | 16.59 | 14.44 | 14.46 | 14.46 | 0.03 | 0 |
| T11Ea | 21.46 | 16.80 | 17.03 | 17.07 | 0.27 | 2 |
| T11Wa | 23.01 | 17.17 | 17.42 | 17.47 | 0.30 | 3 |
| T11Eb | 21.93 | 15.86 | 16.01 | 16.04 | 0.17 | 1 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the 10 kgN/ha/yr min critical load |
|--------------|-----------|-------------------------------------|------------------------------------|--------------------------------------|----------------------|---|
| T11Wb | 23.49 | 16.22 | 16.40 | 16.43 | 0.21 | 2 |
| T11Ec | 23.15 | 15.39 | 15.49 | 15.51 | 0.12 | 1 |
| T11Wc | 24.58 | 15.66 | 15.79 | 15.81 | 0.15 | 1 |
| T11Ed | 24.49 | 14.98 | 15.05 | 15.07 | 0.08 | 0 |
| T11Wd | 25.86 | 15.22 | 15.31 | 15.32 | 0.10 | 1 |
| T11Ee | 25.90 | 14.63 | 14.67 | 14.67 | 0.04 | 0 |
| T11We | 27.17 | 14.80 | 14.85 | 14.86 | 0.06 | 0 |
| T11Ef | 27.65 | 14.48 | 14.50 | 14.50 | 0.03 | 0 |
| T11Wf | 28.85 | 14.60 | 14.63 | 14.64 | 0.04 | 0 |
| T11Eg | 29.52 | 14.40 | 14.42 | 14.42 | 0.02 | 0 |
| T11Wg | 30.65 | 14.48 | 14.50 | 14.50 | 0.03 | 0 |
| T11Eh | 31.48 | 14.37 | 14.39 | 14.39 | 0.01 | 0 |
| T11Wh | 32.58 | 14.43 | 14.45 | 14.46 | 0.02 | 0 |
| T11Ei | 33.46 | 14.36 | 14.38 | 14.38 | 0.02 | 0 |
| T11Wi | 34.54 | 14.41 | 14.43 | 14.43 | 0.02 | 0 |
| T12Wa | 56.64 | 28.05 | 28.39 | 28.38 | 0.33 | 3 |
| T12Wb | 53.29 | 25.15 | 25.42 | 25.42 | 0.27 | 2 |
| T12Wc | 48.70 | 21.48 | 21.67 | 21.67 | 0.19 | 1 |
| T12Wd | 46.24 | 19.25 | 19.38 | 19.38 | 0.13 | 1 |
| T12We | 43.50 | 16.87 | 16.94 | 16.94 | 0.07 | 0 |
| T12Wf | 42.62 | 15.69 | 15.73 | 15.73 | 0.05 | 0 |
| T12Wg | 42.48 | 14.98 | 15.01 | 15.01 | 0.02 | 0 |
| T12Wh | 43.07 | 14.73 | 14.75 | 14.75 | 0.02 | 0 |
| T12Wi | 43.87 | 14.61 | 14.63 | 14.63 | 0.02 | 0 |

Notes: Bold denotes change of greater than 1% of critical load.

Table F.2 Total acid deposition at modelled transect points (keq N / ha/yr)

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the CL function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T1Ea | 1.77 | 1.48 | 1.47 | 1.47 | -0.008 | 0 |
| T1Wa | 1.58 | 1.36 | 1.36 | 1.35 | -0.006 | 0 |
| T1Eb | 1.57 | 1.36 | 1.35 | 1.35 | -0.006 | 0 |
| T1Wb | 1.41 | 1.25 | 1.25 | 1.25 | -0.004 | 0 |
| T1Ec | 1.42 | 1.26 | 1.26 | 1.26 | -0.004 | 0 |
| T1Wc | 1.29 | 1.18 | 1.18 | 1.18 | -0.003 | 0 |
| T1Ed | 1.30 | 1.19 | 1.19 | 1.18 | -0.003 | 0 |
| T1Wd | 1.20 | 1.12 | 1.12 | 1.12 | -0.001 | 0 |
| T1Ee | 1.17 | 1.11 | 1.11 | 1.10 | -0.001 | 0 |
| T1We | 1.11 | 1.07 | 1.07 | 1.07 | -0.001 | 0 |
| T1Ef | 1.10 | 1.07 | 1.07 | 1.07 | 0.000 | 0 |
| T1Wf | 1.07 | 1.05 | 1.05 | 1.05 | 0.000 | 0 |
| T1Eg | 1.07 | 1.04 | 1.04 | 1.04 | 0.000 | 0 |
| T1Wg | 1.05 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T1Eh | 1.05 | 1.04 | 1.04 | 1.04 | 0.000 | 0 |
| T1Wh | 1.04 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T1Ei | 1.05 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T1Wi | 1.04 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T2Ea | 1.86 | 1.54 | 1.55 | 1.55 | 0.008 | 0 |
| T2Wa | 1.56 | 1.35 | 1.35 | 1.35 | 0.005 | 0 |
| T2Eb | 1.66 | 1.41 | 1.42 | 1.42 | 0.006 | 0 |
| T2Wb | 1.39 | 1.24 | 1.24 | 1.24 | 0.004 | 0 |
| T2Ec | 1.49 | 1.30 | 1.31 | 1.31 | 0.004 | 0 |
| T2Wc | 1.27 | 1.17 | 1.17 | 1.17 | 0.003 | 0 |
| T2Ed | 1.35 | 1.22 | 1.22 | 1.22 | 0.004 | 0 |
| T2Wd | 1.19 | 1.12 | 1.12 | 1.12 | 0.002 | 0 |
| T2Ee | 1.20 | 1.12 | 1.13 | 1.13 | 0.002 | 0 |
| T2We | 1.11 | 1.07 | 1.07 | 1.07 | 0.001 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the CL function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T2Ef | 1.12 | 1.08 | 1.08 | 1.08 | 0.001 | 0 |
| T2Wf | 1.07 | 1.05 | 1.05 | 1.05 | 0.001 | 0 |
| T2Eg | 1.08 | 1.05 | 1.05 | 1.05 | 0.001 | 0 |
| T2Wg | 1.05 | 1.03 | 1.04 | 1.04 | 0.001 | 0 |
| T2Eh | 1.06 | 1.04 | 1.04 | 1.04 | 0.001 | 0 |
| T2Wh | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T2Ei | 1.05 | 1.04 | 1.04 | 1.04 | 0.001 | 0 |
| T2Wi | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T3Ea | 1.65 | 1.41 | 1.40 | 1.40 | -0.007 | 0 |
| T3Wa | 1.37 | 1.23 | 1.23 | 1.23 | -0.004 | 0 |
| T3Eb | 1.50 | 1.31 | 1.31 | 1.31 | -0.005 | 0 |
| T3Wb | 1.27 | 1.17 | 1.16 | 1.16 | -0.002 | 0 |
| T3Ec | 1.37 | 1.23 | 1.23 | 1.23 | -0.004 | 0 |
| T3Wc | 1.19 | 1.12 | 1.12 | 1.12 | -0.001 | 0 |
| T3Ed | 1.27 | 1.17 | 1.17 | 1.17 | -0.002 | 0 |
| T3Wd | 1.14 | 1.09 | 1.09 | 1.09 | -0.001 | 0 |
| T3Ee | 1.15 | 1.10 | 1.10 | 1.10 | -0.001 | 0 |
| T3We | 1.08 | 1.05 | 1.05 | 1.05 | 0.000 | 0 |
| T3Ef | 1.10 | 1.06 | 1.06 | 1.06 | 0.000 | 0 |
| T3Wf | 1.05 | 1.04 | 1.04 | 1.04 | 0.000 | 0 |
| T3Eg | 1.06 | 1.04 | 1.04 | 1.04 | 0.000 | 0 |
| T3Wg | 1.04 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T3Eh | 1.05 | 1.03 | 1.04 | 1.04 | 0.000 | 0 |
| T3Wh | 1.03 | 1.02 | 1.03 | 1.03 | 0.000 | 0 |
| T3Ei | 1.04 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T3Wi | 1.03 | 1.02 | 1.02 | 1.02 | 0.000 | 0 |
| T4Ea | 1.65 | 1.40 | 1.40 | 1.40 | -0.003 | 0 |
| T4Wa | 1.62 | 1.39 | 1.39 | 1.38 | -0.003 | 0 |
| T4Eb | 1.46 | 1.29 | 1.29 | 1.28 | -0.002 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the CL function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T4Wb | 1.44 | 1.27 | 1.27 | 1.27 | -0.002 | 0 |
| T4Ec | 1.33 | 1.21 | 1.21 | 1.21 | -0.001 | 0 |
| T4Wc | 1.31 | 1.20 | 1.20 | 1.20 | -0.001 | 0 |
| T4Ed | 1.23 | 1.15 | 1.15 | 1.15 | -0.001 | 0 |
| T4Wd | 1.22 | 1.14 | 1.14 | 1.14 | -0.001 | 0 |
| T4Ee | 1.13 | 1.08 | 1.08 | 1.08 | 0.000 | 0 |
| T4We | 1.12 | 1.08 | 1.08 | 1.08 | 0.000 | 0 |
| T4Ef | 1.08 | 1.05 | 1.05 | 1.05 | 0.000 | 0 |
| T4Wf | 1.08 | 1.05 | 1.05 | 1.05 | 0.000 | 0 |
| T4Eg | 1.05 | 1.04 | 1.04 | 1.04 | 0.000 | 0 |
| T4Wg | 1.05 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T4Eh | 1.04 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T4Wh | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T4Ei | 1.04 | 1.03 | 1.03 | 1.03 | 0.000 | 0 |
| T4Wi | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T5Ea | 1.53 | 1.33 | 1.35 | 1.36 | 0.028 | 2 |
| T5Wa | 1.34 | 1.21 | 1.23 | 1.23 | 0.017 | 1 |
| T5Eb | 1.38 | 1.24 | 1.25 | 1.26 | 0.020 | 2 |
| T5Wb | 1.23 | 1.15 | 1.16 | 1.16 | 0.011 | 1 |
| T5Ec | 1.28 | 1.17 | 1.19 | 1.19 | 0.014 | 1 |
| T5Wc | 1.17 | 1.11 | 1.12 | 1.12 | 0.008 | 0 |
| T5Ed | 1.20 | 1.13 | 1.13 | 1.14 | 0.010 | 1 |
| T5Wd | 1.12 | 1.08 | 1.08 | 1.09 | 0.006 | 0 |
| T5Ee | 1.12 | 1.08 | 1.08 | 1.08 | 0.005 | 0 |
| T5We | 1.08 | 1.05 | 1.05 | 1.05 | 0.003 | 0 |
| T5Ef | 1.08 | 1.05 | 1.06 | 1.06 | 0.003 | 0 |
| T5Wf | 1.06 | 1.04 | 1.04 | 1.04 | 0.002 | 0 |
| T5Eg | 1.06 | 1.04 | 1.04 | 1.04 | 0.002 | 0 |
| T5Wg | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the CL function |
|------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T5Eh | 1.05 | 1.03 | 1.04 | 1.04 | 0.002 | 0 |
| T5Wh | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T5Ei | 1.05 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T5Wi | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T6Ea | 1.38 | 1.24 | 1.25 | 1.26 | 0.019 | 2 |
| T6Wa | 1.22 | 1.14 | 1.15 | 1.15 | 0.011 | 1 |
| T6Eb | 1.29 | 1.18 | 1.19 | 1.20 | 0.014 | 1 |
| T6Wb | 1.16 | 1.10 | 1.11 | 1.11 | 0.008 | 0 |
| T6Ec | 1.22 | 1.14 | 1.15 | 1.15 | 0.011 | 1 |
| T6Wc | 1.12 | 1.08 | 1.08 | 1.08 | 0.006 | 0 |
| T6Ed | 1.16 | 1.10 | 1.11 | 1.11 | 0.008 | 0 |
| T6Wd | 1.09 | 1.06 | 1.06 | 1.06 | 0.004 | 0 |
| T6Ee | 1.10 | 1.06 | 1.07 | 1.07 | 0.004 | 0 |
| T6We | 1.06 | 1.04 | 1.04 | 1.04 | 0.002 | 0 |
| T6Ef | 1.07 | 1.04 | 1.05 | 1.05 | 0.003 | 0 |
| T6Wf | 1.05 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T6Eg | 1.05 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T6Wg | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T6Eh | 1.04 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T6Wh | 1.03 | 1.02 | 1.03 | 1.03 | 0.001 | 0 |
| T6Ei | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T6Wi | 1.03 | 1.02 | 1.02 | 1.02 | 0.001 | 0 |
| T7Ea | 2.32 | 1.84 | 1.88 | 1.87 | 0.027 | 2 |
| T7Wa | 1.80 | 1.50 | 1.53 | 1.52 | 0.017 | 1 |
| T7Eb | 2.02 | 1.65 | 1.67 | 1.67 | 0.021 | 2 |
| T7Wb | 1.55 | 1.34 | 1.36 | 1.36 | 0.012 | 1 |
| T7Ec | 1.76 | 1.48 | 1.50 | 1.50 | 0.016 | 1 |
| T7Wc | 1.39 | 1.25 | 1.26 | 1.25 | 0.009 | 0 |
| T7Ed | 1.54 | 1.34 | 1.36 | 1.35 | 0.012 | 1 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the CL function |
|-------------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T7Wd | 1.27 | 1.17 | 1.18 | 1.18 | 0.006 | 0 |
| T7Ee | 1.30 | 1.19 | 1.20 | 1.20 | 0.007 | 0 |
| T7We | 1.15 | 1.09 | 1.10 | 1.10 | 0.004 | 0 |
| T7Ef | 1.18 | 1.11 | 1.12 | 1.12 | 0.004 | 0 |
| T7Wf | 1.09 | 1.06 | 1.06 | 1.06 | 0.003 | 0 |
| T7Eg | 1.11 | 1.07 | 1.07 | 1.07 | 0.003 | 0 |
| T7Wg | 1.06 | 1.04 | 1.04 | 1.04 | 0.002 | 0 |
| T7Eh | 1.08 | 1.05 | 1.06 | 1.05 | 0.002 | 0 |
| T7Wh | 1.04 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T7Ei | 1.07 | 1.04 | 1.05 | 1.05 | 0.002 | 0 |
| T7Wi | 1.04 | 1.03 | 1.03 | 1.03 | 0.001 | 0 |
| T8Wa | 1.76 | 1.48 | 1.50 | 1.50 | 0.017 | 1 |
| T8Wb | 1.54 | 1.34 | 1.36 | 1.35 | 0.012 | 1 |
| T8Wc | 1.40 | 1.25 | 1.26 | 1.26 | 0.009 | 0 |
| T8Wd | 1.28 | 1.18 | 1.18 | 1.18 | 0.007 | 0 |
| T8We | 1.16 | 1.10 | 1.10 | 1.10 | 0.004 | 0 |
| T8Wf | 1.10 | 1.06 | 1.07 | 1.07 | 0.003 | 0 |
| T8Wg | 1.06 | 1.04 | 1.05 | 1.05 | 0.002 | 0 |
| T8Wh | 1.05 | 1.04 | 1.04 | 1.04 | 0.002 | 0 |
| T8Wi | 1.05 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T9Ea | 1.70 | 1.44 | 1.50 | 1.51 | 0.066 | 6 |
| T9Wa | 1.58 | 1.36 | 1.41 | 1.41 | 0.055 | 5 |
| T9Eb | 1.50 | 1.31 | 1.35 | 1.36 | 0.047 | 4 |
| T9Wb | 1.40 | 1.25 | 1.28 | 1.29 | 0.038 | 3 |
| T9Ec | 1.37 | 1.23 | 1.26 | 1.26 | 0.034 | 3 |
| T9Wc | 1.28 | 1.18 | 1.20 | 1.20 | 0.027 | 2 |
| T9Ed | 1.26 | 1.16 | 1.19 | 1.19 | 0.024 | 2 |
| T9Wd | 1.20 | 1.13 | 1.14 | 1.14 | 0.019 | 1 |
| T9Ee | 1.15 | 1.09 | 1.11 | 1.11 | 0.013 | 1 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the CL function |
|--------------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T9We | 1.11 | 1.07 | 1.08 | 1.08 | 0.010 | 1 |
| T9Ef | 1.09 | 1.06 | 1.07 | 1.07 | 0.008 | 0 |
| T9Wf | 1.07 | 1.05 | 1.05 | 1.05 | 0.006 | 0 |
| T9Eg | 1.06 | 1.04 | 1.05 | 1.05 | 0.005 | 0 |
| T9Wg | 1.05 | 1.03 | 1.04 | 1.04 | 0.004 | 0 |
| T9Eh | 1.05 | 1.03 | 1.04 | 1.04 | 0.004 | 0 |
| T9Wh | 1.04 | 1.03 | 1.03 | 1.03 | 0.003 | 0 |
| T9Ei | 1.04 | 1.03 | 1.03 | 1.03 | 0.003 | 0 |
| T9Wi | 1.04 | 1.03 | 1.03 | 1.03 | 0.003 | 0 |
| T10Ea | 2.10 | 1.68 | 1.75 | 1.75 | 0.067 | 7 |
| T10Wa | 1.68 | 1.42 | 1.46 | 1.47 | 0.041 | 4 |
| T10Eb | 1.83 | 1.51 | 1.56 | 1.56 | 0.050 | 5 |
| T10Wb | 1.45 | 1.28 | 1.31 | 1.31 | 0.027 | 2 |
| T10Ec | 1.60 | 1.37 | 1.41 | 1.41 | 0.036 | 3 |
| T10Wc | 1.33 | 1.20 | 1.22 | 1.22 | 0.019 | 2 |
| T10Ed | 1.42 | 1.26 | 1.28 | 1.28 | 0.025 | 2 |
| T10Wd | 1.23 | 1.14 | 1.16 | 1.16 | 0.013 | 1 |
| T10Ee | 1.23 | 1.14 | 1.15 | 1.15 | 0.013 | 1 |
| T10We | 1.13 | 1.08 | 1.09 | 1.09 | 0.007 | 0 |
| T10Ef | 1.14 | 1.09 | 1.09 | 1.09 | 0.008 | 0 |
| T10Wf | 1.08 | 1.05 | 1.06 | 1.06 | 0.005 | 0 |
| T10Eg | 1.08 | 1.05 | 1.06 | 1.06 | 0.005 | 0 |
| T10Wg | 1.05 | 1.04 | 1.04 | 1.04 | 0.003 | 0 |
| T10Eh | 1.06 | 1.04 | 1.05 | 1.05 | 0.003 | 0 |
| T10Wh | 2.04 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T10Wi | 3.04 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T11Ea | 4.31 | 1.20 | 1.21 | 1.21 | 0.019 | 2 |
| T11Wa | 5.35 | 1.22 | 1.24 | 1.24 | 0.022 | 2 |
| T11Eb | 6.20 | 1.13 | 1.14 | 1.14 | 0.012 | 1 |

| | 2017 Base | Scenario A – 2031 Projected Base | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- A) | As a % of the CL function |
|--------------|-----------|--|------------------------------------|--------------------------------------|----------------------|------------------------------|
| T11Wb | 7.24 | 1.15 | 1.17 | 1.17 | 0.015 | 1 |
| T11Ec | 8.15 | 1.09 | 1.10 | 1.10 | 0.009 | 0 |
| T11Wc | 9.18 | 1.11 | 1.12 | 1.12 | 0.011 | 1 |
| T11Ed | 10.10 | 1.07 | 1.07 | 1.07 | 0.006 | 0 |
| T11Wd | 11.13 | 1.08 | 1.09 | 1.09 | 0.007 | 0 |
| T11Ee | 12.06 | 1.04 | 1.04 | 1.04 | 0.003 | 0 |
| T11We | 13.08 | 1.05 | 1.06 | 1.06 | 0.004 | 0 |
| T11Ef | 14.04 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T11Wf | 15.06 | 1.04 | 1.04 | 1.04 | 0.003 | 0 |
| T11Eg | 16.03 | 1.02 | 1.03 | 1.03 | 0.001 | 0 |
| T11Wg | 17.04 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T11Eh | 18.03 | 1.02 | 1.02 | 1.02 | 0.001 | 0 |
| T11Wh | 19.04 | 1.03 | 1.03 | 1.03 | 0.002 | 0 |
| T11Ei | 20.03 | 1.02 | 1.02 | 1.02 | 0.001 | 0 |
| T11Wi | 21.03 | 1.02 | 1.03 | 1.03 | 0.002 | 0 |
| T12Wa | 23.54 | 2.00 | 2.02 | 2.02 | 0.023 | 2 |
| T12Wb | 24.23 | 1.79 | 1.81 | 1.81 | 0.019 | 2 |
| T12Wc | 24.83 | 1.53 | 1.54 | 1.54 | 0.013 | 1 |
| T12Wd | 25.58 | 1.37 | 1.38 | 1.38 | 0.009 | 0 |
| T12We | 26.32 | 1.20 | 1.21 | 1.21 | 0.005 | 0 |
| T12Wf | 27.18 | 1.12 | 1.12 | 1.12 | 0.003 | 0 |
| T12Wg | 28.10 | 1.07 | 1.07 | 1.07 | 0.002 | 0 |
| T12Wh | 29.07 | 1.05 | 1.05 | 1.05 | 0.001 | 0 |
| T12Wi | 30.06 | 1.04 | 1.04 | 1.04 | 0.001 | 0 |

Note: Bold denotes a change in deposition of 1% of the critical load.



Appendix G

Sensitivity test – NH₃ alternative conversion factor

As the factor of 0.022 used to convert NO_x to NH_3 , derived from the AQC report, is considered to be a worst case approach, a sensitivity test has been carried out using a factor of 0.007 derived from the NAEI emission factors. This has been used to recalculate the predicted NH_3 annual mean concentration in Table F.1, as well as the nitrogen (Table F.2) and acid deposition (Table F.3), for Scenario B – Do Minimum and Scenario C – Do Something. As expected, predicted concentrations and deposition values are lower when the NAEI factor is used to convert NO_x to NH_3 . Due to the uncertainty around ammonia emissions, it is considered more robust to use the AQC conversion factor.

Table G.1 Predicted annual mean NH_3 ($\mu\text{g m}^{-3}$) – comparison of conversion factors

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|--------------------------------|--------------------------------|------------------|-------------------------------|--------------------------------|------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C-B) |
| T1Ea | 0.9 | 0.9 | -0.001 | 1.2 | 1.2 | -0.003 |
| T1Wa | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.002 |
| T1Eb | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.002 |
| T1Wb | 0.8 | 0.8 | -0.001 | 1.0 | 1.0 | -0.002 |
| T1Ec | 0.8 | 0.8 | -0.001 | 1.0 | 1.0 | -0.002 |
| T1Wc | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T1Ed | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T1Wd | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T1Ee | 0.8 | 0.8 | <0.001 | 0.9 | 0.8 | -0.001 |
| T1We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T1Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Ea | 0.9 | 0.9 | -0.001 | 1.3 | 1.3 | -0.003 |
| T2Wa | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.002 |
| T2Eb | 0.9 | 0.9 | -0.001 | 1.2 | 1.2 | -0.002 |
| T2Wb | 0.8 | 0.8 | <0.001 | 1.0 | 1.0 | -0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T2Ec | 0.9 | 0.9 | -0.001 | 1.0 | 1.0 | -0.002 |
| T2Wc | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T2Ed | 0.8 | 0.8 | <0.001 | 1.0 | 1.0 | -0.001 |
| T2Wd | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T2Ee | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T2We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T2Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Ea | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.002 |
| T3Wa | 0.8 | 0.8 | <0.001 | 1.0 | 1.0 | -0.001 |
| T3Eb | 0.9 | 0.9 | <0.001 | 1.0 | 1.0 | -0.001 |
| T3Wb | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T3Ec | 0.8 | 0.8 | <0.001 | 1.0 | 1.0 | -0.001 |
| T3Wc | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.000 |
| T3Ed | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T3Wd | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Ee | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T3Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T3Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Ea | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.003 |
| T4Wa | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.003 |
| T4Eb | 0.8 | 0.8 | -0.001 | 1.0 | 1.0 | -0.002 |
| T4Wb | 0.8 | 0.8 | -0.001 | 1.0 | 1.0 | -0.002 |
| T4Ec | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T4Wc | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T4Ed | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T4Wd | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T4Ee | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T4Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Ea | 0.9 | 0.9 | 0.001 | 1.1 | 1.1 | 0.004 |
| T5Wa | 0.8 | 0.8 | 0.001 | 1.0 | 1.0 | 0.002 |
| T5Eb | 0.8 | 0.8 | 0.001 | 1.0 | 1.0 | 0.002 |
| T5Wb | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |
| T5Ec | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.002 |
| T5Wc | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T5Ed | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |
| T5Wd | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T5Ee | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T5We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T5Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T6Ea | 0.8 | 0.8 | 0.002 | 1.0 | 1.0 | 0.005 |
| T6Wa | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.003 |
| T6Eb | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.004 |
| T6Wb | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.002 |
| T6Ec | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.003 |
| T6Wc | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T6Ed | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.002 |
| T6Wd | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T6Ee | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T6We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T6Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T6Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T6Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T6Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T6Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T6Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T6Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T6Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T7Ea | 1.0 | 1.0 | -0.003 | 1.6 | 1.6 | -0.009 |
| T7Wa | 0.9 | 0.9 | -0.002 | 1.3 | 1.3 | -0.005 |
| T7Eb | 1.0 | 1.0 | -0.002 | 1.4 | 1.4 | -0.007 |
| T7Wb | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.004 |
| T7Ec | 0.9 | 0.9 | -0.002 | 1.2 | 1.2 | -0.005 |
| T7Wc | 0.8 | 0.8 | -0.001 | 1.0 | 1.0 | -0.002 |
| T7Ed | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.003 |
| T7Wd | 0.8 | 0.8 | -0.001 | 0.9 | 0.9 | -0.002 |
| T7Ee | 0.8 | 0.8 | -0.001 | 0.9 | 0.9 | -0.002 |
| T7We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | -0.001 |
| T7Ef | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | -0.001 |
| T7Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T7Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | -0.001 |
| T7Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T7Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T7Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T7Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T7Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T8Wa | 0.9 | 0.9 | -0.002 | 1.2 | 1.2 | -0.005 |
| T8Wb | 0.9 | 0.9 | -0.001 | 1.1 | 1.1 | -0.003 |
| T8Wc | 0.8 | 0.8 | -0.001 | 1.0 | 1.0 | -0.002 |
| T8Wd | 0.8 | 0.8 | -0.001 | 0.9 | 0.9 | -0.002 |
| T8We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | -0.001 |
| T8Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T8Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T8Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|--------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T8Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Ea | 0.9 | 0.9 | 0.001 | 1.2 | 1.2 | 0.002 |
| T9Wa | 0.9 | 0.9 | <0.001 | 1.2 | 1.2 | 0.001 |
| T9Eb | 0.9 | 0.9 | <0.001 | 1.1 | 1.1 | 0.001 |
| T9Wb | 0.8 | 0.8 | <0.001 | 1.0 | 1.0 | 0.001 |
| T9Ec | 0.8 | 0.8 | <0.001 | 1.0 | 1.0 | 0.001 |
| T9Wc | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |
| T9Ed | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |
| T9Wd | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |
| T9Ee | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | <0.001 |
| T9We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T9Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Ea | 1.0 | 1.0 | 0.001 | 1.5 | 1.5 | 0.003 |
| T10Wa | 0.9 | 0.9 | 0.001 | 1.2 | 1.2 | 0.002 |
| T10Eb | 0.9 | 0.9 | 0.001 | 1.3 | 1.3 | 0.003 |
| T10Wb | 0.9 | 0.9 | <0.001 | 1.1 | 1.1 | 0.001 |
| T10Ec | 0.9 | 0.9 | 0.001 | 1.2 | 1.2 | 0.002 |
| T10Wc | 0.8 | 0.8 | <0.001 | 1.0 | 1.0 | 0.001 |
| T10Ed | 0.9 | 0.9 | <0.001 | 1.0 | 1.0 | 0.001 |
| T10Wd | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |
| T10Ee | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | 0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|--------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T10We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T10Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Ea | 0.8 | 0.8 | 0.001 | 1.0 | 1.0 | 0.003 |
| T11Wa | 0.8 | 0.8 | 0.001 | 1.0 | 1.0 | 0.003 |
| T11Eb | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.002 |
| T11Wb | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.002 |
| T11Ec | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T11Wc | 0.8 | 0.8 | 0.001 | 0.9 | 0.9 | 0.002 |
| T11Ed | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T11Wd | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T11Ee | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11We | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | 0.001 |
| T11Ef | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Wf | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Eg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Eh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Ei | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T11Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T12Wa | 1.1 | 1.1 | <0.001 | 1.8 | 1.8 | -0.001 |
| T12Wb | 1.0 | 1.0 | <0.001 | 1.5 | 1.5 | -0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|--------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T12Wc | 0.9 | 0.9 | <0.001 | 1.3 | 1.3 | -0.001 |
| T12Wd | 0.9 | 0.9 | <0.001 | 1.1 | 1.1 | -0.001 |
| T12We | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | <0.001 |
| T12Wf | 0.8 | 0.8 | <0.001 | 0.9 | 0.9 | <0.001 |
| T12Wg | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T12Wh | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |
| T12Wi | 0.8 | 0.8 | <0.001 | 0.8 | 0.8 | <0.001 |

Table G.2 Predicted total nitrogen deposition (kg N / ha/yr) – comparison of conversion factors

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T1Ea | 18.41 | 18.38 | -0.028 | 20.71 | 20.67 | -0.044 |
| T1Wa | 17.35 | 17.33 | -0.020 | 19.06 | 19.02 | -0.032 |
| T1Eb | 17.32 | 17.30 | -0.020 | 19.01 | 18.98 | -0.032 |
| T1Wb | 16.38 | 16.37 | -0.016 | 17.56 | 17.53 | -0.024 |
| T1Ec | 16.48 | 16.47 | -0.016 | 17.71 | 17.69 | -0.024 |
| T1Wc | 15.73 | 15.73 | -0.009 | 16.55 | 16.54 | -0.014 |
| T1Ed | 15.81 | 15.80 | -0.012 | 16.67 | 16.65 | -0.017 |
| T1Wd | 15.24 | 15.23 | -0.008 | 15.79 | 15.78 | -0.011 |
| T1Ee | 15.07 | 15.07 | -0.004 | 15.54 | 15.53 | -0.008 |
| T1We | 14.75 | 14.75 | -0.004 | 15.05 | 15.04 | -0.006 |
| T1Ef | 14.73 | 14.72 | -0.004 | 15.00 | 15.00 | -0.006 |
| T1Wf | 14.53 | 14.53 | -0.001 | 14.71 | 14.71 | -0.002 |
| T1Eg | 14.52 | 14.52 | -0.003 | 14.69 | 14.68 | -0.004 |
| T1Wg | 14.41 | 14.41 | <0.001 | 14.52 | 14.51 | -0.001 |
| T1Eh | 14.44 | 14.44 | <0.001 | 14.57 | 14.57 | -0.001 |
| T1Wh | 14.36 | 14.36 | <0.001 | 14.45 | 14.45 | -0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T1Ei | 14.41 | 14.41 | <0.001 | 14.51 | 14.51 | -0.001 |
| T1Wi | 14.35 | 14.35 | <0.001 | 14.43 | 14.43 | -0.001 |
| T2Ea | 19.11 | 19.08 | -0.028 | 21.82 | 21.77 | -0.044 |
| T2Wa | 17.33 | 17.31 | -0.020 | 19.03 | 19.00 | -0.030 |
| T2Eb | 17.92 | 17.89 | -0.021 | 19.94 | 19.91 | -0.033 |
| T2Wb | 16.34 | 16.32 | -0.012 | 17.48 | 17.47 | -0.019 |
| T2Ec | 16.93 | 16.91 | -0.016 | 18.40 | 18.38 | -0.025 |
| T2Wc | 15.71 | 15.70 | -0.008 | 16.51 | 16.50 | -0.013 |
| T2Ed | 16.14 | 16.13 | -0.009 | 17.18 | 17.16 | -0.015 |
| T2Wd | 15.24 | 15.23 | -0.004 | 15.79 | 15.78 | -0.008 |
| T2Ee | 15.27 | 15.27 | -0.005 | 15.85 | 15.84 | -0.008 |
| T2We | 14.77 | 14.77 | -0.001 | 15.07 | 15.07 | -0.002 |
| T2Ef | 14.85 | 14.84 | -0.004 | 15.19 | 15.19 | -0.006 |
| T2Wf | 14.56 | 14.56 | <0.001 | 14.74 | 14.74 | -0.001 |
| T2Eg | 14.60 | 14.59 | <0.001 | 14.80 | 14.80 | -0.001 |
| T2Wg | 14.43 | 14.43 | -0.003 | 14.56 | 14.55 | -0.004 |
| T2Eh | 14.50 | 14.50 | <0.001 | 14.67 | 14.66 | -0.001 |
| T2Wh | 14.39 | 14.39 | <0.001 | 14.48 | 14.48 | <0.001 |
| T2Ei | 14.46 | 14.45 | -0.003 | 14.59 | 14.59 | -0.004 |
| T2Wi | 14.36 | 14.36 | <0.001 | 14.45 | 14.45 | <0.001 |
| T3Ea | 17.76 | 17.74 | -0.019 | 19.69 | 19.67 | -0.027 |
| T3Wa | 16.19 | 16.18 | -0.011 | 17.25 | 17.24 | -0.015 |
| T3Eb | 16.91 | 16.89 | -0.015 | 18.37 | 18.34 | -0.021 |
| T3Wb | 15.61 | 15.60 | -0.007 | 16.36 | 16.35 | -0.011 |
| T3Ec | 16.20 | 16.20 | -0.008 | 17.28 | 17.27 | -0.013 |
| T3Wc | 15.21 | 15.21 | -0.004 | 15.75 | 15.75 | -0.006 |
| T3Ed | 15.63 | 15.62 | -0.007 | 16.39 | 16.38 | -0.011 |
| T3Wd | 14.91 | 14.90 | -0.004 | 15.28 | 15.28 | -0.005 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T3Ee | 14.99 | 14.99 | -0.004 | 15.41 | 15.41 | -0.005 |
| T3We | 14.60 | 14.60 | <0.001 | 14.81 | 14.80 | -0.001 |
| T3Ef | 14.68 | 14.68 | <0.001 | 14.94 | 14.94 | -0.001 |
| T3Wf | 14.45 | 14.45 | <0.001 | 14.59 | 14.59 | -0.001 |
| T3Eg | 14.50 | 14.50 | <0.001 | 14.66 | 14.66 | -0.001 |
| T3Wg | 14.37 | 14.37 | <0.001 | 14.46 | 14.46 | <0.001 |
| T3Eh | 14.43 | 14.43 | <0.001 | 14.56 | 14.56 | -0.001 |
| T3Wh | 14.34 | 14.34 | <0.001 | 14.41 | 14.41 | <0.001 |
| T3Ei | 14.40 | 14.40 | <0.001 | 14.50 | 14.50 | -0.001 |
| T3Wi | 14.32 | 14.32 | <0.001 | 14.39 | 14.39 | <0.001 |
| T4Ea | 17.75 | 17.74 | -0.019 | 19.70 | 19.66 | -0.035 |
| T4Wa | 17.62 | 17.61 | -0.016 | 19.49 | 19.46 | -0.031 |
| T4Eb | 16.70 | 16.69 | -0.011 | 18.06 | 18.04 | -0.022 |
| T4Wb | 16.59 | 16.58 | -0.014 | 17.88 | 17.86 | -0.024 |
| T4Ec | 16.01 | 16.00 | -0.010 | 16.99 | 16.97 | -0.017 |
| T4Wc | 15.90 | 15.90 | -0.006 | 16.82 | 16.81 | -0.013 |
| T4Ed | 15.45 | 15.45 | -0.005 | 16.13 | 16.12 | -0.011 |
| T4Wd | 15.37 | 15.36 | -0.005 | 15.99 | 15.98 | -0.010 |
| T4Ee | 14.88 | 14.87 | -0.004 | 15.24 | 15.23 | -0.007 |
| T4We | 14.82 | 14.82 | -0.001 | 15.15 | 15.15 | -0.003 |
| T4Ef | 14.61 | 14.61 | -0.001 | 14.83 | 14.82 | -0.002 |
| T4Wf | 14.57 | 14.57 | -0.001 | 14.77 | 14.76 | -0.002 |
| T4Eg | 14.45 | 14.45 | <0.001 | 14.59 | 14.59 | -0.001 |
| T4Wg | 14.43 | 14.43 | <0.001 | 14.55 | 14.54 | -0.001 |
| T4Eh | 14.40 | 14.40 | <0.001 | 14.50 | 14.50 | -0.001 |
| T4Wh | 14.38 | 14.38 | <0.001 | 14.47 | 14.47 | <0.001 |
| T4Ei | 14.37 | 14.37 | <0.001 | 14.46 | 14.46 | -0.001 |
| T4Wi | 14.35 | 14.35 | -0.003 | 14.43 | 14.43 | -0.003 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T5Ea | 17.31 | 17.36 | 0.052 | 19.01 | 19.08 | 0.070 |
| T5Wa | 16.17 | 16.20 | 0.032 | 17.24 | 17.28 | 0.043 |
| T5Eb | 16.42 | 16.46 | 0.038 | 17.62 | 17.67 | 0.051 |
| T5Wb | 15.53 | 15.55 | 0.021 | 16.24 | 16.27 | 0.028 |
| T5Ec | 15.81 | 15.84 | 0.028 | 16.68 | 16.71 | 0.036 |
| T5Wc | 15.16 | 15.18 | 0.017 | 15.68 | 15.70 | 0.022 |
| T5Ed | 15.33 | 15.35 | 0.020 | 15.93 | 15.96 | 0.026 |
| T5Wd | 14.88 | 14.89 | 0.010 | 15.25 | 15.26 | 0.013 |
| T5Ee | 14.85 | 14.86 | 0.010 | 15.20 | 15.21 | 0.013 |
| T5We | 14.61 | 14.61 | 0.004 | 14.82 | 14.83 | 0.005 |
| T5Ef | 14.62 | 14.62 | 0.007 | 14.84 | 14.85 | 0.008 |
| T5Wf | 14.48 | 14.48 | 0.003 | 14.63 | 14.63 | 0.004 |
| T5Eg | 14.48 | 14.48 | <0.001 | 14.63 | 14.64 | 0.001 |
| T5Wg | 14.41 | 14.41 | <0.001 | 14.51 | 14.51 | <0.001 |
| T5Eh | 14.43 | 14.44 | 0.003 | 14.56 | 14.56 | 0.003 |
| T5Wh | 14.38 | 14.38 | <0.001 | 14.47 | 14.47 | <0.001 |
| T5Ei | 14.41 | 14.41 | <0.001 | 14.52 | 14.52 | <0.001 |
| T5Wi | 14.37 | 14.37 | <0.001 | 14.47 | 14.46 | <0.001 |
| T6Ea | 16.42 | 16.47 | 0.053 | 17.62 | 17.70 | 0.078 |
| T6Wa | 15.47 | 15.50 | 0.030 | 16.15 | 16.19 | 0.043 |
| T6Eb | 15.88 | 15.92 | 0.041 | 16.78 | 16.84 | 0.059 |
| T6Wb | 15.10 | 15.12 | 0.019 | 15.58 | 15.61 | 0.028 |
| T6Ec | 15.46 | 15.49 | 0.030 | 16.14 | 16.18 | 0.043 |
| T6Wc | 14.87 | 14.88 | 0.015 | 15.23 | 15.25 | 0.021 |
| T6Ed | 15.10 | 15.12 | 0.019 | 15.58 | 15.61 | 0.028 |
| T6Wd | 14.69 | 14.69 | 0.008 | 14.94 | 14.96 | 0.012 |
| T6Ee | 14.71 | 14.73 | 0.011 | 14.99 | 15.00 | 0.016 |
| T6We | 14.50 | 14.50 | 0.004 | 14.65 | 14.66 | 0.006 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T6Ef | 14.53 | 14.54 | 0.007 | 14.71 | 14.72 | 0.010 |
| T6Wf | 14.41 | 14.41 | 0.003 | 14.52 | 14.53 | 0.005 |
| T6Eg | 14.42 | 14.42 | 0.004 | 14.54 | 14.54 | 0.005 |
| T6Wg | 14.36 | 14.36 | <0.001 | 14.44 | 14.44 | 0.001 |
| T6Eh | 14.38 | 14.39 | 0.003 | 14.48 | 14.48 | 0.004 |
| T6Wh | 14.34 | 14.34 | <0.001 | 14.41 | 14.41 | 0.001 |
| T6Ei | 14.36 | 14.36 | <0.001 | 14.45 | 14.45 | 0.001 |
| T6Wi | 14.33 | 14.33 | <0.001 | 14.39 | 14.39 | <0.001 |
| T7Ea | 21.95 | 21.89 | -0.064 | 26.35 | 26.24 | -0.111 |
| T7Wa | 18.86 | 18.82 | -0.040 | 21.43 | 21.36 | -0.068 |
| T7Eb | 20.18 | 20.13 | -0.050 | 23.52 | 23.44 | -0.085 |
| T7Wb | 17.38 | 17.35 | -0.027 | 19.11 | 19.07 | -0.045 |
| T7Ec | 18.66 | 18.62 | -0.039 | 21.11 | 21.05 | -0.065 |
| T7Wc | 16.45 | 16.43 | -0.018 | 17.67 | 17.64 | -0.031 |
| T7Ed | 17.36 | 17.34 | -0.026 | 19.09 | 19.04 | -0.044 |
| T7Wd | 15.74 | 15.73 | -0.013 | 16.57 | 16.55 | -0.021 |
| T7Ee | 15.92 | 15.90 | -0.016 | 16.85 | 16.82 | -0.026 |
| T7We | 15.01 | 15.00 | -0.008 | 15.44 | 15.43 | -0.012 |
| T7Ef | 15.20 | 15.19 | -0.008 | 15.74 | 15.73 | -0.014 |
| T7Wf | 14.67 | 14.67 | -0.001 | 14.92 | 14.91 | -0.003 |
| T7Eg | 14.77 | 14.77 | -0.001 | 15.08 | 15.07 | -0.004 |
| T7Wg | 14.47 | 14.47 | <0.001 | 14.62 | 14.62 | -0.001 |
| T7Eh | 14.62 | 14.61 | -0.004 | 14.84 | 14.83 | -0.005 |
| T7Wh | 14.41 | 14.41 | <0.001 | 14.52 | 14.52 | -0.001 |
| T7Ei | 14.53 | 14.53 | -0.001 | 14.71 | 14.71 | -0.002 |
| T7Wi | 14.37 | 14.37 | <0.001 | 14.46 | 14.46 | <0.001 |
| T8Wa | 18.65 | 18.62 | -0.036 | 21.11 | 21.05 | -0.062 |
| T8Wb | 17.36 | 17.33 | -0.026 | 19.08 | 19.04 | -0.044 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|--------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T8Wc | 16.48 | 16.47 | -0.018 | 17.72 | 17.69 | -0.030 |
| T8Wd | 15.79 | 15.78 | -0.010 | 16.64 | 16.63 | -0.018 |
| T8We | 15.06 | 15.06 | -0.005 | 15.53 | 15.52 | -0.009 |
| T8Wf | 14.72 | 14.72 | -0.001 | 15.00 | 15.00 | -0.003 |
| T8Wg | 14.52 | 14.52 | <0.001 | 14.70 | 14.70 | -0.001 |
| T8Wh | 14.45 | 14.45 | <0.001 | 14.59 | 14.59 | 0.000 |
| T8Wi | 14.42 | 14.42 | 0.003 | 14.54 | 14.54 | 0.003 |
| T9Ea | 18.64 | 18.67 | 0.039 | 21.12 | 21.17 | 0.048 |
| T9Wa | 17.82 | 17.85 | 0.035 | 19.83 | 19.87 | 0.043 |
| T9Eb | 17.31 | 17.34 | 0.029 | 19.03 | 19.06 | 0.035 |
| T9Wb | 16.67 | 16.70 | 0.026 | 18.03 | 18.06 | 0.031 |
| T9Ec | 16.48 | 16.50 | 0.023 | 17.73 | 17.76 | 0.027 |
| T9Wc | 15.95 | 15.97 | 0.016 | 16.91 | 16.93 | 0.020 |
| T9Ed | 15.80 | 15.81 | 0.013 | 16.67 | 16.69 | 0.017 |
| T9Wd | 15.41 | 15.42 | 0.010 | 16.07 | 16.08 | 0.013 |
| T9Ee | 15.08 | 15.09 | 0.010 | 15.55 | 15.57 | 0.012 |
| T9We | 14.85 | 14.86 | 0.007 | 15.20 | 15.21 | 0.008 |
| T9Ef | 14.73 | 14.74 | 0.004 | 15.02 | 15.03 | 0.005 |
| T9Wf | 14.59 | 14.60 | 0.006 | 14.81 | 14.82 | 0.008 |
| T9Eg | 14.53 | 14.53 | 0.003 | 14.70 | 14.71 | 0.004 |
| T9Wg | 14.45 | 14.45 | 0.001 | 14.59 | 14.59 | 0.001 |
| T9Eh | 14.45 | 14.45 | 0.003 | 14.59 | 14.59 | 0.004 |
| T9Wh | 14.40 | 14.40 | <0.001 | 14.51 | 14.51 | 0.001 |
| T9Ei | 14.41 | 14.41 | <0.001 | 14.53 | 14.53 | 0.001 |
| T9Wi | 14.37 | 14.37 | <0.001 | 14.46 | 14.46 | 0.001 |
| T10Ea | 20.68 | 20.70 | 0.020 | 24.52 | 24.56 | 0.038 |
| T10Wa | 18.23 | 18.24 | 0.011 | 20.57 | 20.59 | 0.022 |
| T10Eb | 19.10 | 19.11 | 0.015 | 21.96 | 21.99 | 0.029 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T10Wb | 16.86 | 16.87 | 0.009 | 18.38 | 18.40 | 0.016 |
| T10Ec | 17.72 | 17.73 | 0.011 | 19.75 | 19.77 | 0.020 |
| T10Wc | 16.09 | 16.09 | 0.005 | 17.17 | 17.18 | 0.010 |
| T10Ed | 16.64 | 16.65 | 0.009 | 18.04 | 18.05 | 0.016 |
| T10Wd | 15.51 | 15.51 | 0.005 | 16.25 | 16.25 | 0.008 |
| T10Ee | 15.49 | 15.49 | 0.005 | 16.22 | 16.23 | 0.008 |
| T10We | 14.90 | 14.90 | 0.001 | 15.30 | 15.30 | 0.003 |
| T10Ef | 14.96 | 14.96 | 0.004 | 15.38 | 15.39 | 0.006 |
| T10Wf | 14.62 | 14.62 | 0.003 | 14.86 | 14.86 | 0.005 |
| T10Eg | 14.64 | 14.64 | 0.003 | 14.88 | 14.89 | 0.005 |
| T10Wg | 14.45 | 14.45 | <0.001 | 14.59 | 14.60 | 0.001 |
| T10Eh | 14.52 | 14.52 | <0.001 | 14.70 | 14.70 | 0.001 |
| T10Wh | 14.39 | 14.39 | <0.001 | 14.50 | 14.50 | 0.001 |
| T10Wi | 14.37 | 14.37 | <0.001 | 14.46 | 14.46 | 0.001 |
| T11Ea | 16.04 | 16.07 | 0.031 | 17.03 | 17.07 | 0.047 |
| T11Wa | 16.29 | 16.33 | 0.035 | 17.42 | 17.47 | 0.053 |
| T11Eb | 15.38 | 15.40 | 0.019 | 16.01 | 16.04 | 0.029 |
| T11Wb | 15.63 | 15.65 | 0.023 | 16.40 | 16.43 | 0.035 |
| T11Ec | 15.04 | 15.05 | 0.015 | 15.49 | 15.51 | 0.022 |
| T11Wc | 15.23 | 15.25 | 0.016 | 15.79 | 15.81 | 0.024 |
| T11Ed | 14.76 | 14.77 | 0.008 | 15.05 | 15.07 | 0.012 |
| T11Wd | 14.92 | 14.93 | 0.012 | 15.31 | 15.32 | 0.017 |
| T11Ee | 14.50 | 14.51 | 0.004 | 14.67 | 14.67 | 0.006 |
| T11We | 14.62 | 14.63 | 0.004 | 14.85 | 14.86 | 0.007 |
| T11Ef | 14.40 | 14.40 | <0.001 | 14.50 | 14.50 | 0.001 |
| T11Wf | 14.48 | 14.49 | 0.004 | 14.63 | 14.64 | 0.006 |
| T11Eg | 14.34 | 14.34 | <0.001 | 14.42 | 14.42 | 0.001 |
| T11Wg | 14.40 | 14.40 | <0.001 | 14.50 | 14.50 | 0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|--------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T11Eh | 14.32 | 14.32 | <0.001 | 14.39 | 14.39 | <0.001 |
| T11Wh | 14.37 | 14.37 | <0.001 | 14.45 | 14.46 | 0.001 |
| T11Ei | 14.31 | 14.31 | <0.001 | 14.38 | 14.38 | <0.001 |
| T11Wi | 14.35 | 14.35 | 0.003 | 14.43 | 14.43 | 0.004 |
| T12Wa | 23.22 | 23.21 | -0.001 | 28.39 | 28.38 | -0.008 |
| T12Wb | 21.37 | 21.38 | 0.003 | 25.42 | 25.42 | -0.003 |
| T12Wc | 19.01 | 19.01 | 0.001 | 21.67 | 21.67 | -0.003 |
| T12Wd | 17.55 | 17.55 | -0.001 | 19.38 | 19.38 | -0.004 |
| T12We | 15.98 | 15.98 | -0.001 | 16.94 | 16.94 | -0.002 |
| T12Wf | 15.20 | 15.20 | <0.001 | 15.73 | 15.73 | -0.001 |
| T12Wg | 14.73 | 14.73 | <0.001 | 15.01 | 15.01 | -0.001 |
| T12Wh | 14.56 | 14.56 | <0.001 | 14.75 | 14.75 | <0.001 |
| T12Wi | 14.48 | 14.48 | <0.001 | 14.63 | 14.63 | <0.001 |

Table G.3 Predicted acid deposition (keq N / ha/yr) – comparison of conversion factors

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T1Ea | 1.31 | 1.31 | -0.002 | 1.47 | 1.47 | -0.003 |
| T1Wa | 1.23 | 1.23 | -0.001 | 1.36 | 1.35 | -0.002 |
| T1Eb | 1.23 | 1.23 | -0.001 | 1.35 | 1.35 | -0.002 |
| T1Wb | 1.17 | 1.16 | -0.001 | 1.25 | 1.25 | -0.002 |
| T1Ec | 1.17 | 1.17 | -0.001 | 1.26 | 1.26 | -0.002 |
| T1Wc | 1.12 | 1.12 | -0.001 | 1.18 | 1.18 | -0.001 |
| T1Ed | 1.12 | 1.12 | -0.001 | 1.19 | 1.18 | -0.001 |
| T1Wd | 1.08 | 1.08 | -0.001 | 1.12 | 1.12 | -0.001 |
| T1Ee | 1.07 | 1.07 | <0.001 | 1.11 | 1.10 | -0.001 |
| T1We | 1.05 | 1.05 | <0.001 | 1.07 | 1.07 | <0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T1Ef | 1.05 | 1.05 | <0.001 | 1.07 | 1.07 | <0.001 |
| T1Wf | 1.03 | 1.03 | <0.001 | 1.05 | 1.05 | <0.001 |
| T1Eg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T1Wg | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T1Eh | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T1Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T1Ei | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T1Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T2Ea | 1.36 | 1.36 | -0.002 | 1.55 | 1.55 | -0.003 |
| T2Wa | 1.23 | 1.23 | -0.001 | 1.35 | 1.35 | -0.002 |
| T2Eb | 1.27 | 1.27 | -0.001 | 1.42 | 1.42 | -0.002 |
| T2Wb | 1.16 | 1.16 | -0.001 | 1.24 | 1.24 | -0.001 |
| T2Ec | 1.20 | 1.20 | -0.001 | 1.31 | 1.31 | -0.002 |
| T2Wc | 1.12 | 1.12 | -0.001 | 1.17 | 1.17 | -0.001 |
| T2Ed | 1.15 | 1.15 | -0.001 | 1.22 | 1.22 | -0.001 |
| T2Wd | 1.08 | 1.08 | <0.001 | 1.12 | 1.12 | -0.001 |
| T2Ee | 1.09 | 1.09 | <0.001 | 1.13 | 1.13 | -0.001 |
| T2We | 1.05 | 1.05 | <0.001 | 1.07 | 1.07 | <0.001 |
| T2Ef | 1.06 | 1.06 | <0.001 | 1.08 | 1.08 | <0.001 |
| T2Wf | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | <0.001 |
| T2Eg | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | <0.001 |
| T2Wg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T2Eh | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T2Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T2Ei | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T2Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T3Ea | 1.26 | 1.26 | -0.001 | 1.40 | 1.40 | -0.002 |
| T3Wa | 1.15 | 1.15 | -0.001 | 1.23 | 1.23 | -0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T3Eb | 1.20 | 1.20 | -0.001 | 1.31 | 1.31 | -0.001 |
| T3Wb | 1.11 | 1.11 | -0.001 | 1.16 | 1.16 | -0.001 |
| T3Ec | 1.15 | 1.15 | -0.001 | 1.23 | 1.23 | -0.001 |
| T3Wc | 1.08 | 1.08 | <0.001 | 1.12 | 1.12 | <0.001 |
| T3Ed | 1.11 | 1.11 | -0.001 | 1.17 | 1.17 | -0.001 |
| T3Wd | 1.06 | 1.06 | <0.001 | 1.09 | 1.09 | <0.001 |
| T3Ee | 1.07 | 1.07 | <0.001 | 1.10 | 1.10 | <0.001 |
| T3We | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | <0.001 |
| T3Ef | 1.04 | 1.04 | <0.001 | 1.06 | 1.06 | <0.001 |
| T3Wf | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T3Eg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T3Wg | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T3Eh | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T3Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T3Ei | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T3Wi | 1.02 | 1.02 | <0.001 | 1.02 | 1.02 | <0.001 |
| T4Ea | 1.26 | 1.26 | -0.001 | 1.40 | 1.40 | -0.002 |
| T4Wa | 1.25 | 1.25 | -0.001 | 1.39 | 1.38 | -0.002 |
| T4Eb | 1.19 | 1.19 | -0.001 | 1.29 | 1.28 | -0.002 |
| T4Wb | 1.18 | 1.18 | -0.001 | 1.27 | 1.27 | -0.002 |
| T4Ec | 1.14 | 1.14 | -0.001 | 1.21 | 1.21 | -0.001 |
| T4Wc | 1.13 | 1.13 | <0.001 | 1.20 | 1.20 | -0.001 |
| T4Ed | 1.10 | 1.10 | <0.001 | 1.15 | 1.15 | -0.001 |
| T4Wd | 1.09 | 1.09 | <0.001 | 1.14 | 1.14 | -0.001 |
| T4Ee | 1.06 | 1.06 | <0.001 | 1.08 | 1.08 | <0.001 |
| T4We | 1.05 | 1.05 | <0.001 | 1.08 | 1.08 | <0.001 |
| T4Ef | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | <0.001 |
| T4Wf | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | <0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T4Eg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T4Wg | 1.03 | 1.03 | <0.001 | 1.03 | 1.03 | <0.001 |
| T4Eh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T4Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T4Ei | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T4Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T5Ea | 1.23 | 1.24 | 0.004 | 1.35 | 1.36 | 0.005 |
| T5Wa | 1.15 | 1.15 | 0.002 | 1.23 | 1.23 | 0.003 |
| T5Eb | 1.17 | 1.17 | 0.003 | 1.25 | 1.26 | 0.004 |
| T5Wb | 1.10 | 1.11 | 0.001 | 1.16 | 1.16 | 0.002 |
| T5Ec | 1.12 | 1.13 | 0.002 | 1.19 | 1.19 | 0.003 |
| T5Wc | 1.08 | 1.08 | 0.001 | 1.12 | 1.12 | 0.002 |
| T5Ed | 1.09 | 1.09 | 0.001 | 1.13 | 1.14 | 0.002 |
| T5Wd | 1.06 | 1.06 | 0.001 | 1.08 | 1.09 | 0.001 |
| T5Ee | 1.06 | 1.06 | 0.001 | 1.08 | 1.08 | 0.001 |
| T5We | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | <0.001 |
| T5Ef | 1.04 | 1.04 | <0.001 | 1.06 | 1.06 | 0.001 |
| T5Wf | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T5Eg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T5Wg | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T5Eh | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T5Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T5Ei | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T5Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T6Ea | 1.17 | 1.17 | 0.004 | 1.25 | 1.26 | 0.006 |
| T6Wa | 1.10 | 1.10 | 0.002 | 1.15 | 1.15 | 0.003 |
| T6Eb | 1.13 | 1.13 | 0.003 | 1.19 | 1.20 | 0.004 |
| T6Wb | 1.07 | 1.08 | 0.001 | 1.11 | 1.11 | 0.002 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|-------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T6Ec | 1.10 | 1.10 | 0.002 | 1.15 | 1.15 | 0.003 |
| T6Wc | 1.06 | 1.06 | 0.001 | 1.08 | 1.08 | 0.002 |
| T6Ed | 1.07 | 1.08 | 0.001 | 1.11 | 1.11 | 0.002 |
| T6Wd | 1.04 | 1.05 | 0.001 | 1.06 | 1.06 | 0.001 |
| T6Ee | 1.05 | 1.05 | 0.001 | 1.07 | 1.07 | 0.001 |
| T6We | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T6Ef | 1.03 | 1.03 | 0.001 | 1.05 | 1.05 | 0.001 |
| T6Wf | 1.02 | 1.03 | <0.001 | 1.03 | 1.03 | <0.001 |
| T6Eg | 1.03 | 1.03 | <0.001 | 1.03 | 1.03 | <0.001 |
| T6Wg | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T6Eh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T6Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T6Ei | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T6Wi | 1.02 | 1.02 | <0.001 | 1.02 | 1.02 | <0.001 |
| T7Ea | 1.56 | 1.56 | -0.005 | 1.88 | 1.87 | -0.008 |
| T7Wa | 1.34 | 1.34 | -0.003 | 1.53 | 1.52 | -0.005 |
| T7Eb | 1.44 | 1.43 | -0.004 | 1.67 | 1.67 | -0.006 |
| T7Wb | 1.24 | 1.23 | -0.002 | 1.36 | 1.36 | -0.003 |
| T7Ec | 1.33 | 1.32 | -0.003 | 1.50 | 1.50 | -0.005 |
| T7Wc | 1.17 | 1.17 | -0.001 | 1.26 | 1.25 | -0.002 |
| T7Ed | 1.24 | 1.23 | -0.002 | 1.36 | 1.35 | -0.003 |
| T7Wd | 1.12 | 1.12 | -0.001 | 1.18 | 1.18 | -0.002 |
| T7Ee | 1.13 | 1.13 | -0.001 | 1.20 | 1.20 | -0.002 |
| T7We | 1.07 | 1.07 | -0.001 | 1.10 | 1.10 | -0.001 |
| T7Ef | 1.08 | 1.08 | -0.001 | 1.12 | 1.12 | -0.001 |
| T7Wf | 1.04 | 1.04 | <0.001 | 1.06 | 1.06 | <0.001 |
| T7Eg | 1.05 | 1.05 | <0.001 | 1.07 | 1.07 | <0.001 |
| T7Wg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T7Eh | 1.04 | 1.04 | <0.001 | 1.06 | 1.05 | <0.001 |
| T7Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T7Ei | 1.03 | 1.03 | <0.001 | 1.05 | 1.05 | <0.001 |
| T7Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T8Wa | 1.33 | 1.32 | -0.003 | 1.50 | 1.50 | -0.004 |
| T8Wb | 1.23 | 1.23 | -0.002 | 1.36 | 1.35 | -0.003 |
| T8Wc | 1.17 | 1.17 | -0.001 | 1.26 | 1.26 | -0.002 |
| T8Wd | 1.12 | 1.12 | -0.001 | 1.18 | 1.18 | -0.001 |
| T8We | 1.07 | 1.07 | <0.001 | 1.10 | 1.10 | -0.001 |
| T8Wf | 1.05 | 1.05 | <0.001 | 1.07 | 1.07 | <0.001 |
| T8Wg | 1.03 | 1.03 | <0.001 | 1.05 | 1.05 | <0.001 |
| T8Wh | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T8Wi | 1.03 | 1.03 | <0.001 | 1.03 | 1.03 | <0.001 |
| T9Ea | 1.33 | 1.33 | 0.003 | 1.50 | 1.51 | 0.003 |
| T9Wa | 1.27 | 1.27 | 0.003 | 1.41 | 1.41 | 0.003 |
| T9Eb | 1.23 | 1.23 | 0.002 | 1.35 | 1.36 | 0.003 |
| T9Wb | 1.19 | 1.19 | 0.002 | 1.28 | 1.29 | 0.002 |
| T9Ec | 1.17 | 1.17 | 0.002 | 1.26 | 1.26 | 0.002 |
| T9Wc | 1.13 | 1.14 | 0.001 | 1.20 | 1.20 | 0.001 |
| T9Ed | 1.12 | 1.12 | 0.001 | 1.19 | 1.19 | 0.001 |
| T9Wd | 1.10 | 1.10 | 0.001 | 1.14 | 1.14 | 0.001 |
| T9Ee | 1.07 | 1.07 | 0.001 | 1.11 | 1.11 | 0.001 |
| T9We | 1.06 | 1.06 | <0.001 | 1.08 | 1.08 | 0.001 |
| T9Ef | 1.05 | 1.05 | <0.001 | 1.07 | 1.07 | <0.001 |
| T9Wf | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | 0.001 |
| T9Eg | 1.03 | 1.03 | <0.001 | 1.05 | 1.05 | <0.001 |
| T9Wg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T9Eh | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|--------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T9Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T9Ei | 1.03 | 1.03 | <0.001 | 1.03 | 1.03 | <0.001 |
| T9Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T10Ea | 1.47 | 1.47 | 0.001 | 1.75 | 1.75 | 0.003 |
| T10Wa | 1.30 | 1.30 | 0.001 | 1.46 | 1.47 | 0.002 |
| T10Eb | 1.36 | 1.36 | 0.001 | 1.56 | 1.56 | 0.002 |
| T10Wb | 1.20 | 1.20 | 0.001 | 1.31 | 1.31 | 0.001 |
| T10Ec | 1.26 | 1.26 | 0.001 | 1.41 | 1.41 | 0.001 |
| T10Wc | 1.14 | 1.15 | <0.001 | 1.22 | 1.22 | 0.001 |
| T10Ed | 1.18 | 1.18 | 0.001 | 1.28 | 1.28 | 0.001 |
| T10Wd | 1.10 | 1.10 | <0.001 | 1.16 | 1.16 | 0.001 |
| T10Ee | 1.10 | 1.10 | <0.001 | 1.15 | 1.15 | 0.001 |
| T10We | 1.06 | 1.06 | <0.001 | 1.09 | 1.09 | <0.001 |
| T10Ef | 1.06 | 1.06 | <0.001 | 1.09 | 1.09 | <0.001 |
| T10Wf | 1.04 | 1.04 | <0.001 | 1.06 | 1.06 | <0.001 |
| T10Eg | 1.04 | 1.04 | <0.001 | 1.06 | 1.06 | <0.001 |
| T10Wg | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T10Eh | 1.03 | 1.03 | <0.001 | 1.05 | 1.05 | <0.001 |
| T10Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T10Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T11Ea | 1.14 | 1.14 | 0.002 | 1.21 | 1.21 | 0.003 |
| T11Wa | 1.16 | 1.16 | 0.002 | 1.24 | 1.24 | 0.004 |
| T11Eb | 1.09 | 1.10 | 0.001 | 1.14 | 1.14 | 0.002 |
| T11Wb | 1.11 | 1.11 | 0.002 | 1.17 | 1.17 | 0.003 |
| T11Ec | 1.07 | 1.07 | 0.001 | 1.10 | 1.10 | 0.002 |
| T11Wc | 1.08 | 1.08 | 0.001 | 1.12 | 1.12 | 0.002 |
| T11Ed | 1.05 | 1.05 | 0.001 | 1.07 | 1.07 | 0.001 |
| T11Wd | 1.06 | 1.06 | 0.001 | 1.09 | 1.09 | 0.001 |

| | NAEI conversion factor (0.007) | | | AQC conversion factor (0.022) | | |
|--------------|------------------------------------|--------------------------------------|----------------------|------------------------------------|--------------------------------------|----------------------|
| | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) | Scenario B – 2031 Do Minimum | Scenario C – 2031 Do Something | Difference (C- B) |
| T11Ee | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T11We | 1.04 | 1.04 | <0.001 | 1.06 | 1.06 | 0.001 |
| T11Ef | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T11Wf | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |
| T11Eg | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T11Wg | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T11Eh | 1.02 | 1.02 | <0.001 | 1.02 | 1.02 | <0.001 |
| T11Wh | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T11Ei | 1.02 | 1.02 | <0.001 | 1.02 | 1.02 | <0.001 |
| T11Wi | 1.02 | 1.02 | <0.001 | 1.03 | 1.03 | <0.001 |
| T12Wa | 1.65 | 1.65 | <0.001 | 2.02 | 2.02 | -0.001 |
| T12Wb | 1.52 | 1.52 | <0.001 | 1.81 | 1.81 | <0.001 |
| T12Wc | 1.35 | 1.35 | <0.001 | 1.54 | 1.54 | <0.001 |
| T12Wd | 1.25 | 1.25 | <0.001 | 1.38 | 1.38 | <0.001 |
| T12We | 1.14 | 1.14 | <0.001 | 1.21 | 1.21 | <0.001 |
| T12Wf | 1.08 | 1.08 | <0.001 | 1.12 | 1.12 | <0.001 |
| T12Wg | 1.05 | 1.05 | <0.001 | 1.07 | 1.07 | <0.001 |
| T12Wh | 1.04 | 1.04 | <0.001 | 1.05 | 1.05 | <0.001 |
| T12Wi | 1.03 | 1.03 | <0.001 | 1.04 | 1.04 | <0.001 |

wood.